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UNITED STATES ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
PRODUCT ASSURANCE DIRECTORATE
DOVER, NJ 07801

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## **RELIABILITY HANDBOOK**

Second Edition
July 1979

## NUCLEAR SYSTEMS DIVISION

PRODUCT ASSURANCE DIRECTORATE

US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND

DOVER, NEW JERSEY

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## **PREFACE**

This handbook is intended as a guide for determining reliability of functioning characteristics of weapon components by testing to failure.

Component reliability of weapon systems is basically a function of engineering design.

Margins of safety used in engineering design to create high reliabilities must be measured by testing to failure techniques to obtain unbiased estimates of reliability.

The author does not hold that the concepts and principles presented herein are final. Revisions will inevitably be made as the state of the art advances.

## **SUMMARY**

- 1. The following are set forth:
- a. The concept of reliability of functioning characteristics of weapon components in terms of stress and strength.
  - b. The operating engineering definition of reliability;
  - c. The complex nature of reliability,
  - d/ Ultimate reliability in terms of safety margins,
  - e. The relationship between test and use conditions. Assault
- f) The limitations of reliability determinations imposed by testing facilities, information and cost.
- 2. A two-phase testing procedure which meets the need for demonstrating high reliabilities with small sample sizes is described in a rational, objective manner. The first phase involves use of fractional-factorial experimental designs to survey effects of important environments. The second phase is a test-to-failure procedure (using the environment found most severe in the first phase) so conducted that reliability-in-use can be calculated from test results.
- 3. The need to plan experiments in advance of data collection and, to test to failure and emphasized. The requirements of a good experiment are treated.
- 4. Several useful fractional-factorial test plans are completely laid out in the form of treatment procedures. Tests of increased severity most useful in testing to failure are described. Examples are given for applying these methods.
- 5. Useful statistical tables, a glossary of terms, and a list of references are included.

## INTRODUCTION

This handbook has been prepared for those engineers and scientists conducting reliability experiments who would like to use statistical techniques to *improve the efficiency of their experiments*. However, it is advisable, especially in the planning stages of testing programs, to supplement the information in this manual by occasional consultations with a statistician.

Planning experiments in the modern statistical sense compols the experimenter explicitly to formulate his objectives and the procedures required to attain them. This often leads to the recognition of fallacies and other difficulties in advance of data collecting.

The statistical aspects of reliability are not new. All of the necessary concepts are adequately treated in modern statistical literature. The lack of information about measurable characteristics of the missile system and the environment it experiences in use, as well as the high cost of test specimens, have created the current problems.

The techniques described in this manual are the most efficient known. They are designed to *inaximize the amount of information obtainable from a given sample size. Very high reliabilities* (0.9999 and higher if they exist) can be demonstrated from very small sample sizes (25 to 30 items). In addition, these techniques are definitive enough to serve as standard procedures throughout the same or different organizations over extended periods of time.

Uniform application of these techniques is as important as their efficiency. A large part of the value of experimentally determined reliability data is the scope of applicability. Reliability data collected by means of standardized procedures are cumulative in the mathematical sense. Hence, the precision with which reliability values are known can be improved with time as additional data are collected. This makes it possible to accumulate a reference file of reliability data on a variety of standard components.

For those readers not thoroughly familiar with statistical terms a glossary of these terms has been included in Appendix 2.

## RELIABILITY CONCEPT

It is assumed that for every missile component there exists a true but unknown "strength" created by the particular (parts) design developed and used by the engineer in building the component. It is further assumed that the true "strength" is a constant and not a random variable for any particular design over short periods of time.

An item will not fail until the applied stress exceeds the items "strength." If the "strength" is much greater than the stress expected to be experienced in use, the chance (probability) of failure in use is very small, and the chance of success (reliability) is very high. It is in this sense that "high reliability" is defined. That is, high reliability means high probability of successful functioning under actual use conditions; it does not mean high reliability under the test conditions.

## RELIABILILITY DEFINITION

The accepted statistical definition of reliability is that reliability is "the probability of successful functioning in use." This is a general definition that is applicable any operating system. However, to define reliability from an operating engineering point of view, the general definition must be modified to include:

- a. The environmental conditions under which successful functioning is required.
- b. The characteristics that are required to function successfully.
- c. The length of time or the number of times successful functioning is required.
- d. When successful functioning is required.

This means that every component can have as many reliabilities as a number equal to the possible combinations of environmental conditions, measurable characteristics and functioning times.

Under the definition that an item cannot fail until the stress exceeds its strength, the reliability with respect to any environment can be determined only if the test specimens are stressed by that environment until failure is obtained. This means that successively higher levels of severity must be used until failure is obtained, as in the applications of successively greater loads until failure is obtained in a tensile test. When the magnitude of the stress at the point of failure cannot be directly observed, then an exploratory type test such as the Bruceton up and-down method is required. This procedure generates the failure rate curve from which the average (ultimate) strength (the point at which the stress equals the strength) can be obtained by finding the stress at which 50 percent of the items fail. In any case the ultimate strength of an item is determined in such a manner that the reliability-in-use can be predicted from the test results.

## LIMITATIONS

## A. Laboratory Testing

In laboratory testing, it is difficult to reproduce the conditions which components will experience operationally. In use, several environments occur simultaneously; in the laboratory, the environments usually have to be applied in sequence. As a result, the environment experienced in use is more severe than that applied at comparable levels of severity in the laboratory. Furthermore, interactions among environments and among components raise the level of severity experienced in use by an additional amount. The extent to which the level of severity is increased in these cases is usually not known.

To cope with unknowns of this kind, engineers use "margins (or factors) of safety" to assure successful functioning in use. As a rational consequence, testing procedures used to test components must, to be of any value, determine the actual margins of safety the engineers have succeeded in building into the new item. To accomplish this, with the limitations imposed by cost considerations, careful planning prior to data collection is required. Useful and realistic component reliability values cannot be obtained by accident or as a by-product of a testing program designed for some other purpose, such as controlling quality. However, reliability values can supplement but not replace quality control and other engineering information.

## B. Information

A complicated system of any kind cannot be fully characterized or described by a single numerical value. Just as the "whole man" cannot be fully described by an intelligence quotient, a whole missile system cannot be fully described or characterized by a single reliability value. Fully to characterize the expected performance of a missile, all possible reliabilities should be:

- a. Determined and weighted in accordance with:
  - (1) Their engineering importance,
  - (2) Probability of occurrence of the various environments.
  - (3) Duration and intensity of the environment,
  - (4) Presence of interaction among environments and among components, and
- b. Mathematically combined:
- (1) In accordance with the way the environments occur (i.e., simultaneously, in combination, or in sequence),
- (2) In various ways to predict the probability of successful functioning of the major and minor subassemblies,
- (3) In accordance with the system circuitry to predict the reliabilities of the over-all system.

#### C. Cost

The cost of measuring the magnitude and interaction effects of the multitude of variables affecting performance of complex missile systems is prohibitive, as in the cost of determining all of an item's possible reliability values, or even a large number of these values. These costs will perhaps remain prohibitive as long as there is a reasonable alternative.

#### **SAFETY MARGINS**

The use of safety margins to assure successful functioning under unpredictable conditions is not new. Currently, reliance is placed on the "safety factor" or the "margin of safety" as an alternative for information. If the expected nominal "stress" (or load) in use is 100 units, designing an item with the "strength" to withstand several times this "stress" gives intuitive assurance that the item will function successfully without failure (i.e., be reliable). Such an item will surely withstand 100 units of "stress" (be highly reliable under this condition) and has a good chance of functioning successfully even when the applied "stress" varies widely, the quality of the material is substandard, or the workmanship is poor. A large margin of safety, then, is a means of assuring successful functioning in the presence of uncontrolled and indeterminate variations in environment, materials, and workmanship. This concept of "stress" and "strength" can be used as a corollary to the definition of reliability given above: An item cannot fail until the stress exceeds its strength. The point at which the stress equals the strength measures the average (ultimate) strength. At this point the reliability equals 50 percent. To raise the reliability above this level, the strength must exceed the expected in-use stress. High strength relative to the stress means high reliability, since the higher the strength, the less likely a failure is to occur.

Construction engineers design an item to with tand several times the load expected in use (for the above reasons), then evaluate the design by neasuring the safety factor of a few representative specimens. This can only be done by applying a load until the specimens break, or fail in some other manner. The breaking load is a measure of the ultimate strength. The "safety factor" is the ultimate strength divided by the load expected in use. The "margin of safety" is the difference between those two loads divided by the expected load in use. Calculating either of these values is as far as construction engineers usually go; they do not calculate a numerical value for the probability of success in use (reliability) created by the safety factor. If the safety factor is large, they feel confident in concluding (predicting) the item was not fail in use.

Missile engineers also use safety margins. They design margins of safety into missile components in many subtle ways and for the same reasons: to assure successful performance in use under uncontrolled and unpredictable conditions. Here, too, the "margin of safety" designed into an item can only be determined by testing to failure. The "stress" required to cause failure can also be termed ultimate "strength."

## ULTIMATE RELIABILITY

The reliability obtained by testing to failure is the ultimate (maximum) reliability, whether a margin of safety is used or not. This is the only unbiased measure of the true reliability created by the design of the item.

Testing without failure demonstrates reliability only in proportion to the number of test specimens used. This is a biased estimate of the ultimate reliability. This means that the ultimate reliability cannot be determined by testing a finite number of specimens without failure.

When only one of the possible total number of reliabilities can be determined, the logical choice is to determine the minimum reliability. If the latter is satisfactory, all other possible reliabilities with respect to separate environments will also be satisfactory. Without a knowledge of the values of all reliabilities, meaningful and realistic system reliabilities can only be predicted from component reliabilities on the basis of the minimum reliabilities.

Experiments must be designed\*. This requires planning in advance of data collection. Test plans must be specifically designed to assure, in advance of data collection, that specified objectives will be attained, for reliability can neither be tested, nor analyzed into an item.

Environmental conditions which cause the poorest (minimum) reliabilities can be found most efficiently (with smallest sample sizes) by means of fractional-factorial designs or their optimized modifications. The object here is to survey environments considered most important to the functioning of the item and to find the environment having the most severe effect (i.e., causing the lowest reliability). This environment is then used to determine the minimum ultimate reliability by testing to failure, using tests of increased severity.

## 7. TESTING WITHOUT FAILURE

The margin of safety designed into a missile component can be determined only by testing to failure. To do otherwise, practically nullifies the value of test results and makes the engineer's effort to use safety margins ineffective. If the test procedure does not measure safety margins, the engineer has no evidence that they exist, and may conclude that other means of increasing reliability (e.g., redundancy) must be used. This line of action is not only costly, bu may create other problems, such as: misplaced center of gravity, overweight, and lack of space.

Testing without failure, which entails large sample sizes, is costly. By this method, it takes 460 items to demonstrate a reliability of at least 99.5 percent with 90 percent confidence. The same reliability can be demonstrated (if it exists in the item) with 25-30 items by testing to failure, using tests of increased severity. In addition the results of testing without failure causes difficulty in calculating system reliability from component reliability because zeros cannot be mathematically manipulated.

Because testing without failure cannot measure ultimate reliability with small sample sizes, trends cannot be detected early enough for taking timely corrective action. For example, if the ultimate reliability of an item actually exceeds that specified in the military characteristics (0.995 or higher), and only 25 items are tested at the use condition without failure during each testing period, no trend will be detected until ultimate reliability of the lot, or stockpile, drops below 0.91 (at the 90 percent confidence level).

<sup>\*</sup> See Reference 12

#### **RELATION BETWEEN TEST AND USE CONDITIONS**

To translate the reliability demonstrated under test conditions to a "reliability-in-use" value, the relation between the "use" and "test" conditions must be established. Experience has shown that this relationship can be adequately represented by frequency distributions. This places the relationship on a probabilistic basis, and also makes possible the use of the laws of probability. If then, the test results are properly collected (see Lab Test Methods), the reliability-in-use can be calculated by extrapolation.

## TEST PLANS

Plans should be made to conduct experiments in two stages:

## A. Factorial experiments:

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For each type of component, the separate effects of the critical environments can be determined most efficiently in one integrated factorial experiment. From these results, the environments having the most severe effects should be selected. When only attribute data can be obtained the optimum condition for conducting this experiment is at a level of severity at which approximately 50 percent of the test specimens can be expected to fail. This type of experiment is highly efficient. The effect of as many as 7 environments can be determined with 8 test specimens, or the effects of 15 environments with 16 test specimens.

## B. Testing to Failure

Within the limitations imposed upon the experiment, determine the reliability with respect to as many as possible of the environments having the most severe effects. This can be accomplished most efficiently using a test of increased severity such as the Bruceton up-and-down method. It is only with this type of test that the ultimate "strength" can be determined when the occurrence of a failure cannot be detected by inspection or when the magnitude of the stress at the point of failure cannot be directly observed. From this information the predicted ultimate "reliability-in-use" can be calculated. Ultimate "reliability-in-use" of any magnitude that exists in an item can be demonstrated with as few as 25 to 30 test specimens by testing the failure with tests of increased severity.

## MODERN STATISTICAL CONCEPTS

## INTRODUCTION

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Because of the nature of reliability and because of the methods required to determine reliability, modern statistical concepts, such as probability, experimental error, population — sample relation, frequency distributions, confidence intervals, sample size, and design of experiment techniques must be understood, if reliability experiments are to be conducted and reliability values calculated and interpreted. It is only with these concepts that the vexing problem of demonstrating high reliabilities with small sample sizes can be solved.

Modern statistical methods of experimentation contain a new ingredient not explicit in mathematics: *Error*. The new philosophy assumes that there is an error in every measurement made and as a consequence, the true values of measurable characteristics can never be known exactly. To cope with this deficiency of measuring processes, repeated measurements are made. Then from this data an interval is calculated which we believe includes the true value represented by the data. Intervals of this kind are called confidence intervals.

Included in the method of calculating these intervals is a means of controlling the proportion of the time that the true value is expected to fall within the interval. Thus the name. This proportion expresses our "confidence" of being right in our prediction that the true value will fall in the interval calculated. Formulas for calculating confidence intervals are given below in Section IX: Reliability Confidence intervals.

#### EXPERIMENTAL ERRORS

If the same characteristic is repeatedly measured with an "accurate" device under constant conditions, the same result will not always be obtained. As a matter of fact, the same result will seldom be repeated. However, it will be noticed that most of the values will cluster rather closely. Only a few very small and very large values will be obtained. It is assumed that these observed deviations are due to chance errors in the measuring process. They are called experimental errors.

## POPULATION VS SAMPLE

The family of values generated by repeated measurements of the same characteristic is called a *population*. A population is generally assumed to be infinite. Any sub-portion of a population is called a sample of that population. A sample is always finite.

## PREDICTION ERRORS

The reasoning behind the new philosophy is as follows: The observations or measurements made in any experiment are, in fact, finite samples of a much larger (infinite) body of data that

could exist had thousands (infinite) of observations been made of the same characteristic under the same constant conditions. It is assumed that unless an infinite number of observations is made, the true value of the characteristic measured will never be exactly known. This reasoning requires focus of attention not on the observed values but on what these values represent — the larger family of all possible values of the characteristic being measured. The objective is to infer from the sample something about the population. Experience has taight that prediction (an inference) cannot be made with certainty. There is always a chance of being wrong. Errors of this type are called the prediction errors.

## FREQUENCY DISTRIBUTION

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if all measurements referred to above are divided into small groups or cells having a range equal to about one-tenth the total range (from maximum to minimum) of all values, there will be about ten cells. Then if a count is taken of the number of values falling within the range of a particular cell, the ratio of this number to the total number of measurements available is the relative frequency of occurrence of measurements (events) in that cell. If the total number of measurements available is very large (1,000 or more) and all values falling within the cell are counted, a very good estimate of the true frequency of occurrence of values in that cell for that particular population will result. Doing this for all the cells would give values that could be plotted on a bar graph as follows: Arrange the cells along the abscissa in ascending order according to the magnitude of the midpoints of their range; erect bars over these midpoints with height proportional to the relative frequency in each cell and widths equal to the cell width. This bar graph is known as a histogram.

## NORMAL DISTRIBUTION

As the total number of values used is increased and the cell width (range) decreased, the step-wise form of the bar graph fades into a smooth curve that is called a frequency distribution. In practice, this is actually how a frequency distribution is formed. It means what the name implies. It is a distribution of (relative) frequencies.

Experience has shown that the families of values generated by repeated measurements of the same characteristic under controlled conditions have definite forms. The most common of these forms and the most useful is called the *normal* frequency distribution. This is the smooth curve described above. It is bellshaped. The family of values forming this distribution is called the normal population.

As the cell width in the bar graph decreases and approaches zero, the height of the bar represents the relative frequency for a single value on the abscissa. Thus there is a relative frequency for any value in the population of measurements. The sum of all the frequencies equals the frequency of all the values in the population which is assigned the numerical value of one. The equation for this function is known, but it is of no direct importance for the purpose of this discussion. It can be found in any standard text on statistics.

## **PROBABILITY**

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From a practical point of view relative frequencies (proportions) are estimates of probabilities. By definition, if it is certain that an event will occur, it is said that the probability of occurrence is equal to unity. If it is certain that an event will *not* occur, it is said that the probability of occurrence is equal to zero.

In the above exemple, if the cell width was equal to the range of the population (from the maximum to the minimum value in the population) it would be certain that the next value taken would fall within this "cell." As a result of taking repeated measurements, all of the values would fall within this "cell." The number of values falling within this "cell" divided by the total number of values will equal unity. That is, the probability of a value's falling within the "cell" (the event) is equal to one.

If, on the other hand, a new cell is taken having a maximum limit less than the minimum of the above population, it is certain that the next value taken from the above population will not fall within the new cell. If repeated measurements are taken from the above population, none of the values will fall within the new cell. The number of values falling within the cell divided by the total number of values will equal zero. That is, the probability of a value's falling within the cell (the event) is equal to zero.

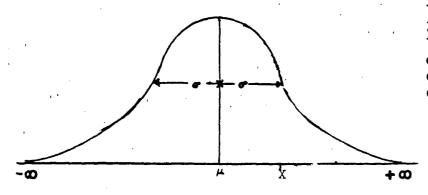
The area under the normal frequency distribution is used to measure probabilities. As shown above, the magnitude of the ordinate associated with any value on the abscissa is a measure of the relative frequency of occurrence (or probability of occurrence) of that value. The summation of all the ordinates below any particular value on the abscissa is, of course, equal to the area under the curve below that ordinate. This area is then a measure of the probability of occurrence of all values in the population below the given value.

#### **PARAMETERS**

Just two parameters or characteristics of the normal frequency distribution are required to define this curve completely. The first parameter is the central value around which most of the values belonging to a particular population will naturally cluster. This parameter is called the true or population mean and is measured by the arithmetic average of all the values in the population. The other parameter required is the dispersion of values around the central value. This parameter is measured by the root mean square of the deviations from the true mean and is called the true or population standard deviation.

Graphically, the mean is the ordinate that passes through the center of gravity of the area under the curve, since this curve is symmetrical. The mean is equal to the mode (the most frequently occurring value) and the median (the middle value).

Also, graphically, the standard deviation is equal to the horizontal distance between the ordinate of the mean and the inflection point on the curve on either side of the mean ordinate.



The Normal Deviate:  $Z = (x - \mu)/\sigma$ This is the linear measure of distance along the base of the curve in standard deviation units.

Where:  $\mu$  = The true population mean.

 $\sigma$  = The true population standard deviation.

X = Any observed value.

The true mean plus or minus one standard deviation includes 68.27 percent of the total area under the curve. The mean plus or minus two standard deviations will include 95.45 percent of the total area under the curve. These values are used to make probability statements. They mean either or both of the following:

A. In generating a normal family of values, 68 percent of the total number of values will lie within plus or minus one standard deviation of the mean. This is especially true if the total number is very large – i.e., 1,000 or more.

B. Randomly chosen values from the normal population have a 68 percent chance or a probability of 0.68 of falling within plus or minus one standard deviation of the mean.

This distribution is unique in nature. It is the curve of regression for the distribution of all small sample averages.

The meaning of the word random as used in modern statistics can be better described than defined. The phrase "randomly chosen values" describes a selection procedure of a very special kind. This procedure is free of biases of all sorts. It is the only procedure which will permit the free play of chance variations, which are the theoretical basis for all modern statistical techniques.

Random selection or random sampling can be accomplished by physically mixing the items before sampling, or by numbering all of the items and then using a table of random numbers to determine which items to select and in what order to select them. Random selection is the process used in lotteries, all numbered tickets being deposited in a revolving drum and a single drawing made by a blindfolded person. It is assumed that such a procedure is completely unbiased, that chance alone is at play, and that each ticket in the drum has an equal chance of being selected. The process of random selection then, not only permits the laws of chance to determine which item is to be chosen, but also the order in which successive items are chosen. This procedure relieves the experimenter completely of any responsibility concerning "which item" and "which order." In the lottery, the operator wants to be "fair." In an experiment, the experimenter wants to be unbiased.

## 11. SAMPLING

In a lottery the relative frequency of occurrence of any particular number is equal to the relative frequency of occurrence of any other number in the drum (population). Each number has an equal chance of being selected if the selection procedure is truly random and unbiased. However, the relative frequency of occurrence of the values in a normal population is not equal. Theoretically, all are different. A little reflection will show, however, that random selection will be "fair" and unbiased here, also. If in a bowl, 900 white beads and 100 red beads are mixed well (i.e., randomized), and a handful of beads selected by a blindfolded person, the ratio of red to white beads in that or any other handful will be close to 1 to 9. The average ratio of a large number of trials (handfuls) will be 1 to 9 -- the relative frequencies of the two colored beads in the bowl, the population. This same relation between sample and population holds true in selecting (sampling) values from a normal distribution if sampling is done in a random fashion. That is, every value (or item) in the population has a chance (probability) of being selected equal to the frequency. with which it actually exists in the population. Only samples that can reflect these actual relative frequencies in the population can be considered as representing the population in an unbiased manner. Samples must correctly represent the population from which they are taken if valid inferences are to be made about the population, from the sample. Of course, successive samples drawn from the same population will not be identical, but if randomly selected, the difference between them will be due to chance errors only. Under these circumstances modern statistical techniques will identify them as having come from the same population, which, in fact, they did.

## 12. ESTIMATES

In practice, to make a measurement (or observation) is to estimate the true population mean. The more observations made and averaged together, the better the estimate. This estimate

is called a "point estimate" to distinguish it from an "interval estimate." However, it is assumed that the true mean is never known exactly unless an infinite number of observations is made.

If the root mean square of the deviations of the individual observations is calculated from the average of all observations, the true population standard deviation can be estimated. As with the mean, however, it is assumed that this true parameter is never known exactly unless an infinite number of observations is made.

13. PREDICTIONS

The two predictions made most often in modern statistics are the following:

- A. The magnitude of the true parameters. These predictions are based on interval estimates which are called confidence intervals.
- B. Whether two or more values belong to the same population. These predictions are called tests of significance.

The prediction problem in modern statistics is to estimate first the population mean and standard deviation and then predict what these two population parameters might be or, given two or more estimates, to predict whether they came from the same population. If there are thousands of observations in each of the samples, the sample means and standard deviations are, for all practical purposes, equal to the population parameters and prediction becomes unnecessary. In practice, however, such large samples are generally not available. They are too costly to obtain. The problem, then, is to predict from small samples what the parameters might be or whether the samples came from the same population.

Intuitively, it is known that predictions cannot be made with certainty — there is always a possibility of being wrong. As a result, to be right as often as possible, reliance is placed on planning. In modern statistics, this possibility is maximized, and chances of being right are actually controlled.

To place this on a mathematical basis the assumption is made that the data have a normal frequency distribution. The normal distribution is then used to calculate the probability of being right in making predictions. This is called the *confidence level* of predictions. The techniques of modern statistics have been developed to make predictions. The assumption that the distribution is normal for variable (measured) data is a reasonable one. Experience has shown that the numerical values of measurable characteristics of products manufactured under controlled conditions are normally distributed (Ref. 11). In addition, the central limit theorem states that the distribution of averages of variable data is normal. So, when comparing averages or calculating confidence intervals of measured data, the assumption of normality is quite valid. This is true of attribute (counted) data only where they are transformed to variable data by some such process as the arc-sine transformation.

#### 1. PREDESIGN PHASE

#### A. Common Sense

Experimental plans and experimental results that violate common sense are discarded, not the common sense.

#### B. Past Experience

Use all available knowledge and information from past experience.

## C. Choice of Variables

Make a comprehensive list of all the variables (factors or environmental treatments) whose effects on the components' functioning characteristics are of interest or must be determined. This should include:

- a. Factors of direct interest.
- b. Factors which may help show how the main factors work.
- c. Factors required to determine the effect of experimental technique. In addition to choosing the variables to be used, their order of use must also be established. The order chosen should be the one most likely to be experienced in use or the one considered most severe. The order selected must be held constant throughout the experiment.

#### D. Choice of Factor Levels

#### a. Number of levels

The number of levels used in the designs described in this manual has been limited to two. These designs are the simplest and the most versatile for conducting multi-factor experiments.

#### b. Position of levels

In using only two levels those used are usually the extremes, such as the presence and absence of an environmental treatment or extremely low and high temperatures. The choice of levels used must be arrived at through the use of good judgement, common sense, and detailed knowledge of the purpose and probable outcome of the investigation. Factorial experiments are most efficient in their ability to detect differences among environmental effects when the levels of severity used are such that approximately 50 percent of the test specimens fail.

## E. Scope

Consider the entire scope of the problem. Without regard to cost, time, or effort consider what it is that must be known eventually. If this turns out to be a very large experiment, the cost of which is prohibitive, divide the whole problem into rational parts. This makes possible a systematically planned approach. It also makes it possible to relate your test plan to cost and the amount of information required.

#### F. Possible Outcomes

Consider all possible outcomes and their physical interpretation. Results that have no physical interpretation have no practical value.

## G. Choice of Criteria

Choose carefully the criteria on which conclusions will be based. To insist that a component have a reliability of 0.999 with respect to temperature shock is of little value when it has a reliability of only 0.80 with respect to transportation vibration.

#### H. Formulation of Hypothesis

Develop the right hypothesis by asking the right questions the experimental results are expected to answer. To show conclusively that component A has a much higher reliability than component B has solved nothing if component A cannot be mass produced.

#### I. Type of Measurement

The type of measurement to be used should be considered for the sake of efficiency. Variable type data can vary from minus infinity to plus infinity and furnish the maximum information per observation. Attribute data are "success" "failure" type data and furnish the least information per observation. From this it is clear that variable type data should be used wherever possible in factorial experiments; care should be exercised, however, in using variable data to determine reliability (see below).

#### J. Choice of Experimental Units

## a. Definition of Experimental Unit

An experimental unit (test specimen) is the smallest sub-division of the experimental material that can receive different treatments.

## b. Size of experimental unit

Sufficient homogeneous or uniform material should be available to conduct a complete set of treatment combinations (required by the experimental design) during a single period of time (such as a day) by a single instrument condition (such as calibration) and by a single operator or group of operators. Material produced during a particular period of time by a single process and by a single manufacturer can be considered homogeneous.

## c. Representative nature of experimental units

The experimental units used should not differ in any important respect from the best known (parts) design to which the conclusions are to apply. If design changes are made on the basis of experimental results, the items used to obtain the results are, of course, not representative of the modified design.

#### d. Independence of Experimental Unit

Experimental units should respond independently of one another. Obtaining a failure on one should not affect any of the others. Using a separate item for each treatment combination will usually assure independence.

## K. Choice of Treatments

Treatments are chosen to give as direct an indication as possible of the functioning characteristics of the components and to include as many as possible of the environmental conditions expected in use. This is an engineering decision that must be based on good judgement and intimate knowledge of the purpose of the experiment.

## L. Sequential Approach

The first experiment may have to be considered exploratory in nature. One or more ideas may be generated during the first experiment concerning parts design modifications or questions may be raised from the results of the first experiment concerning the exact effect of the environmental treatments. In either case additional experimentation would be required to:

- a. Confirm the validity of the modified parts design.
- b. Clarify the effects of the environments which produced the questionable results.
- c. Include other treatments.

Committing oneself to a large experiment at the beginning of a new investigation may not be feasible. Small exploratory experiments may indicate a much more promising approach in a short time and with little cost. In this procedure the results of the first experiment are obtained and analyzed before the next experiment is designed.

## DESIGN PHASE

## A. Choice of design

The factorial design and its modifications described in this manual meet the requirements of environmental testing experiments better than any other known design. The advantages of the recommended factorial designs for environmental testing are as follows:

- a. Simple to use and analyze.
- b. No control groups are required.

- c. The two levels of each treatment can be the presence and absence of the treatment, if desired. Alternatively, any two levels of the treatments can be used.
- d. Each treatment effect can be determined independently of all the others. Unambiguous conclusions can be drawn about each treatment's effects.
- e. Complex experiments involving a large number of treatments can be easily handled.
- f. These are the only experimental designs with which the relationships among treatments can be measured. These designs can determine whether the effect of one treatment depends upon any of the others. These relationships are called interactions.
  - g. The probability of being right or wrong can be controlled.
- h. When the number of treatments used becomes large (three or more), only a fraction (1/2, 1/4, 1/8, etc.) of the total number of combinations of treatments and levels need be used. These designs are called fractional factorials and optimum multifactorials.
- i. A type of statistical analysis can be used that distinguishes between variations due to chance and variations having assignable causes.
- j. More information can be obtained from a given number of test specimens than any other known procedure.
- k. The effective sample size is increased by making it possible to use each observation (or measurement) for more than one purpose. In fact, each treatment effect is determined as though the entire experiment is conducted to determine that particular treatment effect alone. As a result, the precision with which each treatment effect is determined can be based on the total number of test specimens used in the experiment.

#### B. Sample Size

In any experimental situation a reasonable balance must be established between using too few test specimens thus obtaining poor precision, and wasting time and material in attaining unnecessarily high precision by using too many test specimens. When there is a preassigned number of test specimens available, the question is whether it is worthwhile to do the experiment at all. If the number or test specimens available is flexible and adequate, the number required for a given precision or reliability can be calculated in advance. The minimum number of test specimens required in the optimized designs is only one more than the total number of treatments used. The more versatile factorial designs require at least 16 items for five through eight treatments and at least 32 items for nine through thirteen treatments. With twice these numbers of items, the latter designs can also measure interactions.

## C. Orthogonality

The property of these designs, known as orthogonality, must be preserved in order to simplify the analysis and interpretation of the results. This can be done by keeping the number of observations per treatment combination equal and constant throughout the entire design. Orthogonality assures that all the environmental effects and their interrelationships can be independently estimated without entanglement.

## D. Confounding

Confounding is the converse of orthogonality. It means confucing, entangling, or equating two or more factors or treatments so that their separate effects cannot be determined. For example, little can be concluded about the separate effects of the environmental treatments if all of the treatments are applied to each item. If a failure is obtained after an item has received two or more treatments, the cause of the failure is ambiguous; it could be the result of any of the following:

- a. The last treatment.
- b. The last two treatments.
- c. All of the treatments.
- d. Any of the other possible combinations.

The exact cause cannot be determined because the treatments are confounded. This type of confounding should be avoided.

## E. Interactions

Interaction is said to be present when certain particular treatment combinations produce unusual results. This is the non-additive or unpredictable portion of the experiment; as such, interaction effects are considered discoveries by the U.S. Patent Office and as such are the only patentable portion of the experiment. When appreciable interaction effects are present, care must be taken in quoting main (avarage) effects. Any statement about the average effect of a treatment must specify the level of the interacting treatment associated with that average.

However, determination of interaction effects may be the most important information obtained from an experiment. It can explain what otherwise appear to be contradictions. This is the extra information furnished by factorials that cannot be obtained from other designs. Plans should be made to use factorials that can measure interaction effects if there is a possibility that they exist. Higher order interactions can be used as estimates of the error term when multiple replication is not used.

## F. Replication

By replication is meant repetition. One complete replication consists of a single observation for each of the treatment combinations in the design. If the observations are performed in sets, so that a complete replication is done in a continuous period of time (such as a day), with a single measuring system (or instrument), by a single operator, the difference among replications can be used to determine whether the external experimental conditions have remained under control. Multiple replications are also used for the following purposes:

- a. Increase the precision with which treatment effects are determined.
- b. Furnish an independent measure of the error term.
- c. As a basis for calculating the failure rate observed for each treatment combination in preparation for transforming attribute data to a continuous scale in analysis of variance procedures.

## G. Blocking

In general, blocking means dividing the entire design into orthogonal sub-groups. This reduces the number of observations that need be taken in one continuous period of time and reduces the amount of homogenous material required in one batch. Differences among blocks due to uncontrolled changes with time and due to changes in material can be mathematically subtracted out of the system. That is, the object of blocking is to make it possible to conduct the experiment in reasonably small portions. Plans should be made to block any large experiment or any experiment expected to extend over a long period of time. Taking observations in complete replication sets is one form of blocking.

## H. Randomization

Randomization can be accomplished by means of a table of random numbers or by drawing well shuffled numbered cards from a hat. The important characteristic of randomization is that it be an objective impersonal procedure. Proper randomization is determined by examining the procedure producing it, not by examining the results. To randomize does not mean to arrange in an order that looks haphazard. The object of randomization is to permit the laws of chance (probability) to have free play. Proper randomization is the most important requirement for a good experiment because it:

- a. Prevents biased results of all kinds due to such things as, human prejudice, weather cycles, trends in time, heterogeneity of experimental material, etc.
  - b. Removes systematic error.
- c. Relieves the experimenter of the responsibility of choosing which item to test or which test to conduct. Each item or test is equally likely to be chosen. In this sense the experiment is "fair" and unbiased.
- d. Assures the validity of statistical techniques, such as the analysis of variance and associated tests of significance which depend for their validity upon the laws of probability.

However, the use of randomization can be abused. Randomization should not be used to conceal large variations. This drastically reduces the sensitivity of the experiment to detect small differences. All variables known to have, or suspected of having, significant effects on the outcome of an experiment must be either controlled or designed into the experiment. The use of randomization should be considered as an expression of ignorance and used only to remove the effects of small variations after every other source of variation has been included in the design, or controlled. Only the use of good engineering judgment and a knowledge of the system can determine how, when, and where to use randomization.

ANALYSIS PHASE

## A. Statistical Significance

3.

The word significance has a special technical meaning in statistics. Its meaning must be understood in order statistically to analyze and interpret experimental results. One of the most important contributions of statistics is that it has established a means of distinguishing between chance variations and assignable causes. When the observed differences are due to chance variations, these differences are said to be non-significant. This means that the observed results originated from the same source (population). When the observed differences have assignable causes they are said to be significantly different. This means that the observed results have originated from different sources (populations). In a well planned experiment these sources can be identified. In the case of a non-significant difference, changing the treatment from its lower level to its higher level has not caused a detectable difference. In the case of a significant difference, changing the treatment from its lower level to its higher level has caused a detectable difference.

## B. Interpretation

In a good experiment each treatment effect should have a unique interpretation. If two or more interpretations are possible, additional work is required to clarify the ambiguities. One of the most important requirements of a good experimental design is that the conclusions be unambiguous. Fortunately the factorial designs are very helpful in avoiding ambiguity. To conclude that an effect is not significant is not the same as saying that the effect does not exist. We can only say that there is insufficient data to detect the effect. However, if the conclusions are that the effects are significant (from the *test* of significance), we can be assured that the effect is real to the extent of the confidence level associated with the test of significance. Further advantages of factorial designs are as follows:

- a. The range of validity of the conclusions concerning the average (main) effects is extended by the inclusion of more than one variable in the experiment.
- b. Physical interpretation of interactions explain and clarify underlying mechanisms and relationships.

## C. Qualitative Data (Success or Failure)

When only one observation is taken for each treatment combination, analysis of the results from the factorial designs described in this manual is made very simple by using the tables

of minimum contrasts in Appendix 3A. These tables are based on the binomial distribution. The test of significance that uses the values in these tables is known as Fisher's Exact Method for 2 x 2 Contingency Tables. This test is valid even for small sample sizes and will determine not only the main effects but also the two-factor interaction effects when the proper designs are used (see example described below). When multiple (but equal number of) observations are taken for each treatment combination, the Fisher method can still be used. However, an alternate method which is slightly more efficient, but which requires more calculating can also be used. This method transforms the qualitative data to a continuous scale through the use of the arc sine of the proportion or percentage of failures found for each treatment combination. The transformed data can be analyzed by the usual analysis of variance techniques. The tests of significance and their interpretations are both made using the transformed data. If the arc sine transformation is considered desirable, it is suggested that a statistician be consulted to conduct the analysis of variance.

## D. Quantitative Data

For quantitative data (such as g - values, voltages, or time) the usual analysis of variance can be conducted on the observed data provided the variances are homogeneous throughout the design. Since this procedure is somewhat involved, lengthy to describe, and is adequately covered in the literature (see ref. 18 and 19), an attempt will not be made to include the analysis of variance techniques in this manual. It is suggested that a statistician be consulted for this analysis.

1.

## PLANNING TEST PROGRAMS

## STATEMENT OF THE PROBLEM

- A. Identify the new and important problem area.
- B. Outline the specific problem within current limitations.
- C. Define exact scope of the test program.
- D. Determine relationship of the particular problem to the whole research or development program.

## 2. BACKGROUND INFORMATION

- A. Investigate all available sources of information.
- B. Tabulate data pertinent to planning new program.

## 3. METHODS DEVELOPMENT

- A. Hold a conference of all parties concerned.
  - a. State the propositions to be proved.
  - b. Agree on magnitude of differences considered worthwhile.
  - c. Outline the possible alternative outcomes.
  - d. Choose the factors to be studied.
- e. Determine the practical range of these factors and the specific levels at which tests will be made.
  - f. Choose the end measurements which are to be made.
  - g. Consider the effect of sampling variability and of precision of test methods.
  - h. Consider possible inter-relationships (or "interactions") of the factors.
- i. Determine limitations of time, cost, materials, manpower, instrumentation and other facilities and of extraneous conditions, such as weather.
  - j. Consider human relations angles of the program.

<sup>&</sup>lt;sup>a</sup>This outline was received in a private communication from Mr. Charles Bicking, Office, Chief of Ordnance.

## DESIGN OF EXPERIMENT

- A. Design the program in preliminary form.
  - a. Prepare a systematic and inclusive schedule.
  - b. Provide for step-wise performance or adaptation of schedule if necessary.
- c. Eliminate effect of variables not under study by controlling, balancing, or randomizing them.
  - d. Minimize the number of experimental runs.
  - e. Choose the method of statistical analysis.
  - f. Arrange for orderly accumulation of data.
  - B. Review the design with all concerned.
    - a. Adjust the program in line with comments.
    - b. Spell out the steps to be followed in unmistakable terms.

## . DATA COLLECTION

- A. Develop methods, materials, and equipment.
- B. Apply the methods or techniques.
- C. Attend to and check details; modify methods if necessary.
- D. Record any modifications of program design.
- E. Take precautions in collection of data.
- F. Record progress of the program.

## ANALYSIS OF DATA

- A. Reduce recorded data, if necessary, to numerical form.
- B. Apply proper mathematical statistical techniques.

## 7. INTERPRETATION OF RESULTS

- A. Consider all the observed data.
- B. Confine conclusions to strict deductions from the evidence at hand.

- C. Test questions suggested by the data by independent experiments.
- D. Arrive at conclusions as to the technical meaning of results as well as their statistical significance.
  - E. Point out implications of the findings for application and for further work.
  - F. Account for any limitations imposed by the methods used.
  - G. State results in terms of verifiable probabilities.

## COMPONENT RELIABILITY

## INTRODUCTION

V.

1.

Reliability is the probability of the successful performance of a specified characteristic:

- A. Under a specified condition or set of conditions,
- B. For a specified length of time,
- C. After a specified period of storage.

The "length of time" requirement can usually be included as part of the specified conditions.

The storage requirement has to do with age or storage life. This requirement involves the use of life-testing techniques. To be useful these techniques must be able to predict storage life from short-term (a few days or weeks) accelerated laboratory tests. In order for these predictions to be valid, the laboratory test results must be correlated with storage life results by actual long-term storage tests. At present this kind of information is not available.

Life-testing techniques can also be used to determine the reliability of an item with respect to environments whose level of severity can only be increased by increasing the length of time of exposure. To do this, however, requires the establishment of a minimum length of exposure time for successful functioning. The difficulty here is that component reliabilities established by tests of increased severity, in which time is the variable, are not comparable with component reliabilities established by tests of increased severity in which the level of the environment is the variable.

These two kinds of component reliability cannot both be used in the same system to calculate the reliability of that system and have the result meaningful.

## The Ideal Test Condition

The ideal condition for determining reliability is that condition found in tensile or compression testing. That is, the following conditions exist which make possible the most efficient determination of the ultimate strength:

- 1. The observed results are in the form of variable-type data.
- 2. The severity of the applied stress can be easily increased until failure occurs.
- 3. The magnitude of the applied stress is continuously available so that the load at the point of failure can be directly observed.
  - 4. The occurrence of failure can be detected by inspection.
  - 5. The average of the observed results is an unbiased estimate of the ultimate strength.

With this combination of conditions and information the greatest precision and accuracy can be obtained with the smallest sample size. Aside from being convenient and easy to conduct, this method gives a direct measure of the ultimate strength and therefore the margin of safety from which reliability-in-use can be calculated.

The efficiency of variable-type data can be fully exploited here since each observed value is at the point of failure. This is the value of the stress that the 50% point on the cumulative frequency curve estimates in the indirect methods described in Section XI 3: Tests of Increased Severity. This average value at the point of failure in the ideal test and the 50% point in the indirect methods is important since it is the only unbiased measure of the ultimate strength, the margin of safety, and the reliability-in-use.

In all reliability testing the characteristics of the ideal testing condition should be kept in mind as a guide in more complicated situations where indirect methods must be used. In this way the disadvantages of testing without failure and collecting variable-type data at a single stress level can be seen in better perspective. For example, measuring the resistance of the circuits of several similar test specimens at a single voltage cannot measure reliability. This procedure gives only one point on the (I<sup>2</sup>R)-strength curve. Where the point at which 50% of the items fail or what the margin of safety is cannot be determined using a single voltage value. Calculating the probability of obtaining resistance values outside given limits with information of this kind assumes that the margin of safety is equal to zero.

## 2. COMPONENT TESTING

Component testing can be accomplished in either of two ways, controlled laboratory tests, or flight tests. Each of these has its advantages and disadvantages:

- A. Advantages of controlled laboratory testing are:
- a. <u>Cost</u> This is the cheapest method both from the cost of test facilities and from the cost of test specimens for determining reliability with respect to separate environments during the development phase.
- b. <u>Information.</u> Complete information can be obtained since the test specimens are available for complete instrumentation and visual examination.
- c. <u>Controlled conditions</u> Each test specimen can be subjected to precisely the desired treatment.
- d. Results Unbiased estimates of reliability can be obtained by testing to failure in a predetermined manner so that the average reliability-in-use can be predicted from the test results
- e. <u>Efficiency</u> Tests of increased severity can be used to demonstrate high reliability with small sample sizes.
- f. System reliability prediction Information can be furnished on a current basis during the development phase of an item which can be used as a guide during development and which can be used to predict the expected system reliability.
  - B. Disadvantages of controlled laboratory testing are:
- a. <u>Facility limitations</u> Environments must be applied in sequence instead of simultaneously as experienced in used.

- b. System reliability prediction System reliabilities are predicted with incomplete information. The extent of component interaction and independence is not known. The degree to which the human factor, during assembly, reduces reliability is also not known.
- c. <u>Sample size</u> Larger sample sizes are required for laboratory testing of components under use conditions than for testing systems in flight to demonstrate a given systems reliability.
  - C. Advantages of flight tests are:
- a. <u>Environment</u> Test specimens are subjected to actual use conditions; all of the environments are applied simultaneously and at the correct level of intensity and duration.
- b. <u>Verification</u> Flight testing is a means of verifying all of the predictions based on component values and other information.
  - D. Disadvantages of flight tests are:
    - a. Observation The tested specimens are not available for examination.
    - b. Measuring system Measurement by telemetry is not precise or reliable.
    - c. Cost The cost of flying a test vehicle is excessive.
- d. Storage characteristics Storage characteristics cannot be determined by flight tests.
- E. From the above description of the relative merits of laboratory testing and flight testing the following conclusions can be drawn:
  - a. Laboratory testing furnishes the most information.
- b. Efforts to improve testing methods should be directed to improving laboratory methods.

CALCULATION

A. Tests of increased severity

$$R = 1 \cdot P$$

Where:

R = Mean reliability over the range of in-use conditions

P = Probability of failure-in-use measured by the overlapping areas under the stress and strength curves (see page 112 for curves) and which can be found by entering a table of areas under the standard normal curve (Appendix 3G) with the following normal deviate:

$$Z = \frac{(X_1 \cdot X_2) \cdot (M_1 \cdot M_2)}{\sqrt{\sigma_1^2 + \sigma_2^2}}$$

A failure can occur only when:

$$x_1>x_2$$

Therefore the normal deviate becomes:

$$z \ge \frac{M_2 \cdot M_1}{\sqrt{\frac{2}{\sigma_1} + \sigma_2^2}}$$

X<sub>1</sub> = any stress value

X<sub>2</sub> = any strength value

M<sub>1</sub> = True (but unknown) mean of the stress distribution

M<sub>2</sub> = True (but unknown) mean of the strength (failure) distribution

 $\sigma_1^2$  = True (but unknown) variance of the stress distribution

 $\sigma_2^2 = True$  (but unknown) variance of the strength (failure) distribution.

The above values can be estimated from sample results as follows:

$$\hat{R} = 1.\hat{P}$$

Where:

A = An estimate of the true reliability (R)

P = An estimate of the true probability (P) of failure-in-use which can be found by entering a table of areas under the standard normal curve (appendix 3G) with the following calculated value:

$$T \geq \frac{|\bar{x}_{2} \cdot \bar{x}_{1}|}{\sqrt{\sum_{s_{11}^{2} + s_{12}^{2}}^{2}}}$$

Where:

T = The normal deviate listed in appendix 3G for each P value.

 $X_1$  = Average in-use condition (in terms of the environmental stress level) established by experience or actual measurement of the handling, storage, or flight conditions.

- $\overline{X}_2$  = Average stress at the observed point of failure, or the stress at the point 50-percent point on the failure rate curve established by a test of increased failure when the occurrence of a failure cannot be determined by inspection.
- $|\overline{X}_1 \cdot \overline{X}_2|$  = Absolute difference between the two averages without regard to the algebraic sign, which is a measure of the margin of safety.
- s<sub>1</sub> = Standard deviation of the in-use conditions (in terms of the environmental stress level) established by actual measurement of handling, storage, and flight conditions.
- s<sub>2</sub> = Standard deviation of the stress at the observed point of failure or standard deviation of the failure rate curve (in terms of the environmental stress level) established by a Bruceton-type test of increased severity when the environmental stress levels at the point of failure cannot be observed directly.
- B. <u>Life tests.</u> When time is the variable rather than the level of the environment and the length of time  $(t_i)$  is observed for each failure and the test terminated at the exact time  $(t_a)$  of the last failure:

$$\hat{R} = e^{-t/m}$$

Where:

R = Sample reliability under the *test* condition as the probability of no failures in time (t).

e = 2.7183

$$m = \frac{t_1 + t_2 + \cdots + t_a^{h} + (n-a) t_a}{a} = \frac{h}{a} = Time per failure$$

t<sub>i</sub> = Time to failure of individual components.

h # Time during which "a" failures occurred.

a = Number of components that failed in time (h)

n = Number of components tested.

t # Required failure-free time.

This formula is not applicable during infant mortality or wear-out periods.

- C. <u>Binomial-type data (binomial distribution)</u>. The following technique is applicable when these conditions pertain:
  - a. The lot or population represented by the sample is very large or infinite.
  - b. The sample size is less than 10 percent of the lot size.

c. Each test specimen can fail in only one way.

$$\hat{P} = \frac{k}{n}$$

Where:

R = Sample reliability. The probability of success under the *test* condition.

k = Number of successes.

n = Number of test specimens or number of trials.

D. <u>Variable-type data</u>. By definition reliability is the probability that an item will perform successfully under a specified set of conditions which can include environments, or time, or both. If it does not perform successfully, the item fails. By definition there are only two possible outcomes; success or failure. There are no other alternatives in reliability testing.\* Half of the test specimens used can perform successfully, but any particular specimen cannot "only half succeed" or "succeed half way." Just as when tossing coins, heads can occur on half of the coins, but on any one coin there cannot be a "half of a head."

By definition then, there are only two possible outcomes in reliability testing. Data of this type — called attribute data — have only discrete values — are obtained by a counting process.

Variable data, as the name implies, can vary on a continuous scale-from zero to infinity. This type of data is obtained by a measuring process.

Text books on the subject of statistics state that variable data are more efficient than attribute data because more information is obtained per observation. But this advantage of variable data does not pertain to reliability testing except in the direct method where the observed values estimate the ultimate strength. If variable data be used for reliability testing in other cases, they can only be for the purpose of measuring a characteristic of the test specimen to determine the number of successes or failures. In this application, the "text book" efficiency of variable data is lost — the results obtained in this manner can be used in the formulas given above for calculating reliability.

The probability of a measured value's exceeding a given limit obtained from the average and standard deviation of a dependent variable (such as, ohms resistance, percent elongation, timing accuracy or hardness) at ambient static conditions does not measure reliability. There can never be a reliability with respect to a dependent variable. Dependent variables are properties of an item or material the same as reliability is a property.

<sup>\*</sup>Reliability testing means the stressing of a test specimen by an environment or time, to measure the margin of safety.

An item or material cannot be stressed by, or subjected to, its own properties. In failure testing an item's properties can be used to determine only the number of successes or failures when the item or material is being stressed by or subjected to an independent variable such as, F.M.F. in volts, tensile load in pounds, or vibration in g's. In cases of this kind the observed proportion of successes measures the reliability with respect to the independent variable. The average and standard deviation of dependent variables at ambient static conditions can measure only the quality of material, the quality of the manufacturing process, or the effect of handling or storage on the measured properites — not reliability. Although there can be reliability with respect to storage conditions, this reliability must be measured using time as one of the independent variables in distributions such as the Poisson. Reliabilities of this kind are stated in terms of the probability of no failures in a given length of time, not as the probability of a value exceeding a given limit.

#### INTRODUCTION

The advantages and disadvantages of laboratory and flight tests described above for components also pertain to testing complete systems; however, testing complete systems cannot be used as a prediction procedure during R and D since it is testing after the fact. In addition, testing complete systems is expensive and difficult even in the laboratory. As a result, it is concluded that component testing must be done during the development phase in order to obtain the required detailed information when it is needed. In so doing, all of the shortcomings of the several methods of reliability testing which constitute the state of the arc, culminate in the estimate of system reliability. Some of the errors are compensatory, as:

- A. Errors that underestimate reliability.
  - a. Testing without failure.
  - b. Estimating reliability under extreme use conditions only.
- B. Errors that overestimate reliability.
  - a. Applying environments in sequence instead of simultaneously.
  - b. Estimating reliability with respect to only one environment.
- c. Calculating system relabilities on the assumption that components function and react to environments independently.

To what extent these errors compensate one another is not known.

The one hig advantage of testing complete systems under use conditions after the R and D phase, such as flight tests during stockpile testing, is the higher reliability that can be demonstrated in series systems with a given sample size. For example, if 15 adaption kits are flight trated without a failure, this demonstrates a system reliability of at least 85 percent at the 90 percent (one-sided) confidence level. On the assumption that the adaption kit is made up of 5 major components in series, it would be necessary that 70 of each of the 5 major components be tested without a failure to demonstrate an equivalent system reliability calculated from the components. In addition the difficulty of how to apply the environments to the components in the laboratory would be encountered.

# 2.

## CALCULATION

Obtaining point estimates of system reliabilities from component reliabilities requires the development of a probability equation based on the circuitry of the system and the laws of probability. Since this procedure is treated extensively in readily available literature, such as reference 15, it has not been included here.

When each test specimen (such as a system) can fail in more than one way, the Poisson distribution can be used as follows (ref. 14):

$$^{\wedge}_{R=e}\overline{X}$$

Where:

 $\stackrel{\wedge}{R}$  = Sample reliability under the test condition as the probability of no failures.

e = 2.7183

 $\overline{X}$  = a/n the average number of failures.

a = Number of failures.

n = Number of test specimens.

3.

# **SAFETY**

Safety can be defined as the probability of a catastrophic failure. A measure of this characteristic can be obtained from the techniques described herein for reliability, with slight modification. For the determination of safety, only catastrophic failures can be counted and used. In this case, of course, the objective is to calculate the probability of a failure-in-use — not its complement.

The relation between safety and reliability can best be seen from the following diagram:

### **PROBABILITIES**

### 1. Introduction

# A. Definition

A confidence interval is a range of values within which the true population parametersuch as reliability-is expected to lie. The confidence level associated with this interval is a probability statement expressing the proportion of the time the true value is expected to be within the interval or, is the probability of being right in predicting that the true value will be within the calculated interval.

### B. Best Estimate

In order to calculate a valid confidence interval the "best point estimate" of the true population parameter must first be obtained. Whether an estimator is the "best" depends on how it is determined and how it is used. On the assumption that the estimator used is the correct one for the intended purpose, it is considered an unbiased point estimate if the mean of all the possible sample values equals the true population parameter. This also means that the estimator is accurate. In addition to being unbiased the estimator used should also be efficient. That is, the unbiased estimator chosen for use should have the minimum variance of all the possible unbiased estimators that Lould be used. This means that the estimator should be precise. An estimator that is both unbiased (accurate) and efficient (precise) is said to give the "best estimate" of the true population parameter. It is this kind of estimator that is required to calculate valid confidence intervals or confidence limits.

In most engineering work the arithmetic average of variable data is the "best estimate" of the true mean of the population represented by the data. That is, the arithmetic mean meets the requirements of a "best estimate" since:

- (1) The mean of all the possible sample (arithmetic) averages equals the true mean and is therefore unbiased.
- (2) The variance of the arithmetic mean is smaller than those of other possible estimators, such as the median, mode, or mid-range.

What has been said above for variable data is also true for attribute data. This means that in both cases the "best estimate" of the true population mean is the observed or sample average.

In reliability testing the "best estimate" is the observed proportion of successes or failures. Anything else cannot qualify as a "best estimate." For example, the various attempts that

have been made to avoid the dilemma created by obtaining no failures in a test sample include the use of the lower limit of the 50% confidence level as the "best estimate." This value cannot qualify as a "best estimate" since:

(1) The lower limit of a confidence interval can rarely be an unbiased estimate of the "true value" the interval is expected to encompass; (2) any lower confidence limit which equals or exceeds 50% has a larger variance than the observed value.

In summary, then, the *observed* sample average (or proportion) is the only value around which a confidence interval should be placed.

### CALCULATION FOR COMPONENTS

# A. For tests of increased severity

Calculate the limits of the confidence interval for  $X_2$  as follows (ref. 3):

$$\overline{X}_2 + ts_2$$
 $\sqrt{n_2}$ 

Where:

2.

X<sub>2</sub> = Average stress of the failure distribution, or the stress at the 50 percent point on the failure rate curve generated by a test of increased severity.

t = Coefficient by which the standard deviation is multiplied to control the confidence level.

s<sub>2</sub> = Standard deviation of the failure rate curve (generated by a test of increased severity) in terms of the stress.

 $n_2$  = Sample size used to obtained  $\overline{X}_2$ .

These adjusted values of  $X_2$  are then substituted for  $X_2$  in the above formula for reliability from tests of increased severity and the reliability recalculated for both limits. These recalculated values can be taken as the upper and lower limits of the confidence interval for the average (point estimate) reliability-in-use.

# 3. Life tests

When the length of time  $(t_i)$  is observed for each failure and the test terminated at the exact time  $(t_a)$  of the last failure.

$$e^{\text{-}Ut/2am}\!\leqslant R\!\leqslant\! e^{\text{-}Lt/2am}$$

Where:

R = True Reliability

e = 2.7183

U \* Upper percentage point of the chi-square distribution obtained from Appendix 3c for half alpha and 2a degress of freedom.

- L = Lower percentage point of the chi-square distribution obtained from Appendix 3c for one minus half alpha and 2a degrees of freedom
- t = Required failure-free time.

$$m = \underbrace{t_1 + t_2 + t_3 + \dots + t_a + (n-a)t_a}_{a}$$

- n = Number of components tested.
  - C. Attribute-type data

# a. Binomial distribution:

The following technique is applicable when each test specimen can fail in only one way and when any one of these conditions pertain (page 120 ref. 21):

- (1) The lot or population represented by the sample is very large or infinite.
- (2) The sampe size is less than 10% of the lot size.
- (3) Sampling is done with replacement.

Lower Limit (page 373 ref. 23):

$$p_1 = \frac{a}{a + (n-a+1) F_1}$$

Where:

- p<sub>1</sub> = Lower limit of the confidence interval for defects or failures. One minus this proportion is the upper limit of the confidence interval for successes.
- a = Number of defects or failures.
- n = Sample size or the total number of trials.
- F<sub>1</sub> = Upper percentage point from a table of the F-distribution.

Enter the F-table in Appendix 3E with the following values:

$$V_1 = 2 (n-a+1)$$

Upper Limit:

$$P_2 = \frac{(z+1) F_2}{(n-1) + (a+1) F_2}$$

Where:

P<sub>2</sub> = Upper limit of the confidence interval for defects or failures. One minus this proportion is the lower limit of the confidence interval for successes.

a = Number of defects or failures.

n = Sample size or total number of trials.

 $F_2$  = Upper percentage point from a table of the F-distribution.

Enter the F-table in Appendix 3E with the following values:

$$V_1 = 2(a+1)$$

$$V_2 = 2 (n-a)$$

These limits can also be obtained directly from the tables in Appendix 3B.

b. Hypergeometric distribution:

This distribution is applicable when each test specimen can fail in only one way and when all of the following conditions pertain (page 120 ref. 21):

- (1) The lot size is small (finite) but can be considered the population and not a random sample of a much larger volume of material.
  - (2) Sampling is done without replacement.
  - (3) The sample size exceeds 10 percent of the lot size.

The usual formula for the hypergeometric distribution calculates the probability that a given sample will contain exactly "x" defectives. This calculation is based on the size of the lot (population) when the lot fraction defective is known. However, the converse of this is usually required. Thus, knowing the observed fraction defective in the sample, the upper confidence bound of the fraction defective of the lot is required. Tables based on the hypergeometric distribution have been prepared from which the desired information can be obtained directly (see Appendix 3H). In addition, the upper confidence bound of the fraction defective of a finite lot can be estimated by multiplying the upper confidence bound of the fraction defective of an infinite lot by the following factor:

$$\sqrt{\frac{N-n}{N-1}}$$

(see page 121 ref. 21)

#### Where:

N = The lot size.

n = The sample size required to calculate a given upper confidence bound of the fraction defective in an infinite lot, using the binomial distribution.

Care should be taken in the use of the hypergeometric distribution. The upper confidence limit of the fraction defective of a finite lot is less than that for an infinite population when each is predicted from equivalent or identical samples. This comparison is shown in the following table for samples containing no defectives and for the 90 percent one-sided confidence level:

Sample	Lot	Proportion De	efective
Size	<u>Size</u>	Hypergeometric*	Binomial**
2	40	.675	.684
4		.400	.438
8		.225	.250
16		.100	.134
32		.025	.070
5	100	.36	.369
10	e de la companya de l	.19	.206
20		.09	.109
40		.04	.056
- 80		.01	.028
10	200	.20	.206
20		.10	.109
40		.05	.056
80		.02	.028
160		.005	.014

<sup>\*</sup> Finite lot size taken as the population.

<sup>\*\*</sup>Infinite population.

The hypergeometric distribution is useful in acceptance testing where decisions must be made about specific lots of finite size. However, it should not be used in the development stockpile phases of a missile life cycle. In the development phase, decisions must be made about lots of indefinite size. In the stockpile phase, decisions cannot be limited to the small quantity in storage; at this stage of the life cycle, there is interest, also, in what the small stored quantity represents. That is, small quantities are placed in the stockpile to further the state of the art, not to win a war. For this purpose decisions must be made about the larger indefinite quantities represented by the stockpile. Predictions in this case require the use of the binomial rather than the hypergeometric distribution.

## CALCULATION FOR SYSTEMS

# A. Poisson Distribution

When each test specimen (such as a system) can fail in more than one way (ref. 14):

Where:

3.

R = True reliability under the test condition, as the probability of zero failures.

e = -2.7183

U = Upper confidence limit of "c" (the counted number of failures) obtained from Appendix 3D.

L = Lower confidence limit of "c" (the counted number of failures) obtained from Appendix 3D.

n = Number of test specimens (systems) used.

#### B. Other methods

When the system reliability is calculated from component reliabilities, the lower bound of the confidence interval can be obtained by either of two methods recently developed at Picatinny Arsenal: One based on the propagation of errors method to calculate the variance (ref. 16) and one based on the Monte Carlo method of sampling (ref. 17). Both of these procedures are lengthy and involved. An electronic computer may be needed to make the calculations required by either of these methods.

However, before calculating a confidence limit for a system reliability the following should be considered:

a. Confidence limits based on biased estimates are also biased. The confidence level associated with such limits is not valid. Reliability values obtained under conditions that produce less than 50% failures are biased estimates of the true or ultimate reliability.

- b. The magnitude of the differences between the nominal values (point estimate) of high reliabilities and the lower confidence limits based on their variances is always very small and of little practical importance.
- c. If the lower confidence limit of a system reliability is to be determined, the method given above for the binomial distribution for components can be used. In this case the number of failures (a) equals n (1-R) where (R) is the system sample reliability and (n) is the average sample size which equals the sum of the component sample sizes used to determine (R) divided by the number of component types (or kinds) that comprise the system. This procedure is quick and easy to calculate and is sufficiently accurate for most purposes.
- d. Because of the efficiency of testing entire systems as a unit, pointed out above (Section VIII Systems Reliability), every effort should be made to test in this manner. This procedure also avoids the difficult problem of calculating the lower confidence limit of a system reliability derived from component reliabilities. Since the system is the experimental unit (or test specimen) in this case, the confidence limits can be easily calculated by either of the following methods given above:
  - (1) The binomial distribution when the system can fail in only one way.
  - (2) The Poisson distribution when the system can fail in more than one way.

The one exception to the rule of testing systems as a unit is in the development phase where a prediction procedure is required.

1.

## SAMPLE SIZE

### INTRODUCTION

Because of economic considerations, the question of how many specimens to test (or how large a sample size to use) is always given a prominent part in planning any testing program. It is the question most often asked by engineers concerning testing programs. To answer this question from only the economic point of view is not enough. The cheapest testing program is none at all! Of course, if no testing is done there is no verification that the newly developed item is useable and no information concerning the condition of a stored item.

Before the question of sample size can be answered, the following related points must be taken into consideration:

- A. The notion that reliability is related to the number of specimens tested must be discarded. Only the *precision* with which the reliability is determined is related to the sample size.
- B. There is no one single sample size that is applicable to all reliability testing programs. Each program must be considered individually.
- C. A valid sample size cannot be stated without first knowing the *purpose* of the testing program. It is very easy to get the right answer to the wrong problem.

The purpose of planning the sample size prior to data collection is to obtain essential information with minimum cost, effort, and material, essential information being defined as the minimum information required such that additional data will not change the conclusions. To accomplish this the following design of experiment techniques must be considered, since the question of sample size cannot be answered out of this context:

# 2. DESIGN OF EXPERIMENT TECHNIQUES IN SAMPLE SIZE DETERMINATION

### A. Purpose and Objectives:

The purpose of any testing program is to verify the hypothesis that objectives (including requirements) have been achieved or maintained. To do so in any valid quantitative way, the characteristics of the sampling and testing procedures must be adequate, and to do so with the minimum sample size, these procedures must be highly efficient. By efficient is meant maximum precision with minimum sample size.

# B. Precision of Sampling Procedures

In all practical testing programs, especially those in which the testing is destructive, something less than all of the existing items should be tested and from this an inference made about the remaining (usually larger) portion of items. To have these inferences valid the sample must "represent" the remaining portion of the lot or population. If the lot is homogeneous, a representative

sample can be obtained by random selection. That is, each individual item in the lot must have equal change of being selected. If the lot is not homogenous but stratified in some manner according to geographical location, weapon, or manufacturing process, then the sampling plan must be designed to cope with this characteristic of the lot. If the strata are only few in number, then an equal number of randomly selected specimens should be selected from each stratum. The number selected should be apportioned according to the size or importance of each stratum. If the number of strata is large, then specimens should be taken from only a part of the strata. If all strata are equivalent, then a sample of the total number of strata should be randomly selected before the specimens within them are randomly selected. If all of the strata are not equivalent, then the most important or largest strata should be used. In any case, the actual selection of strata or specimens must be done in a random manner either by physical mixing and selection, or by numbering and determining which numbers to select by means of a table of random numbers.

It is important that the sample be stratified correctly to parallel that of the lot. It is only in this way that the heterogeneity of the sample can be kept to a minimum. Any increase in the heterogeneity of the material due to sampling, results in an inflation of the overall variation as measured by the standard deviation of the testing method. As shown below, the magnitude of the standard deviation is of prime importance in calculating sample size.

### C. Precision of Testing Method'

The testing method is in reality a measuring system or device. It "measures" the characteristic of the item being used as a basis for evaluation and decision. As any measuring device, the testing method must be precise and accurate. By precise is meant that characteristic of the method that produces estimates (numerical results) from repeated trials that are close together when in fact there has been little or no variation in the system. Methods which produce estimates close together and do not reflect variations that actually occur in the system are called insensitive rather than precise methods. Obviously this type of method is to be avoided.

It is important to have available the most precise methods possible, since, as can be seen below from the formulas, the sample size varies directly as the square of the standard deviation. The only way precise methods can be made available is via a continuous program of methods development.

#### D. Decision Errors

Because all testing is done on a sample basis, decisions (inferences) must be made about the lot based on the information gained from the sample. This in reality is a form of prediction. We all know that predictions cannot be made with certainty. However, there are only two kit as of error that can be committed in drawing inferences about the lot:

- a. Type I error is rejecting good material.
- b. Type II error is accepting poor material. It is desirable to keep both of these errors small. Their magnitude can be controlled by the number of specimens (sample size) tested in any given situation, as shown below. In practice, the magnitude of these errors chosen is based on the consequences of being wrong. (For example, the consequences of rejecting good material (Type I error) can cost only dollars that the consequences of rejecting good material (Type I error) can cost lives and lose wars.) Then, the sample size required to maintain both errors of the selected levels is calculated.

# E. The Difference that Must be Detected

In a testing program of any kind a decision must be made about at least one of the following requirements before anything can be said about sample size:

- a. The maximum confidence interval that can be tolerated for the particular purpose intended.
- b. The minimum difference (between two values) necessary to be detected for the purpose intended.

These requirements can be established only through knowledge of the objectives and purposes of the system under consideration. Fortunately, this kind of information is usually well known to the engineer. Sample size varies inversely as the square of the difference to be detected. The sample size required to detect a difference of (d/2) is four times that required to detect a difference of (d).

### F. Experimental Design

#### a. Multi-variable Experiments

If effect of more than one variable (such as effect of more than one environment) must be determined, experimental design is extremely important in keeping sample size to a minimum. (By experimental design is meant the pattern or combination of the variables used to collect data.) If these combinations are correctly chosen, efficiency of the experiment can be greatly enhanced. In fact, the efficiency is improved by a factor equal to the number of variables included in the design. For example, to obtain a given precision, a factorial design for three variables requires only one-third the number of test specimens required by the classical one-at-a-time procedure. Factorial design for seven variables requires only one-seventh the number of test specimens required by the classical one-at-a-time procedure. (A factorial design is an experimental one in which all possible combinations of the variable levels are included in the experiment.) At least one test specimen is required for each combination used. When this number becomes large, only a part of the total number of combinations need be used in designs called fractional factorial designs. These fractional designs have the same high efficiency as the full factorial designs. These designs should be used to screen all of the variables of interest to find the most important ones - such as the most severe environment.

### b. Test of Increased Severity

Because of the exploratory nature of this test, an overall sample size cannot be precisely predetermined. The number of test specimens required to obtain the first failure depends upon the magnitude of the existing safety margin and the magnitude of the increments of stress used. After the first failure is obtained, the effective sample size is equal to only one-half the total number of test specimens used in the Bruceton up-and-down and the Two-Stimuli methods. However, these methods are highly efficient. That is, high reliabilities (if they exist) can be demonstrated with small sample sizes. For example, a reliability of .995 at the 90% (one-sided) confidence level can be demonstrated with 40 to 50 items with these methods. Higher reliabilities would require no larger sample size. In addition, these methods make it possible to calculate the reliability under the use condition.

Without these methods the above reliability would require at least 500 items tested without a failure. The reliability demonstrated in this manner would be under the test condition only. It would not be possible to calculate the reliability under the use condition. To demonstrate higher reliabilities (if they exist) would require larger sample sizes.

#### c. Life Test

When time is the variable instead of the environment, as in storage during Stockpile programs, the Poisson distribution is applicable. In this case, the sample size required to demonstrate a given reliability is directly proportional to the ratio of the required shelf life to the length of storage at the time of testing. If this length of storage is short compared to the expected shelf life, very large sample sizes with very few failures are required to demonstrate a reliability above 0.90.

### G. Confidence Intervals

A confidence *interval* is defined as that interval around a sample value (such as the average) in which we expect the true (population) value estimated by the sample to lie. The confidence *level* is a probability statement expressing the proportion of the time the true value can be expected to be within the stated interval. The confidence level is the complement of the Type I error. That is, one minus alpha equals the confidence level. Where alpha is the probability of being wrong (in error), the confidence level is the probability of being right in our predictions. These probabilities can be measured by the area under a frequency distribution curve, such as the normal curve. As a consequence, there are two ways in which an area equal to alpha can be cut off.

- a. By cutting off an area equal to alpha all in one tail of the curve.
- b. By cutting off an area equal to one half of alpha in both tails of the curve.

Either way, the confidence level is the same for a given alpha value. To distinguish between these two ways the first is called a "one-sided" or "one-tail" level, and the second way is called a "two-sided" or "two-tail" level.

The one-and two-sided confidence levels have distinctly different uses:

- a. If there is interest in only one confidence limit, the one-sided level should be used.
- b. If there is interest in both confidence limits, the two-sided level should be used.

The decision concerning which type of confidence level and what magnitude of confidence level to use in any given situation must be made *prior* to obtaining the data. The type of level must be based on the need for one- or two-limit intervals, and the magnitude of level must be based on the consequences of being wrong. To make these decisions after seeing the data affects the value of the confidence level associated with a given confidence interval. Probability statements derived from a set of data are not applicable to that set of data. The fact that one-sided confidence levels for reliability are higher than two-sided levels is not a valid reason for choosing one-sided confidence levels.

With these considerations in mind, the sample size required for a given confidence interval can be calculated as shown below. Conversely, for a given sample size, the magnitude of the associated confidence interval can be calculated. However, for variable type data the standard deviation must be known.

### H. Testing Hypotheses

Tests of hypotheses are used to compare two or more values, such as reliability values. The purpose of tests of this kind is to determine whether observed differences are due to chance variations or whether they are due to assignable causes. This is important in decision making. To decide that the reliability value obtained during the second testing period is smaller than that obtained during the first testing period is very disconcerting if the value obtained in the third testing period is larger than the first reliability value obtained. This is especially disturbing if the decision has led to more testing or replacement of parts, but this is exactly what can happen if the observed differences are due to chance variations. Only through use of statistical tests of significance can this difficulty be avoided.

In hypotheses testing both the alpha (Type I) error and the beta (Type II) error should be controlled to prevent difficulties of the kind described above. The beta error is especially important in Ordnance work because of the consequences of being wrong. The only way that these errors can be controlled at predetermined values is to calculate the sample size required to do so in advance of data collection. Experience has shown that when these two kinds of errors are kept at 5% or below, the risk of making a wrong decision is sufficiently low for most purposes. To reduce these errors below 1% requires very large sample sizes.

### I. Other Considerations

For lots made up of discrete items from which only attribute (success or failure) data can be optained the following additional considerations should be made:

# a. Lot Size vs Sample Size

If the lot is finite in size and less than ten times the size of the sample selected then this fact must be taken into account. The action taken in this regard depends upon the purpose of the testing and the scope of the conclusions drawn as described below.

#### b. Disposition of Selected Specimens

If the testing done destroys the specimens selected or if the specimens are not returned to the lot for any other reason, this fact must be taken into account. Again the action taken in this regard depends upon the purpose of the testing and the scope of the conclusions drawn as described below.

#### c. Purpose of Testing

A decision should be made prior to data collection concerning the purpose of the testing. If the purpose is to draw a conclusion about only those items in a small (finite) lot

and if both of the two above conditions pertain, then the sample size can be reduced slightly through use of the hypergeometric distribution. This distribution finds its most frequent use in acceptance testing where the purpose is to predict the expected fraction infective of a particular small lot of items. If such a lot is placed in stockpile, however, then the hypergeometric assumption is no longer applicable since the purpose of testing is now different. Small lots of material in the stockpile represent larger lots of indefinite size. The characteristics of the invaterial are studied and recorded for their value in future applications. That is, the purpose of testing is to draw inferences about the larger volume of material represented by the small lot on hand. In this latter case, only the binomial assumption concerning lots of infinite size is applicable.

3.

# **CALCULATION**

- A. Sample size required for a given confidence interval
  - a. Variable data

$$n = \frac{(ts)^2}{4^2}$$

Where:

n = Sample size

t = Standard deviate associated with the alpha error used to control the confidence level.

s = Sample standard deviation.

d = Magnitude of the confidence interval in the same units as the standard deviation.

b. Attribute Data

(1) Binomial Distribution

There is no easy, practical way accurately to calculate the sample size required for attribute data. The accurate methods are difficult to calculate and the simple, easy methods are not accurate. The most practical method is to refer to one of the existing tables for binomial confidence intervals to find the sample size required for a given interval. Tables useful for this purpose are:

One-Sided Limits:

Appendix 3B

Two-Sided Limits:

Appendix 3B

# (2) Hypergeometric Distribution

As with the binomial distribution, there is no easy, direct way to calculate the sample size for the hypergeometric distribution. The most practical way to arrive at a sample size in this case is to refer to one of the existing tables for the hypergeometric confidence intervals. From these tables the sample size for a given interval and confidence level can be read directly. Tables useful for this purpose can be found in Appendix 3H.

Alternatively, the sample size required in a hypergeometric distribution can be estimated by multiplying the sample size for the binomial distribution by N/(N+n)

Where:

N = Lot size

n = Sample size required in the binomial distribution.

B. The sample size required to detect a given difference between two sample values in testing a hypothesis:

a. Variable Data

$$n=2 \left[ \frac{(t_1+t_2)}{d} \right] 2$$

Where:

n = Sample size

t<sub>1</sub> = Standard deviate associated with the alpha error

t<sub>2</sub> = Standard deviate associated with the beta error.

s = Sample standard deviation

d = Difference that must be detected.

b. Attribute Data

As mentioned above there is no easy practical way to calculate the sample size for attribute data. The sample size for hypothesis testing using attribute data can best be determined from the tables for minimum contrasts in Appendix 3A. These tables give values in the following format:

# Minimum Contrasts Required for Significance at the 95% Level

<u>N</u>	No. of A's in	sample (1)/	No. of A's in	Sample (2)
4	0/4	1/-		1
5	0/4	1/5	2/-	
10	0/5	1/7	2/8	3/9, etc.
20	0/5	1/7	2/9	3/10, etc.

In this table N is the sample size. The values in the body of the table that appear to be proportions are written in a short-hand method which mean the following:

For a sample size of 5, the value in the first column of this row (0/4) means that if no failures are obtained in the first sample of 5, at least 4 failures must occur in the second sample of 5 before the observed difference can be declared significant at the 95% level of confidence. This, in turn, means that a sample size of 5 can only detect differences of 80% or greater. Larger sample sizes can detect smaller proportional differences. The use of these tables can, of course, be reversed to find the sample size required to detect a given difference.

C. Sample size required in storage programs where time is the variable:

$$N = \frac{a}{1 - R}$$

Where:

N = Sample size

a = Number of failures in time (h)

h = Length of storage

R = Required reliability

1.

#### INTRODUCTION

It is assumed in these methods that the test item can fail in but one way. That is, the binomial distribution is applicable.

Plans should be made to conduct the laboratory experiments in two stages:

- A. Survey the separate effects of the several environmental conditions of interest in one integrated factorial experiment to select the environments causing the highest failure rates.
- B. Determine the ultimate reliability by means of a test of increased severity (testing to failure) using the treatment (environment) found most severe in the factorial experiment.

# 2. FACTORIAL DESIGNS

# A. Advantages

The two-to-the-n<sup>th</sup> factorial designs or their optimized modifications are the most efficient experimental methods known for selecting the treatments causing the highest failure rates. This approach will reduce the magnitude and complexity of the experiments required to determine reliability. More important, all component reliabilities obtained in this manner will have a common basis of determination because the reliability of each component is defined in terms of the environment which has been experimentally found to cause the highest failure rate. This results in predicting the minimum reliability with respect to the separate environments for each component. If all these reliabilities are acceptable the reliabilities associated with all the other environments will also be acceptable. Only in this way can valid and realistic system reliabilities be derived from component reliabilities.

See Appendix 4 for some of the more useful two-to-the-n<sup>th</sup> factorial designs in the form of worksheets. These designs are the most efficient known. Experiments based on these designs may be conducted without changing the treatment procedure except to arrange for the test specimens to receive the number and kind of treatments required by the particular design used. However, the best differentiation among treatments is obtained when the level of severity used will cause 50 percent of the test specimens to fail. This may cause some adjustment of the levels of the treatments used.

For the purpose of this application, the two levels of each treatment can be the *presence* and *absence* of the treatment. Alternatively, any two levels of the treatment can be used.

The number of test specimens required in the optimized designs is one more than the total number of treatments used (ref. 5). The more versatile fractional factorial designs (ref. 6) require at least 16 items for experiments containing from five through eight treatments, and at least 32 items for nine through 13 treatments. With twice these numbers of items, the latter type designs can also measure interactions, i.e., how the effect of any one environment depends upon the others. Interactions among treatments cannot be measured except by factorially designed experiments.

Factorial designs permit a type of statistical analysis that distinguishes between variations due to chance and variations having assignable causes, thereby producing more information from a given number of items than any other known procedure. These designs actually increase the effective sample size by making it possible to use each observation (or measurement) for more than one purpose.

In fact, each treatment effect is determined as though the entire experiment is conducted to determine that particular treatment effect alone. As a result, each treatment effect is determined with a precision equal to the total number of items used in the experiment. The three-treatment-design example described below demonstrates this point.

Further advantages in using factorial designs in environmental testing experiments follows:

- a. No control groups are required.
- b. Each treatment effect can be determined independently of all others. Thus, unambiguous conclusions can be drawn about each treatment effect.
- c. Complex experiments involving a large number of treatments can be easily handled with factorial procedures.
- d. This is the *only* experimental design in which the relationship among the treatments can be measured. The factorial design can determine whether the effect of one environmental treatment depends upon *any* of the others. These effects are called interactions.
  - e. The probability of being right to wrong can be controlled.
- f. When the number of treatments used becomes large (three or more), only a fraction (1/2, 1/4, 1/8, etc.) of the total number of combinations in a factorial design need be used.

When multiple replications cannot be used and only attribute (go, no-go) data are available, these designs can still be used to take advantage of their efficiency. However, in cases of this kind the usual analysis of variance cannot be made. Instead, the usual summations are made to obtain and compare two binomial proportions (by the Fisher exact method) to determine the effect of each treatment. See example No. 1 below.

Results of factorial experiments are used as a guide to select which environment to use for determining reliability prior to conducting the test of increased severity. The factorial experiment surveys all of the environmental treatments of interest (with a minimum number of test specimens) to determine the difference, if any, among the environmental effects. A decision is then

made whether to redesign the item. If the item is considered acceptable at this time, reliability is determined using the environmental treatment or treatments found to be most severe. If no differences are found among the effects, reliability can be determined by using a combination of several of the treatments considered most important from an engineering point of view. If reliability is determined by using the most severe treatments, the reliability values obtained will be lower than those obtained with the other treatments. This is a necessary condition if the system's reliability derived from the component's reliabilities is to be useful.

# B. Full factorial designs (ref. 18).

These designs require more specimens per treatment than do the fractional factorial designs, but they are the only class of designs that can measure all of the interaction effects. A full factorial can be formed by writing down all of the combinations of "n" treatments, each at two levels in a multi-entry table. For example, a full two-cubed factorial can be written as follows:

# 23 FACTORIAL DESIGN

The lower case letters and the symbol (1) in the body of the table identify each of the eight (2<sup>3</sup> = 8) treatment combinations that constitute this design. These combinations are derived from their position in the table. For example, the symbol (1) is located by A1 B1 C1 which means that all three treatments are at their lower level. The lower case letters (ac) are located by A2 B1 C2 which means that treatments A and C are at their higher levels and that treatment B is at its lower level. In this code the lower case of the treatment letter appears in the combination only when the treatment is at its higher level. This results in the formation of all possible combinations of "n" things (treatments) taken 0, 1, 2, ... and n at a time. At least one test specimen or observation is required for each of the treatment combinations. Two or more observations at each treatment combination are required for an independent estimate of experimental error. An equal number of observations at each treatment combination is required to keep the design orthogonal.

### C. Fractional factorials (ref. 6)

As the number of treatment variables increases, the number of treatment combinations, and therefore the number of test specimens required for a complete replication, increases very rapidly. At the same time the number of higher order interactions that can be measured also increases very rapidly. This results in two undesirable situations:

- a. The number of test specimens required is too large.
- b. The information in the higher order interactions (three-factor interactions and above) is of little practical use. Fractional factorial designs were developed to avoid these situations and thereby improve the efficiency of designs for multi-factor experiments.

When less than all of the possible combinations in a factorial design are used, the design is said to be a fractional factorial. For the two-to-the-nth series there can be half, quarter, eighth, sixteenth, etc. portions of the full factorial used. These portions are called fractional replicates, where a full factorial is one replicate.

Fractional factorials cannot be used without losing or giving up some information that is available in the full factorial. However, it is planned in designing a fractional factorial to lose only the least important part of the information. Experience has shown that the higher order interactions in a full factorial are the least important. This fact is made use of by equating new treatments to the higher order interactions. To equate one such interaction to a new variable in a full 26 factorial, for example, creates a half replicate of a 27 factorial. Detailed procedure for designing fractional factorials can be found in reference 18. At least one observation for each treatment combination is required to keep these designs orthogonal.

# D. Treatment procedure

The factorial designs described in Appendix 4 are those most frequently used in environmental experiments. They are described in the form of treatment procedure worksheets to facilitate their use. These worksheets show, in an easy-to-follow manner, how to treat each test specimen in the various fractional factorial designs represented. They can also be used to record and analyze the test results. A blank space in the item column means that the item does not receive the corresponding treatment. A plus mark in the item column means that the item receives the corresponding treatment. The combinations of blank spaces and plus marks in the worksheets correspond to the treatment combinations in the respective fractional factorial designs. The choice of these designs should be based on the following considerations:

- a. The number of treatment effects that must be determined.
- b. Whether interactions can be expected to be present.
- c. The precision required.
- d. The number of test specimens available or that can be made available.

These considerations should be made in the order named.

The blocks in which some of the designs are divided are for the primary purpose of breaking the experiment into homogeneous parts with respect to testing equipment used, operators conducting the experiment, or climatic conditions, such as season of the year, etc. If all such things can be considered constant, then these blocks can be identified with other conditions whose effect it is desired to evaluate, such as, firing conditions, functioning conditions, temperature conditions or different lots of material. Identifying the blocks with different conditions or material does not affect the determination of the treatment effects. The important consideration is that conditions be held constant and materials be homogeneous within the block.

# E. Analysis

An example of one type of analysis that can be used with factorial designs is given in Appendix 1. This is the simplest possible analysis. The type of analysis that can be made depends upon the class of design used, the kind (attribute or variable) and amount (number of replications) of data, and the way (at random or in blocks) data were collected. Some types of analysis, such as the analysis of variance, are quite complicated. As a result, the subject of the analysis of variance (ref. 18) is not included here. It is recommended that statistical analysis of this kind be conducted by statisticians.

#### TESTS OF INCREASED SEVERITY

#### A. Introduction

These methods need be used only when one of the following situations pertains:

- a. The occurrence of a failure cannot be detected by visual inspection at the time of occurrence, as it is in a tensile test.
- b. The magnitude of the stress at the time of failure is not observable, as it is in the tensile test.

The intended use of these methods is to determine the magnitude of the stress at the point of failure (where the stress equals the strength), when this value is not directly observable, as in the case of the effect of vibration on timing accuracy.

The level of severity can be increased in a variety of ways, such as the following:

- a. Using more extreme levels of treatment (e.g., higher or lower temperatures, higher or lower G-values, or higher or lower voltages).
  - b. Applying two or more treatments simultaneously.
  - c. Increasing the length of time the treatment is applied, as in storage tests.

When variable (quantitative) data (such as resistance in ohms, elongation in percent or closing time in seconds) are obtained, it is necessary to compare each observed value with the required value in order to determine success or failure.

#### B. Bruceton up-and-down method (ref. 3)

Starting with the most severe condition expected in use, test one new, unused item. If the item does not fail, increase the level of severity (the stress) one increment\* and again test one

<sup>\*</sup>This value can be estimated by didiving the difference between the maximum, and minimum in-use conditions by six. This is based on the assumption that the extreme in-use conditions are the 3-sigma limits.

new, unused item. Continue this process of increasing the stress one increment at a time and testing one new, unused item at each increment of stress until the first failure is obtained. Then reverse the process by decreasing the stress one increment at a time and testing one new, unused item at each increment of stress until a success is obtained. Repeat the process of increasing the stress to failure and decreasing the stress to success until at least 25 test specimens are used after the first failure. Calculate the level of severity at which 50% of the specimens fail, and the associated standard deviation by the method described in Chapter 19 of ref. 3, using the number of failures for these calculations.

With this information the "reliability-in-use" can be predicted. See the examples in Appendix 1 for details of the calculations.

When the form of the distribution curve is not known or is in doubt, Chebyshev's inequality can be used. This technique is valid for any distribution without an assumption concerning its form. The inequality states that the amount of area under any distribution curve which is farther away from the mean than k standard deviation units is less than 1/k<sup>2</sup>. The reliability calculated by this procedure will always be less than the true value.

When the form of the failure distribution curve is practically normal, as shown by its cumulative frequency approximating a straight line on linear probability paper, probability values can be found by entering a table of areas under a standard normal curve with calculated normal deviates, which equals the difference between any two levels of severity divided by the standard deviations.

# C. Churchman two-stimuli method (ref. 10)

Test one new, unused item at the most severe condition in use. If the item does not fail, increase the level of severity (the stress) one increment\* and, again, test one new, unused item. Continue this process of increasing the stress one increment at a time and testing one new, unused item at each increment of stress until the first failure is obtained. This procedure should cause the first failure within 5 to 10 trials, depending on the magnitude of the safety margin. Using the level of severity causing the first failure, test 10 to 20 items to determine the proportion of failures at this point. Record this proportion and the level of severity used. Then change the stress by an amount equal to about two or three increments. If the first proportion of failures exceeds 50 percent, decrease the stress, and if the first proportion is less than 50 percent, increase the stress to find a second point on the curve. Determine the proportion of failures at this point as before and record this proportion and the level of severity used.

The object is to find two levels of severity such that the proportion of failures differ by at least 20 percent, and yet have the proportions more than zero percent and less than 100 percent. From this information calculate the average and standard deviation of the failure rate by the method described in Reference No. 10. Alternatively, the average and standard deviations can be obtained graphically by plotting the proportion of failures against the corresponding stress level on linear probability paper. Draw a straight line through the two points. The average stress is that stress corresponding to 50 percent failures. The standard deviation is equal to the difference

<sup>\*</sup>One sixth of the difference between the expected maximum and minimum use conditions.

between the stress at the 16 percent point, and the stress at the 50 percent point. By using these values, the reliability-in-use can be calculated as described in Appendix 1.

### D. Discussion of methods.

Which of these methods will be suitable for use in any particular situation depends upon the intended purpose of the experiment. The choice can be based upon the distinguishing characteristics. Both methods are equally efficient, as they both require the same sample size for a given precision.

The two-stimuli method should be used when either of the following physical conditions exists:

- a. The test results are not immediately available after each trial. This would cause undue delay in conducting the Bruceton method which requires that all trail results be known before the condition for the next trial can be determined.
- b. The physical changing of the test conditions is difficult. This would cause undue work in conducting the Bruceton method which requires changing the test condition after each trial.

### E. Method characteristics

### a. Bruceton method

(1) Advantage:

This method leads directly to the 50 percent point with the greatest efficiency.

- (2) Disadvantages:
  - (a) The standard deviation should be known in advance.
- (b) Tests must be conducted in sequence, as the results of each test must be known before the next is conducted.
  - (c) Test conditions must be changed after each trial.

# b. Two-stimuli method.

- (1) Advantages:
  - (a) A number of trials can be conducted concurrently.
  - (b) Only two points on the curve are required.
- (c) This method can be extended so that more than two points are determined. If this is done the form of the distribution can be determined.

# (2) Disadvantages:

two points.

- (a) The form of the strength distribution curve cannot be determined with only
- (b) The assumption of normality is required when only two points are used.

# X APPENDICES

# APPENDIX I

# **EXAMPLES**

# A. Confidence Intervals

a. <u>Life tests.</u> A sample of 20 components (n) hich are required to operate for 240 hours (t), were subjected to a specified use condition for a period of 120 hrs. when the first component failed. The failure rate was assumed to be relatively constant and so the test was discontinued at this point in time (120 hrs.).

The sample point estimate for reliability can be caluclated as follows:

$$\hat{R} = e^{-t/m}$$

When: e = 2.7183

$$m = \frac{1 \times 120 + (20-1)120}{1} = \frac{2400}{1}$$

t = 240 hours.

$$\hat{R} = (2.7183)^{-240/2400} = .90$$

This is the point estimate of the probability of no failures in 240 hours. The 90 percent two sided confidence interval for R can be calculated as follows:

$$e^{-Ut/2am} \leq R > e^{-Lt/2am}$$

When:

e = 2.7183

U = 5.99 (from Appendix 3C for half alpha and 2a degrees of freedom)

L = 0.103 (from Appendix 3C for one minus half alpha and 2a degrees of freedom)

a = 1 (the number of failures)

m × 2400

t = 240

alpha = (1-0.9) = 0.1

$$(2.7183)^{-(5.99)} (240)/2 \times 1 (2400) \le R \ge (2.7183)^{-(0.103)} (240)/2 \times 1 (2400)$$

$$(2.7183)^{-0.3} \le R \ge (2.7183)^{-0.005}$$

Confidence interval:

 $0.74 \leqslant R > 0.995$ 

b. <u>Binomial type data.</u> — A sample of 20 items was taken from a lot of 100 components and tested under the use condition. No failures were obtained.

To accept this specific lot the lower limit of the 90 percent one sided confidence limit for the reliability should be taken from the tables in Appendix 3H which are based on the hypergeometric distribution. The value found in these tables is 9 defectives in the original lot of 100 items. From this then the lower limit for the true reliability of the lot is:

R (lower limit) = 
$$1 - 9/100 = 0.91$$

On the assumption that this value is acceptable and the lot is placed in the stockpile for further testing, the reliability of the items that this lot represents should now be determined from the tables in Appendix 3B which are based on the binomial distribution. From these tables, the lower limit of the true reliability of the items the lot represents is:

R (lower limit) = 
$$1.000 - 0.109 = 0.881$$

c. Systems: (1) A group of 10 telemetered missiles were flight tested. The number of failures found in each missile is as follows:

Missile number		Number of failures
1		0
2		, <b>o</b>
3		0
4		• 0
5		0
6		0
7		0
8		3
9	•	0
10		0
	Total	3

The point estimate for reliability as the probability of no failures under the test condiion can be calculated as follows:

$$R = e^{\overline{X}}$$

When: X = 3/10

# Point estimate:

$$R = (2.7183)^{-0.3} = 0.74$$

The 90 percent two sided confidence interval for the true reliability (R) can be calculated s follows:

$$e^{-U/n} \leqslant R \leqslant e^{-L/n}$$

When:

e = 2.7183

U = 7.75 (from Appendix 3D).

L = 0.818 (from Appendix 3D).

n = 10

 $(2.7183)^{-7.75/10} \le R \le (2.7183)^{-0.818/10}$ 

# Confidence Interval:

$$0.46 \leq R \leq 0.92$$

The point estimate and 90 percent two sided confidence interval calculated from the above imple, using the binomial distribution is:

#### Point estimate:

$$R = 1 - 1/10 = 0.90$$

# Lower limit (for defectives):

$$p_1 = \frac{a}{a + (n - a + 1) F_1}$$

When:

a = 1 (number of defective systems)

n = 10 (number of systems)

# Degrees of freedom:

$$V_1 = 2 (10 - 1 + 1) = 20$$

$$V_2 = 2 \times 1 = 2$$

F<sub>1</sub> = 19.4 (from Appendix 3E Table 2B)

$$p_1 = \frac{1}{1 + 10 \times 19.4} = 0.0051$$

# Upper Limit (for defectives)

$$p_2 = \frac{(a+1) F_2}{(n-a) + (a+1) F_2}$$

When:

a = 1 (number of defective systems)

n = 10 (number of systems)

# Degrees of freedom:

$$V_1 = 2(1+1) = 4$$

$$V_2 = 2(10 - 1) = 18$$

F<sub>2</sub> = 2.93 (from Appendix 3E table 2A)

$$p_2 = \frac{2 \times 2.93}{9 + 2 \times 2.93} = 0.396$$

# Confidence interval:

$$1 = (0.396) = 0.604 \leqslant R \leqslant 1 \cdot (0.0051) = 0.9949$$

(2) A system's reliability was calculated from a total of 200 test specimens and found to be R = 0.995. The 95 percent one sided lower confidence limit is:

Upper Limit (for defectives):

$$p_2 = \frac{(a+1) F_2}{(n \cdot a) + (a+1) F_2}$$

When:

 $a = 0.005 \times 200 = 1$  (average number of defectives)

n = 200

Degrees of freedom

$$V_1 = 2(1+1) = 4$$

$$V_2 = 2 (200-1) = 398 \approx \infty$$

F<sub>2</sub> = 2.37 (From Appendix 3E Table 2A)

$$p_2 = \frac{2 \times 2.37}{(200-1) + 2 \times 2.37} = 0.0233$$

Lower confidence limit:

$$R = 0.995 - 0.023 = 0.972$$

#### B. Factorial Experiment

This example demonstrates how factorially designed environmental experiments can be used in combination with tests of increased severity. A simple three-treatment-experiment example is given below. The treatments used in this example are identified and defined as follows:

Identification	Treatment
A	Transportation vibration
В	Flight shock
C	High temperature

For purposes of the factorial design, each treatment is considered to have two levels:

- a. Lower level is the absence of the treatment (designated by subscript 1).
- b. Higher level is the presence of the treatment (designated by subscript 2).

The total number of possible combinations of three treatments, each at two levels, is two cubed or 8. These 8 combinations can be written in the following pattern:

	A <sub>1</sub>	, <u> </u>	12
<u>B<sub>1</sub></u>	<u>B2</u>	<u>B</u> 1	B <sub>2</sub>
C <sub>1</sub> (1)	b	<b>a</b> .	(a + b)
C <sub>2</sub> c	(b + c)	(a + c)	(a+b+c)

A minimum of 8 items would be required for this plan, each receiving different treatment combinations as follows:

Item Number	Treatment combinations
1	None (1)_
2	B only
3	A only
4	A + B
5	C only
6	B + C
7	A + C
8	A + B + C

By using the letters (a, b, and c) and symbol (1) to represent the results obtained from testing the eight items, it can be shown symbolically that the treatment effects can be independently determined, using the total number of items in the entire experiment for each treatment as follows:

### Effect of treatment A

$$a + (a + b) + (a + c) + (a + b + c) -$$

$$[(1) + b + c + (b + c)] = 4A$$

# Effect of treatment B

$$b + (b + c) + (a + b) + (a + b + c) -$$

$$[(1) + c + a + (a + c)] = 4B$$

### Effect of treatment C

$$c + (b + c) + (a + c) + (a + b + c) -$$
  

$$[(1) + b + a + (a + b)] = 4C$$

One-fourth of these differences equals the average effect of the respective treatments. From the above equations it can be seen that the results obtained from the eight items have been used three times — once for each treatment. This procedure produces an effective sample size equal to  $3 \times 8$ , or 24 items. Each treatment effect has been determined independently of the others with a precision equal to the total number of items used in the experiment.

The above three-factor factorial can be used as an example of a fractional factorial design as follows:

		A <sub>1</sub>	A <sub>2</sub>			
	<u>B<sub>1</sub></u>	B <sub>2</sub>	<u>B<sub>1</sub></u>	B <sub>2</sub>		
C <sub>1</sub>	-	<b>b</b>	a	•		
$c_2$	· <b>C</b>	•	•	(a+b+c)		

A minimum of four items is required in this design. As before, the separate effects can be determined by a process of summation and subtraction as follows:

#### Effect of treatment A

$$a + (a + b + c) - (b + c) = 2A$$

# Effect of treatment B

$$b + (a + b + c) - (a + c) = 2B$$

#### Effect of treatment C

$$c + (a + b + c) - (a + b) = 2C$$

One-half of these differences equals the average effect of the respective treatments.

When there is only one item available for each treatment combination, and only success and failure data are available, the usual analysis of variance cannot be used but the remaining advantages of the factorial design (given previously) still pertain. The above differences, which will be binomial proportions in this case, can be compared by the Fisher exact method for 2 x 2 contingency tables (ref. 7) to determine the treatment effects. A very convenient set of tables for this purpose can be found in ref. 8,\* which contains tables of minimum contrasts based on Fisher's exact method.

a. <u>Sample calculations</u>. The full three-factor-experiment used above might give the following typical set of results, when the figure "one" is entered as a "failure" and a "zero" is entered as a "success." It is assumed that a knowledge of the item being tested has led to the decision that transportation vibration, flight shock, and high temperature *in that order*, are the three environmental conditions most likely to affect the important functioning characteristic of this item; this characteristic is waterproofness. The treatment procedure and worksheet (to record results) for this experiment would be the following two-entry table. A plus mark in the item column means that the item received the corresponding treatment, while a "blank" means that the item did not receive the treatment.

	Treatr	nent	proced	ure .				
Order of		•		Item Nu	ımber			
Treatment	14	<u>5-8</u>	9-12	<u>13-16</u>	<u>17-20</u>	21-24	<u>25-28</u>	<u>29-32</u>
Transportation vibration (A)			+	+		r .	+	+ '
Flight shock (B)		+	***	+		+		+
High temperature (C)			÷		+	+	+	+
Results: Replication 1	1	0	0	1	0	0, .	1	1
2	0	0	0	0	0	1	1	1
3	Q	1	0	. 1	0	1	1	1 .,
4	1	1	0	1	0	0	1	1
Totals	. 2	2	0	3	0	2	4	4

The results of one complete replication should be obtained under a single set of controlled conditions (e.g., in the same day, same operators, same instruments, etc.), before going to the next replication. This will make it possible to determine whether conditions changed significantly during the experiment.

<sup>\*&</sup>quot;See also Appendix 3A"

Placing these results in the usual factorial matrix, the following table would be obtained:

1	A <sub>1</sub>		A <sub>2</sub>	
	B <sub>1</sub>	B <sub>2</sub>	<u>B<sub>1</sub></u>	B <sub>2</sub>
C <sub>1</sub>	1 .	0	0	1
	0	0	0	<b>o</b> .
,	, <b>o</b>	1	0	1
	1	1	<u>o</u>	1
	2	2	Ö	3
c <sub>2</sub>	0	0	1	. 1
	0	1	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1
	0	1	. 1	1
	0	0	<u>1</u>	1
	0	2	4	4

In preparation for analyzing these results, the usual summing process would give the following series of two-factor tables:

# Summing over A:

· ·	B <sub>1</sub>	<u>B<sub>2</sub></u>	Row Totals
c <sub>1</sub>	2	5	7
c <sub>2</sub>	4	<u>6</u>	10
Column totals	6 .	11	17

## Summing over B:

	. A <sub>1</sub>	<u>A2</u>	Row Totals
C <sub>1</sub>	4 .	3	7
c <sub>2</sub>	_2_	8	10
Column Totals	6	11	17
Summing	Over C:		•
	A <sub>1</sub>	<u>A2</u>	Row Totals
B <sub>1</sub>	2	4	6
B <sub>2</sub>	4	7	11
Column Totals	6	11	17

Note that approximately 50 percent (17/32) failures were obtained. This is the condition under which the greatest resolution of effects is obtained. Each one of the marginal totals is the sum of 16 observations. The results can now be analyzed and interpreted as follows:

Source		Effects	Test of Significance*
Main Effects			
Transportation vibratio	on (A)	6/16 vs 11/16	Non-significant
Flight shock (B)		6/16 vs 11/16	Non-significant
High temperature (C)		7/16 vs 10/16	Non-significant
Replication	1. 4/8		Non-significant
	2.3/8		
	3. 5/8		
•	4.5/8		

<sup>\*</sup>From Appendix 3A Table 1.

Effects	Test of Significance*
8/16 vs 9/16	Non-significant
5/16 vs 12/16	Significant
8/16 vs 9/16	Non-significant
6/16 vs 11/16	Non-significant
	8/16 vs 9/16 5/16 vs 12/16 8/16 vs 9/16

<sup>\*</sup>From Appendix 3A Table 1.

#### b. Interpretation (when the above order is used)

- (1) The replication effect is not significant. This means that the conditions of the experiment did not change significantly from the beginning to the end. Therefore, the results can be accepted as valid from this standpoint.
- (2) None of the effects is significant except the A x C interaction. This means that the combination of transportation vibration and high temperature treatments has caused a larger difference in the number of failures than would be expected due to chance variations alone.
- (3) None of the treatments taken alone is significant, although the flight shock and transportation vibration effects approach significance. These results suggest the need for additional flight-shock and transportation vibration tests if these treatments are considered important from an engineering point of view.

These results show clearly that the combination of transportation vibration and high temperature is the most severe condition. From this, reliability should be defined in terms of waterproofness after transportation vibration and high temperature. If this reliability is acceptable, the waterproofness reliabilities under all of the other conditions used will also be acceptable.

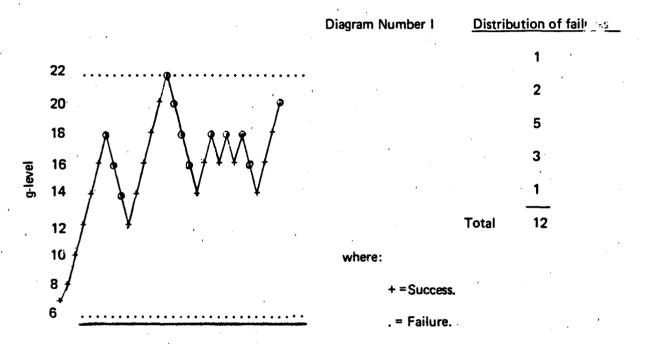
### C. Tests of Increased Severity

a. <u>Bruceton method (ref. 3)</u>. The results from the factorial experiment described above show that the Bruceton "up-and-down" procedure can be conducted by varying the severity (g-force level) of the transportation vibration treatment and using the same high temperature (without variation) as that used in the factorial experiment. This can be done since the high temperature main effect (difference in the number of failures between the presence and absence of this treatment) is not significant. Assuming that the average g-force expected in use is 4 g's with a standard deviation of 2 g's, then using increments of 2 g's and starting at 6 g's, apply the vibration and temperature treatments and conduct the waterproofness test on one new, unused item. If the item does not fail, increase the g-level one increment and again test one new, unused item. Continue this process of increasing the g-level one increment at a time and testing one new, unused item at each g-level until the first failure is obtained. Then reverse the process by decreasing the g-level one increment at a time and testing one new, unused item at each g-level until an item successfully passes the

waterproofness test. Repeat the process of increasing the g-level to failure and decreasing the g-level to success, until at least 12 items have been made to fail in this manner.

Ordinarily the Bruceton method would not be used for this test. Since the result of each test must be known before the next test can be run, this method would consume far too much time. It is used here for demonstration purposes only. In practice the Two-stimuli method should be used for a test of this kind, since several of the tests could be conducted concurrently with a considerable saving of time.

Record the results in graphic form for convenience and count the number of failures obtained at each g-level. The following can be used as an example of the type of observed data that could be obtained:



Calculate the average  $(\overline{X})$  and standard deviation (s) of the failure rate as follows (ref. 3):

Where:

$$A = \sum_{x=0}^{x=k} fx; \qquad B = \sum_{x=0}^{x=k} f(x)^2$$

k = Number of g-levels over which the failures are distributed.

f = Observed frequency of failure.

x = Code numbers used for ease of calculation.

$$X = y^{1} + d (A/N - 1/2)$$

$$S = 1.62 d \left( \frac{NB - A^{2}}{N^{2}} + .029 \right)$$

Where:

y<sup>1</sup> = Lowest level at which a failure is obtained.

d = 2 g's. - the increment used.

N = Total number of failures.

This formula for the standard deviation is an approximation which is quite accurate when exceeds 0.3.  $\frac{(NB - N)}{N}$ 

Using these formulas and the observed data, the average and standard deviation for the above example can be calculated as follows:

<u>f</u>	<u>x</u>	<u>fx</u>	fx <sup>2</sup>
1	4	4	16
2	3	6	18
5	2	10	20
<b>3</b> ′	1	3	3
1	0	0	0
N = 12		A = 23	B = 57

$$\overline{X}_2 = 14 + 2(23/12 - 1/2) = 16.8 \text{ g/s}$$

$$s_2 = 1.62 \times 2$$
  $\left[ \frac{12 \times 57 \cdot (23)}{(12)^2} + 0.029 \right] = 3.58 \text{ g/s}$ 

The cumulative frequency of the observed failure distribution plotted on linear probability paper closely approximates a straight line. From this it can be concluded that the assumption of normality is sufficiently valid for use as a basis to predict the expected reliability-in-use.

Therefore, the point estimate for the (waterproofness) reliability-in-use can be calculated as follows:

Where:

P = The probability of failure-in-use.

The probability of failure-in-use can be measured by the area under the normal curve associated with the Z-value calculated as follows:

$$Z = \frac{(X_1 - X_2) - (M_1 - M_2)}{\sqrt{\sigma_1^2 + \sigma_2^2}}$$

When:  $X_1 \geqslant X_2$  a failure is obtained.

$$Z \geqslant \frac{M_2 \cdot M_1}{\sqrt{\frac{2}{\sigma_1} + \sigma_2^2}}$$

Where:

 $X_1$  = Any stress value.

 $X_2$  = Any strength value.

M<sub>1</sub> = True mean of the stress distribution.

M<sub>2</sub> = True mean of the strength distribution.

 $\sigma_1^2$  True variance of the stress distribution.

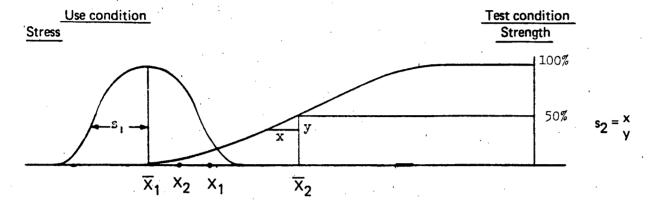
 $\sigma_2^2$  = True variance of the strength distribution.

$$\frac{M_2 \cdot M_1}{M_1} = Safety margin.$$

The relation between the safety margin and a measure of probability is shown above. If the product of the safety margin and the average stress in use is divided by  $\sqrt{\sigma_1^2 + \sigma_2^2}$ , we have a measure of probability — the standard deviate.

Graphically, the relationship between the test conditions and use condition can be depicted as follows:

#### Diagram Number II



Where:

The horizontal axis represents the g-forces increasing to the right. The bell shaped curve represents the distribution of g-forces under the use condition (the stress curve).

The S-shaped curve represents the distribution of failures under the test condition obtained by the Bruceton method (the strength curve).

When:

 $\overline{X_1}$  = 4 g's - an estimate of M<sub>1</sub> the true average stress.

 $s_1 = 2 g's$  - an estimate of  $\sigma_1$  the true standard deviation of the stress.

 $\overline{X_2}$  = 16.8 g's - an estimate of M<sub>1</sub> the true average strength (the 50 percent point on the strength curve.)

 $s_2 = 3.48$  g's - an estimate of  $\sigma_2$ , the true standard deviation of the strength.

X<sub>1</sub> = any stress value.

 $X_2$  = any strength value.

From the above, the average (point estimate) reliability-in-use can be calculated as follows:

$$T \geqslant \frac{\overline{X_2 \cdot X_1}}{\sqrt{x_1 + x_2^2}}$$

$$T > \frac{16.8 - 4.0}{\sqrt{(3.58)^2 + (2)^2}} > 3.12$$

From Appendix 3G the probability of a failure-in-use associated with this T-value is: P<sub>1</sub> < 0.00090.

#### Reliability Point Estimate:

The lower confidence limit for the one sided 95 percent confidence level can be calculated as follows:

The 95 percent single sided lower confidence limit of the average strength:

$$\overline{X}_2$$
  $\xrightarrow{ts_2}$  (see ref. 3)

Where:

 $\overline{X_2}$  = 16.8 - the observed average strength.

t = 1.80 — the t-value associated with the single sided 95 percent confidence level and eleven ( $n_2$ -1) degrees of freedom found in Appendix 3F.

 $s_2 = 3.58$  - the standard deviation of the strength.

 $n_2 = 12$  — the sample size used to determine the strength.

Then the 95 percent single sided lower confidence limit for the strength is:

$$16.8 \cdot \frac{(1.80) (3.58)}{\sqrt{12}} = 14.94$$

The lower bound of the reliability-in-use can be calculated as follows:

$$T_2 \geqslant \frac{14.94 - 4.0}{\sqrt{(3.58)^2 + (2)^2}}$$

 $T_2 > 2.67$ 

The probability of a failure-in-use associated with this T-value (appendix 3G) is:

The lower bound of the reliability-in-use is:

These values are the predicted reliabilities-in-use. They have been demonstrated with a total of 62 items (32 in the factorial experiment and 30 in the Bruceton up-and-down method). To demonstrate this reliability by doing all of the testing at the use condition, would require that 786 items be tested <u>without</u> a single failure.

b. <u>Two stimuli method</u>. The results of the factorial experiment described above can also be used to exemplify this method of predicting reliability-in-use. Beginning at one increment (one standard deviation) above the average use-condition, the g-level can be increased one increment at a time (as in the Bruceton method) until the first failure is obtained. The proportions of failures at this point and at a point three increments above this point are as follows:

g-level	Proportions of failures
12.0	1/10
18.0	6/10

This method (under these conditions) required a total of 23 test specimens — 3 before obtaining the first failure and 10 at each of the two points on the curve.

Calculate the average (H) and the standard deviation (S) of the failure rate as follows (ref. 10):  $H = X_1 + d$  (H)'

$$\cdot$$
 S = d S<sup>1</sup>

Where:

 $X_1 = 12$  g's the weaker stimulus.

 $p_1 = 0.10$ , the proportion of failures at 12 g's.

 $p_2 = 0.60$ , the proportion of failures at 18 g's.

d = 6 g's (18 - 12 g's) the increment used.

H' 0.8350, the factor associated with p<sub>1</sub> and p<sub>2</sub> in table II of ref. 10 for calculating the average.

S<sup>1</sup> = 0.6515, the factor associated with p<sub>1</sub> and p<sub>2</sub> in table II of ref. 10 for calculating the standard deviation.

H = Average (50 percent point) of the failure distribution (strength) curve.

S = Standard deviation of the failure distribution (strength) curve.

When:

$$\overline{H}$$
 = 12.0 + 6.0 (0.8350) = 17.0 g/s.

$$S = (0.6515) = 3.9 \text{ g/s}.$$

These same values can be obtained graphically by simply plotting the proportion of failures versus the corresponding g-forces on linear probability paper. The average is the g-force corresponding to the 50 percent point, and the standard deviation is the slope of the line thru the two points, or is the difference between the g-forces corresponding to the 16 and 50 percent points.

Using these values for the average and standard deviation, the point estimate and lower confidence limit for the (waterproofness) reliability-in-use can be calculated as in the examples for the Bruceton method.

#### **APPENDIX 2**

#### **GLOSSARY OF TERMS**

#### Attribute

A qualitative characteristic (such as acceptable or rejectionable, success or failure, rusted or not rusted, wet or dry, black or white, miss or hit), which can have two or more categories.

#### Attribute data

Data denoting a qualitative characteristic. This type of data can have only discrete values and is derived by counting the number of times each category occurs, such as, four failures and six successes.

#### Best Estimate

An estimator is said to give the "best estimate" of the true population parameter if it complies with the following requirements which are taken as the definition of the word "best":

- A. The average of all possible values of the estimator equals the true population parameter.
- B. In any particular case the deviation of the estimator from the true population parameter is less than any other possible estimator.

#### Binomial data

Attribute data that has only two categories or only two possible outcomes such as success and failure.

#### Blocking

In experimental design, a block is a homogeneous group of items, all treated under controlled conditions such as by the same operator, the same calibration of the measuring instrument, or the same short period of time. The purpose of blocking is to reduce the effect of the heterogeneity of material and changing conditions by dividing the experiment into rational subdivisions.

#### Confidence interval

The range of values within which the true population parameter (mean or standard deviation) is expected to lie. The confidence level associated with this interval is a probability statement expressing the proportion of the time the true value is expected to be within the interval.

#### Confidence level

The confidence level is the probability of being right in our predictions or conclusions. This value is equal to one minus the error of the first kind. The magnitude of this error that can be tolerated should be established during the planning stage of the experiment (prior to data collecting) based on the consequences of being wrong and thereby establish the confidence level.

#### Confounding

When certain comparisons can be made only for treatments in combination and not for separate treatments, those treatment effects are said to be confounded. Conclusions drawn about the separate effects in this case will be ambiguous. Confounding is often a deliberate feature of the experimental design but may arise from inadvertent imperfections.

#### Criterion

The measu able characteristic used to evaluate the treatment effects. Criteria can also be considered as the dependent variables used as a standard of reference to distinguish between the independent variable effects. Velocity, functioning time, voltage, rate of detonation, etc., can be criteria.

#### Degrees of freedom

The number of degrees of freedom is equal to the number of independent observations minus the number of parameters (such as the mean) estimated. That is, degrees of freedom usually equal the sample size minus one. In computing the variance for example, only (n-1) of the deviations from the mean can be independent. The n<sup>th</sup> deviation has to be restricted in order to make the sum of all "n" deviation total zero.

#### **Effect**

In statistics the meaning of the word effect is synonomous with the word difference. A treatment effect is the difference caused by the treatment, such as the difference in the measured results before and after the treatment.

#### Efficiency

An estimator or an experimental design is said to be efficient if a given precision can be obtained with a smaller sample size or with less time and cost.

#### Error

Chance variations are considered errors in statistics. Deviations from the expected value, due to chance, form the familiar bell shaped normal curve. This is sometimes called the normal curve of error. Error in the statistical sense does not imply that a mistake has been made.

#### Error mean square

The error mean square is the variance and is also the square of the standard deviation. It is calculated by finding the sum of the squares of the deviations of the individual sample values from their mean and dividing by the number of degrees of freedom.

#### Error of estimate

The difference between an estimated value and the true value.

#### Error of first kind

If, as a result of a statistical test, the null hypothesis is rejected when it is true, then it is said that an error of the first kind is committed. This type of error is also called:

- a. The alpha error.
- b. The producer's risk.
- c. The risk of rejecting good material.

The magnitude of this error should be established from the consequences of being wrong and controlled at that level by calculating the required sample size.

#### Error of observation

An error of observation arises from insperfections in the method of measurement or from numan mistakes.

#### Error of second kind

If, as a result of a statistical test, the null hypothesis is accepted when it is false, then it is said that an error of the second kind is committed. This type of error is also called:

- a. The beta error.
- b. The consumer's risk.
- c. The risk of accepting poor material.

After the error of the first kind has been established, the error of the second kind is controlled by the sample size. This error is very important in Ordnance work because it controls the probability of accepting poor material.

#### Estimate

An estimate is the particular value obtained by an estimator in a given set of circumstances.

#### Estimator

An estimator is the method of estimating a constant of a parent population. It is usually expressed as a function of sample values (such as the average) and therefore is a variable.

#### Experimental error

Experimental error is the chance variation to be expected under controlled conditions. It is not the result of mistakes in experimental design or avoidable imperfections in technique.

#### Experimental unit

An experimental unit is the smallest subdivision of the experimental material that can receive different treatments in the actual experiment. It is also known as a test specimen.

#### **Factor**

A factor is a quantity under examination (in an experiment) as a possible cause of variation. In practice the terms factor, treatment, and variable are loosely used interchangeably in this sense.

#### Factorial experiment

An experiment which investigates all of the possible treatment combinations that may be formed from the factor versions under investigation.

#### Fractional factorial experiment

This is a fractional part of a factorial experiment. When three or more factors are used in a factorial experiment only a fractional part (1/2, 1/4, 1/8) of the total number of possible combinations need be used if certain of the interactions can be considered negligible. This device can be resorted to without loss of efficiency when the number of factors to be investigated makes the full factorial so large that it is impractical to use.

#### **Hypothesis**

A hypothesis is a contention based on preliminary observation of what appears to be fact. It is the prediction derived from past experience that is to be verified or rejected by experimentation. Natural "laws" are hypothesis which have been subjected to various tests and have been accepted. In statistical tests two hypothesis are used:

- a. The <u>null hypothesis</u> is a hypothesis of "no difference." This is the assumption that the contemplated changes will make no difference. This hypothesis is formulated for the express purpose of being rejected in the process of controlling the error of the first kind.
- b. The <u>alternative hypothesis</u> is the operational statement of the experimenter's prediction. It is the positive statement that the changes will make a detectable difference. If the resultant data reject the null hypothesis the alternative hypothesis will be accepted.

#### Independence

Measurements are independent if the taking of one does not effect any of the others. That is, there is no correlation among them. Treatment effects are said to be independent if, in an orthogonal experiment, there is no interaction.

#### Interaction

Interaction is a measure of the extent to which the effect of changing the level of one factor depends on the level of another factor. Interaction is said to be present when a certain particular combination of treatments produces unusual (unpredictable) results. Only factorial type experiments can measure interaction effects.

#### Levels

The level of a factor (or treatment) denotes the intensity with which it is used or applied. Levels of a factor may be either qualitative, such as presence and absence of the treatment, or the levels may be quantitative, such as the number of volts applied.

#### Main effects

A main effect is the average difference(s) bettreen (or among) the levels of a variable or treatment when averaged over all of the other treatmens which form a part of the same orthogonal experiment. If significant interaction effects are present, care must be taken in stating the main effects. In such cases the level of the interacting treatment associated with the stated main effect must also be stated.

#### Normal distribution

The physical appearance of a normal distribution is the familiar bell-shaped curve. A normal distribution can not be represented by only a single curve. It is actually a family of curves whose areas under them are distributed in a very specific manner. A normal curve has the following properties:

- a. Continuous.
- b. Symmetrical.
- c. Unimodal.
- d. Asymptotic to x-axis.
- e. Completely described by the mean and standard deviation.
- f. The distance between the ordinate of the mean and the inflection point on either half of the curve is equal to the standard deviation.
- g. The area included between the ordinates drawn thru the two inflection points equals 68.27 percent of the total area under the curve.

#### Parameter

A parameter is a quantity such as the mean or standard deviation, calculated from a population. The population mean and standard deviation are parameters and as such are constants. In actual practice parameters are usually unknown.

#### Point estimate

This is one of the two principal bases of estimation in statistical analysis. Point estimation endeavors to give the best single estimated value of a parameter, as compared with interval estimation which specifies a range of values. Since a point estimate includes an error of measurement, the difference between a point and an interval is not always clear. In interpretation they often amount to the same thing.

#### **Population**

A population is any set of individuals or objects having some common observable characteristic. The term population may refer either to the individuals measured or to the measurements themselves. A population is usually considered to consist of an *infinite* number of individuals. The curve of the normal distribution graphically represents a population.

#### Precision

Precision is a property of the measuring system and refers to the ability of the system to reproduce previous results. Precision should be distinguished from accuracy which refers to the magnitude of the difference between the observed values and the true value of the characteristic being measured. Precision should also be distinguished from the sensitivity of the measuring system which is the ability of the system to detect actual variations that occur. An insensitive system will give the false impression of high precision (small variation).

#### Probability

In applied statistics probability can be considered a relative frequency or a simple proportion. Probability is the relative frequency of events in a very long sequence of trials. For example, the probability of a particular coin falling heads up is the ratio of the number of heads occurring to the total number of trials in a sequence of trials. In somewhat similar fashion a normal distribution can be formed from a very large body of data. As a result, the area under the normal curve is used as a measure of probability.

#### Randomization

The word randomization has a very special technical meaning in statistics. It means rearranging a group of items or numbers into a series or sequence having no recognizable pattern. The essential feature of randomization is that is should be an objective impersonal procedure. Whether or not proper randomization has been obtained should not be determined by an examination of the individuals randomized, but rather by examining the properties of the procedure by which randomization was accomplished. The objectives of randomizing are as follows:

- a. To give the laws of chance free play.
- b. To give every possible sequence an equally likely chance of occurring.

- c. To assure that adjacent individuals are completely independent.
- d. To remove biases of any kind.
- e. To prevent systematic error.

#### Reliability

In missile technology reliability is the probability of success in performing a specified function, under a specified condition, for a specified length of time, and after a specified period of time. From this it is clear that any particular component can have many reliability values simultaneously-one for every possible combination of function, condition, and time.

#### Replication

Replication is the performance of an experiment in its entirety one or more times. Two or more replications are usually for the purpose of obtaining an independent measure of the sampling or experimental error. Replication should be distinguished from repetition, in that, replication means repetition carried out under the same conditions, at the same time, by the same operators, with the same instruments, and with the same homogeneous material. A replication is sometimes considered a block.

#### Sample

Any finite subset of a population is a sample of that population.

#### Sample size

The sample size is the number of items or individual values in the sample.

#### Standard deviation

a. <u>Definition</u>. The standard deviation is a measure of the variation among the individual values in a sample and a measure of the dispersion among the individual values in a frequency distribution. It is the most efficient measure of precision and is designated by the lower case letter "s". This value is large for large variations (poor precision) and small for small variations (good precision). Although the word "error" is sometimes used in referring to the standard deviation or its square (the variance) these values can measure only precision in the true sense of the word. They do not measure accuracy.

If the term standard deviation is stated alone and not modified or otherwise qualified by an accompanying word or phrase, it is understood that the term refers to the standard deviation of the individual sample measurements. This value can be calculated from the sample data and is a variable.

There are two additional kinds of standard deviations:

- 1. The population standard deviation which is a constant and cannot be calculated from the sample data. This value is designated by the small Greek letter sigma and is usually considered unknown unless a very large body of data is collected to measure it or unless it is assigned a value as in a specification requirement.
- 2. The standard deviation of the mean is a measure of the variation among several sample averages. This value can be calculated from sample data and it is a variable. It is usually designated by the lower case letter "s" with the subscript X. If all of the sample sizes are equal this value can be calculated by dividing the standard deviation of the individual sample values by the square root of the number of individual values in each of the samples.
  - b. Calculation of the standard deviation for variable type data:

$$s = \underbrace{\sum_{i=1}^{i=n} (\overline{x} \cdot x_i)^2}_{n-1} = \underbrace{\sum_{i=1}^{i=n} (x_i)^2 \cdot \underbrace{\sum_{i=1}^{i=n} x_i}_{n-1}}_{2}$$

where:

s = Sample standard deviation of the individual values.

= This symbol means to add all of the "n" quantities

i = 1 = designated by the parentheses. It is read: sum from i = 1 to i = n.

 $\overline{X}$  = Sample average.

x; = Any one of the "n" values that make up the sample.

n = Sample size or the number of individual values that make up the sample.

(n-1) = Number of degrees of freedom associated with the standard deviation.

s<sup>2</sup> = Sample variance of the individual values.

 $s/\sqrt{n}$  = Sample standard deviation of the mean (s<sub>v</sub>).

#### Statistic

A statistic is a summary value calculated from a sample of values. The sample mean is a statistic and as such is a variable, not a constant.

#### Statistical significance

A difference or an effect is said to be statistically significant if it is greater than that expected due to chance alone. If the probability (chance) is very small that a value came from a particular population, the difference between that value and the mean of the population is said to be statistically significant.

#### Statistics '

The subject of statistics is the science of collecting, analyzing, and interpreting numerical data.

#### Treatment.

In experimentation, a treatment is a stimulus which is applied in order to observe the effect on the experimental situation. A treatment may refer to a physical substance, a procedure, or anything which is capable of controlled application. In statistical parlance a treatment is the variable being studied or the experimental condition.

#### True Value

The true value is another expression for a population parameter such as the population mean or standard deviation. The true value can also be the expected value or the theoretical value.

#### Validation -

Validation is a procedure which provides, by reference to independent sources, evidence that an inquiry is free from bias, or otherwise conforms to its declared purpose. In statistics it is usually applied to a sample investigation with the object of showing that the sample is reasonably representative of the population and that the information collected is accurate.

#### Variable

A variable is any quantity or measurable characteristic which varies. More precisely in statistics a variable is any quantity which can have any one of a specified set of values.

#### Variable data

Variable data is a term used to describe a type of data that can vary on a continuous scale from zero to infinity. Weight in pounds, length in feet, E.M.F. in volts, and temperature in degrees are variable type data.

#### Variance

Variance is a measure of variation in a sample, or dispersion in a frequency distribution. The variance is equal to the square of the standard deviation.

Table 1

MINIMUM CONTRASTS 95% (TWO SIDED) TEST

N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

N	No. of A's in Sample (1)/No. of A's in Sample (2)
4	0/4 1/-
5	0/4 1/5 2/-
6	0/5 1/6 2/-
7	0/5 1/6 2/7 3/-
8	0/5 1/6 2/7 3/8 4/-
9	0/5 1/6 2/8 3/8 4/9 5/-
10	0/5 1/7 2/8 3/9 4/10 5/10 6/-
11	0/5 1/7 2/8 3/9 4/10 5/11 6/11 7/-
12	0/5 1/7 2/8 3/9 4/10 5/11 6/12 7/12 8/-
13	0/5 1/7 2/8 3/9 4/10 5/11 6/12 7/13 8/13 9/-
14	0/5 1/7 2/8 3/10 2/11 5/12 6/12 7/13 8/14 9/14 10/-
15	0/5 1/7 2/9 3/10 4/11 5/12 6/13 7/14 8/14 9/15 10/15 11/-
16	0/5 1/7 2/9 3/10 4/11 5/12 6/13 7/14 8/15 9/15 10/16 11/16 12/-
17	0/5 1/7 2/9 3/10 4/11 5/12 6/13 7/14 8/15 9/16 10/16 11/17 12/17
	13/-
18	0/5 1/7 2/9 3/10 4/11 5/12 6/13 7/14 8/15 9/16 10/17 11/17 12/18
	13/18 14/-
19	0/5 1/7 2/9 3/10 4/11 5/12 6/14 7/14 8/15 9/16 10/17 11/18 12/18
	13/19 14/19 15/-

# Table 1 (Continued)

# MINIMUM CONTRASTS 95% (TWO SIDED) TEST

# N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

N	No. of A's in Sample (1)/No. of A's in Sample (2)
20	0/5 1/7 2/9 3/10 4/11 5/13 6/14 7/15 8/16 9/16 10/17 11/18 12/19
	13/19 14/20 15/20 16/-
30	0/6 1/8 2/9 3/11 4/12 5/13 6/15 7/16 8/17 9/18 10/19 16/25 17/25
	20/28 21/28 23/30 24/30 25/-
40	0/6 1/8 2/9 3/11 4/12 5/14 6/15 7/16 8/18 9/19 10/20 23/33 24/33
	27/36 28/36 30/38 31/38 33/40 34/40 35/-
50	0/6 1/8 2/10 3/11 4/13 5/14 6/15 7/17 8/18 9/19 10/20 11/22 29/40
	30/40 34/44 35/44 38/47 39/47 41/49 42/49 44/50 45/-
60	0/6 1/8 2/10 3/11 4/13 5/14 6/16 7/17 8/18 9/20 10/21 11/22 12/23
	13/24 14/26 35/47 36/47 41/52 42/52 45/55 46/55 48/57 49/57 51/59
	52/59 53/60 54/60 55/-
70	0/6 1/8 2/10 3/11 4/13 5/14 6/16 7/17 8/18 9/20 10/21 11/22 12/23
• •	13/25 18/30 19/32 20/33 39/52 40/52 46/58 47/58 51/62 52/62 55/65
	56/65 58/67 59/67 61/69 62/69 63/70 64/70 65/-
80	0/6 1/8 2/10 3/11 4/13 5/14 6/16 7/17 8/19 9/20 10/21 11/22 12/24
٠	13/25 14/26 15/27 16/29 23/36 24/38 43/57 44/57 52/65 53/65 57/69
	58/69 62/73 63/73 65/75 66/75 68/77 69/77 71/79 72/79 73/80 74/80
•	75/-

# Table 1 (Continued)

# MINIMUM CONTRASTS 95% (TWO SIDED) TEST N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

N ·	No. of A's in Sample (1)/ No. of A's in Sample (2)
90	0/6 1/8 2/10 3/11 4/13 5/14 6/16 7/17 8/19 9/20 10/21 11/23 12/24
	13/25 14/26 15/28 20/33 21/35 31/45 32/47 44/59 45/59 56/70 57/70
,	63/76 64/76 68/80 69/80 72/83 73/83 75/85 76/85 78/87 79/87 81/89
	82/89 83/90 84/90 85/-
100	0/6 1/8 2/10 3/11 4/13 5/15 6/16 7/17 8/19 9/20 10/21 11/23 12/24
	13/25 14/27 18/31 19/33 25/39 26/41 60/75 61/75 68/82 69/82 74/87
	75/87 78/90 79/90 82/93 83/93 86/96 87/96 88/97 89/97 91/99 92/99
	93/100 94/100 95/-
150	0/6 1/8 2/10 3/12 4/13 5/15 6/16 7/18 8/19 9/20 10/22 11/23 12/24
	13/26 14/27 15/28 16/30 19/33 20/35 25/40 26/42 32/48 33/50 41/58
	42/60 91/109 92/109 101/118 102/118 109/125 110/125 116/131 117/131
	121/135 122/135 125/138 126/138 129/141 130/141 133/144 134/144
,	136/146 137/146 139/148 140/148 141/149 142/149 143/150 144/150 145/-
200	0/6 1/8 2/10 3/12 4/13 5/15 6/16 7/18 8/19 9/21 10/22 11/23 12/25
	13/26 14/27 15/29 18/32 19/34 22/37 23/39 27/43 28/45 33/50 34/52
	41/59 42/61 51/70 52/72 65/85 66/87 114/135 115/135 129/149 130/149
	140/159 141/159 149/167 150/167 156/173 157/173 162/178 163/173
	167/182 168/182 172/186 173/186 176/189 177/189 180/192 181/192
	183/194 184/194 186/196 187/196 189/198 190/198 191/199 192/199
	193/200 194/200 195/-

#### Table 1 (Continued)

# MINIMUM CONTRASTS 95% (TWO SIDED) TEST N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

No. of A's in Sample (1)/ No. of A's in Sample (2)

N

0/6 1/8 2/10 3/12 4/13 5/15 6/16 7/18 8/19 9/21 10/22 11/24 12/25
13/26 14/28 15/29 16/30 17/31 18/33 19/34 20/35 21/37 24/40 25/42
29/46 30/48 35/53 36/55 41/60 42/62 48/68 49/70 56/77 57/79 66/88
67/90 78/101 79/103 95/119 96/121 180/205 181/205 198/222 199/222
211/234 212/234 222/244 223/244 231/252 232/252 239/259 240/259
246/265 247/265 253/271 254/271 259/276 26C/276 264/280 265/280
268/283 269/283 273/287 274/287 277/290 278/290 280/292 281/292
283/294 284/294 286/296 287/296 289/298 290/298 291/299 292/299
293/300 294/300 295/-

Table 2

# MINIMUM CONTRASTS 99% (TWO SIDED) TEST N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

	N	N of A's in Sample (1)/ No. of A's in Sample (2)	
	5	0/5 1/-	
	6	0/6 1/-	
	7	0/6 1/7 2/-	
	8	0/6 1/8 2/8 3/-	
	9 .	0/6 1/8 2/9 3/9 4/-	
	10	0/7 1/8 2/9 3/10 4/-	
	11	C/7 1/8 2/9 3/10 4/11 5/ <del>-</del>	
•	12	0/7 1/8 2/10 3/11 4/11 5/12 6/-	
•	13	0/7 1/9 5/13 6/13 7/-	
	14	0/7 1/9 6/14 7/14 8/-	
	15	c/7 1/9 7/15 8/15 9/-	
	16	0/7 1/9 2/10 3/12 4/13 5/14 6/14 8/16 9/16 10/-	
	17	0/7 1/9 2/11 7/16 8/16 9/17 10/17 11/-	
•	18	0/7 1/9 2/11 8/17 9/17 10/18 11/18 12/-	•
	19	0/7 1/9 2/11 9/13 10/18 11/19 12/19 13/-	
	20	0/7 1/9 2/11 4/13 5/15 6/16 7/16 10/19 11/19 12/20 13/20 14/-	
	30	0/5 1/10 2/12 3/13 4/15 10/21 16/27 17/27 18/28 19/29 20/29	
		21/30 22/30 23/+	
•	40	0/8 1/10 2/12 3/14 4/15 5/17 8/20 9/22 19/32 20/32 24/36 25/36	
		27/38 28/38 29/39 30/39 31/40 32/40 33/-	
	50	0/8 1/10 2/12 3/14 4/15 5/17 6/18 7/20 9/22 10/24 27/41 28/41	
		31/44 32/44 34/46 35/46 37/48 38/48 39/49 40/49 41/50 42/50 43/	•
		· ·	

# Table 2 (Continued)

# MINIMUM CONTRASTS 99% (TWO SIDED) TEST N = TOTAL NUMBER OF TRAILS IN EACH SAMPLE

N	No. of A's in Sample (1)/No. A's in Sample (2)
60	0/8 1/10 2/12 3/14 4/16 5/17 6/19 8/21 9/23 11/25 12/27
	19/34 20/36 24/40 25/41 26/41 34/49 35/49 38/52 39/52
	42/55 43/55 45/57 46/57 47/58 48/58 49/59 50/59 51/60
,	52/60 53/-
70	0/8 1/10 2/12 3/14 4/16 5/17 6/19 7/20 8/22 10/24 11/26
	14/29 15/31 21/37 22/39 32/49 33/49 34/50 40/56 41/56
	45/60 46/60 49/63 50/63 52/65 53/65 55/67 56/67 57/68
	58/68 59/69 60/69 61/70 62/70 63/-
80	0/8 1/10 2/12 3/14 4/16 5/18 6/19 7/21 9/23 10/25 12/27
	13/29 16/32 17/34 24/41 25/43 38/56 39/56 47/64 48/64
	52/68 53/68 56/71 57/71 60/74 61/74 63/76 64/76 65/77 66/77
	67/78 68/78 69/79 70/79 71/80 72/80 73/-
90	0/8 1/10 2/12 3/14 4/16 5/18 6/19 7/21 8/22 9/24 11/26 12/28
	15/31 16/33 19/36 20/38 28/46 29/48 43/62 44/62 53/71 54/71
	58/75 59/75 63/79 64/79 67/82 68/82 70/84 71/84 73/86 74/86
	75/87 76/87 77/88 78/88 79/89 80/89 81/90 82/90 83/-
100	0/8 1/10 2/13 3/14 4/16 5/18 6/19 7/21 8/22 9/24 10/25 11/27
	14/30 15/32 18/35 19/37 23/41 24/43 33/52 34/54 47/67 48/67
	58/77 59/77 64/82 65/82 69/86 70/86 74/90 75/90 77/92 78/92
	80/94 81/94 83/96 84/96 85/97 86/97 88/99 89/99 90/99 91/100
	92/100 93/-
	60 70 80

## Table 2 (Continued)

# MINIMUM CONTRASTS 99% (TWO SIDED) TEST

# N = TOTAL NUMBER OF TRIALS IN EACH SAMPLE

N	No. of A's in Sample (1)/No. of A's in Sample (2)
150	0/8 1/11 2/13 3/15 4/16 5/18 6/20 7/21 8/23 9/24 10/26
•	11/27 12/29 14/31 15/33 17/35 18/37 21/40 22/42 26/46
	27/48 31/52 32/54 39/61 40/63 51/74 52/76 75/99 76/99
	88/111 89/111 97/119 98/119 103/124 104/124 109/129 110/129
·	114/133 115/133 118/136 119/136 122/139 123/139 125/141 126/141
4	128/143 129/143 131/145 132/145 133/146 134/146 136/148 137/148
	138/149 139/149 140/150 141/150 142/150 143/-
200	0/8 1/11 2/13 3/15 4/16 5/18 6/20 7/21 8/23 9/24 10/26 11/27
•	12/29 13/30 14/32 16/34 17/36 19/38 20/40 23/43 24/45 26/47
	27/49 31/53 32/55 36/59 37/61 43/67 44/69 51/76 52/78 63/89
	64/91 110/137 111/137 123/149 124/149 132/157 133/157 140/164
•	141/164 146/169 147/169 152/174 159/174 156/177 157/177
, .	161/181 162/181 165/184 166/184 169/187 170/187 172/189 173/189
·	175/191 176/191 178/193 179/193 181/195 182/195 183/1:6 184/196
	186/198 187/198 188/199 189/199 190/200 191/200 192/200 193/-
300	C/8 1/11 2/13 3/15 4/17 5/18 6/2C 7/22 8/23 9/25 1C/26 11/28
•	12/29 13/31 15/33 16/35 17/36 18/38 20/40 21/42 23/44 24/46
	27/49 28/51 31/54 32/56 35/59 36/61 40/65 41/67 45/71 46/73 51/78
	52/80 58/86 59/88 66/95 67/97 76/106 77/108 88/119 89/121 107/139
	108/141 160/193 161/193 180/212 181/212 193/224 194/224 204/234
•	205/234 213/242 214/242 221/249 222/249 228/255 229/255 234/260
	235/260 240/265 241/265 245/269 246/269 250/273 251/273 255/277
	256/277 259/280 260/280 263/283 264/283 266/285 267/285 270/288
	271/288 273/290 274/290 276/292

<u>N</u>	£	<u>C</u>	<u>.500</u>	<u>. 800</u>	<u>. 900</u>	<u>.950</u>	.990	.995
. 1	0		.500	.800	. 900	<b>. 95</b> 0	•990	• 995
2	0		.129 .198	.581 .912	.684 .949	.776 .975	• 900 • 995	• 929 • 995
3	0 1 2		.206 .500 793	.430 .733 .941	.536 .804 .966	.632 .865 .980	.785 .941 .997	.829 .959 .998
4	0 1 2 3		.159 .386 .614 .841	. 349 . 604 . 803 . 948	.438 .680 .857 .974	.527 .751 .902 .987	.684 .859 .958 .997	.733 .889 .971 1.000
<b>5</b>	0 1 2 3		0.129 0.314 0.500 0.686	0.275 0.490 0.673 0.831	0.369 0.584 0.753 0.888	0.451 0.657 0.811 0.924	0.602 0.778 0.894 0.967	0.653 0.815 0.917 0.977
6	0 1 2 3		0.109 0.264 0.421 0.579	0.235 0.422 0.585 0.731	0.319 0.510 0.667 0.799	0.393 p.582 0.729 0.847	0.536 0.706 0.827 0.915	0.586 0.746 0.856 0.934
. 7	0 1 2 3 4		0.094 0.228 0.364 0.500 0.636	0.205 0.371 0.517 0.650 0.772	0.280 0.453 0.596 0.721 0.830	0.348 0.521 0.659 0.775 0.871	0.482 0.643 0.764 0.858 0.929	0.531 0.685 0.797 0.882 0.945
8	0 1 2 3 lı		0.083 0.201 0.321 0.140 0.560	0.182 0.330 0.462 0.584 0.697	0.250 0.406 0.538 0.655 0.760	0.312 0.471 0.600 0.711 0.807	0.438 0.590 0.707 0.802 0.879	0.484 0.632 0.742 0.830 0.900

<u>N</u>	£	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	.990	<u>. 995</u>
9	0 1 2 3 4 5		0.074 0.180 0.286 0.393 0.500 0.607	0.164 0.298 0.418 0.529 0.634 0.732	0.226 0.368 0.490 0.599 0.699 0.790	0.283 0.429 0.550 0.655 0.749 0.831	0.401 0.544 0.656 0.750 0.829 0.895	0.445 0.585 0.693 0.781 0.854 0.913
10	0123456		0.067 0.162 0.259 0.355 0.452 0.548 0.645	0.149 0.271 0.381 0.484 0.581 0.673 0.761	0.206 0.337 0.450 0.552 0.646 0.733 0.812	0.259 0.394 0.507 0.607 0.696 0.778 0.850	0.369 0.504 0.612 0.703 0.782 0.850 0.907	0.411 0.544 0.648 0.735 0.809 0.872 0.923
11 (	0123456	. ;	0.061 0.148 0.235 0.324 0.412 0.500 0.588	0.136 0.249 0.350 0.445 0.536 0.622 0.705	0.189 0.310 0.415 0.511 0.599 0.682 0.759	0.238 0.364 0.470 0.564 0.650 0.729 0.800	0.342 0.470 0.572 0.660 0.738 0.806 0.866	0.382 0.509 0.608 0.693 0.767 0.831 0.886
12	0 1 2 3 4 5 6 7		0.056 0.136 0.217 0.298 0.379 0.460 0.540 0.621	0.126 0.230 0.324 0.412 0.497 0.578 0.656 0.731	0.175 0.288 0.386 0.475 0.559 0.638 0.712 0.781	0.221 0.339 0.438 0.527 0.609 0.685 0.755 0.819	0.319 0.440 0.537 0.622 0.698 0.765 0.825	0.357 0.477 0.573 0.655 0.728 0.791 0.848 0.897
13	01234567		0.052 0.126 0.200 0.275 0.350 0.125 0.500 0.575	0.116 0.213 0.301 0.384 0.463 0.539 0.613 0.684	0.162 0.268 0.360 0.1111 0.523 0.598 0.669 0.736	0.206 0.316 0.410 0.495 0.573 0.645 0.713 0.776	0.298 0.413 0.506 0.588 0.661 0.727 0.787 0.841	0.334 0.149 0.541 0.621 0.691 0.755 0.811 0.862

C = One-sided confidence level N = Sample size E = Observed number of failures in a sample of N trials

N	<u>F</u>	<u>C</u>	.500	.800	<u>. 900</u>	<u>.950</u>	<u>•990</u>	<u>•995</u>
14	0 1 2 3 4 5 6 7 8		0.048 0.117 0.186 0.256 0.326 0.395 0.465 0.535 0.605	0.109 0.199 0.281 0.359 0.434 0.506 0.575 0.643 0.708	0.152 0.251 0.337 0.417 0.492 0.563 0.631 0.695 0.757	0.193 0.297 0.385 0.466 0.540 0.610 0.675 0.736 0.794	0.280 0.389 0.478 0.557 0.527 0.692 0.751 0.805 0.854	0.315 0.424 0.512 0.589 0.658 0.720 0.777 0.828 0.873
15	0 1 2 3 4 5 6 7 8 9		0.045 0.109 0.174 0.239 0.305 0.370 0.435 0.500 0.565 0.630	0.102 0.187 0.264 0.337 0.407 0.476 0.542 0.606 0.668 0.728	0.142 0.236 0.317 0.393 0.464 0.532 0.596 0.658 0.718	0.181 0.279 0.363 0.440 0.511 0.577 0.640 0.700 0.756 0.809	0.264 0.368 0.453 0.529 0.597 0.660 0.718 0.771 0.821 0.865	0.298 0.402 0.486 0.561 0.627 0.688 0.744 0.795 0.841 0.883
16	0123456789		0.042 0.103 0.164 0.225 0.286 0.347 0.408 0.469 0.531 0.592	0.096 0.176 0.249 0.318 0.385 0.449 0.512 0.573 0.632 0.690	0.134 0.222 0.300 0.371 0.439 0.504 0.565 0.625 0.682 0.737	0.170 0.264 0.344 0.417 0.484 0.548 0.609 0.667 0.721 0.773	0.250 0.349 0.430 0.503 0.569 0.630 0.687 0.739 0.788 0.834	0.282 0.381 0.463 0.534 0.599 0.658 0.713 0.764 0.810 0.853
17	0 1 2 3 4 5 6 7 8 9 10		0.040 0.097 0.154 0.212 0.269 0.327 0.385 0.442 0.500 0.558 0.615	0.090 0.166 0.235 0.301 0.364 0.425 0.485 0.543 0.600 0.655	0.127 0.210 0.284 0.352 0.416 0.478 0.537 0.594 0.650 0.703	0.162 0.250 0.326 0.396 0.461 0.522 0.580 0.636 0.689 0.740 0.788	0.237 0.332 0.410 0.480 0.543 0.603 0.658 0.709 0.758 0.803 0.815	0.268 0.363 0.441 0.510 0.573 0.631 0.685 0.734 0.781 0.824 0.863

<u>N</u>	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>. 995</u>
18	0 1 2 3 4 5 6 7 8 9		0.038 0.092 0.146 0.200 0.255 0.309 0.364 0.418 0.473 0.527	0.086 0.157 0.223 0.285 0.345 0.404 0.460 0.516 0.570 0.623 0.675	0.120 0.199 0.269 0.334 0.396 0.455 0.512 0.567 0.620 0.671 0.721	0.153 0.238 0.310 0.377 0.439 0.498 0.554 0.608 0.659 0.756	0.226 0.316 0.391 0.458 0.520 0.577 0.631 0.681 0.729 0.774	0.255 0.346 0.422 0.488 0.549 0.605 0.658 0.707 0.753 0.795 0.835
19	0 1 2 3 4 5 6 7 8 9 10 11		0.036 0.087 0.138 0.190 0.242 0.293 0.345 0.397 0.448 0.500 0.551 0.603	0.081 0.150 0.212 0.271 0.325 0.384 0.438 0.491 0.543 0.594 0.693	0.114 0.190 0.257 0.319 0.378 0.434 0.489 0.541 0.592 0.642 0.690 0.737	0.146 0.226 0.296 0.359 0.419 0.476 0.530 0.582 0.632 0.680 0.726 0.770	0.215 0.302 0.374 0.439 0.498 0.554 0.606 0.655 0.702 0.746 0.788 0.827	0.243 0.331 0.404 0.468 0.527 0.582 0.633 0.681 0.726 0.768 0.808 0.815
20	0 2 3 4 5 6 7 8 9 10 11 12		0.034 0.083 0.131 0.181 0.230 0.279 0.328 0.377 0.426 0.475 0.525 0.574 0.623	0.077 0.142 0.202 0.259 0.313 0.360 0.418 0.469 0.519 0.568 0.616 0.663 0.709	0.109 0.181 0.245 0.304 0.361 0.415 0.467 0.518 0.567 0.662 0.707 0.751	0.139 0.216 0.283 0.314 0.401 0.456 0.508 0.558 0.606 0.653 0.698 0.741 0.783	0.206 0.289 0.358 0.421 0.478 0.532 0.583 0.631 0.677 0.720 0.761 0.800 0.837	0.233 0.317 0.387 0.449 0.507 0.560 0.610 0.657 0.701 0.743 0.782 0.819 0.854
21	0 1 2 3		0.032 0.079 0.125 0.172	0.074 0.136 0.193 0.247	0.104 0.173 0.234 0.291	0.133 0.207 0.271 0.329	0.197 0.277 0.3hh 0.40h	0.223 0.304 0.372 0.432

								ססר
$\overline{N}$	F	<u>C</u>	<u>.500</u>	.800	<u>• 900</u>	· <u>• 950</u>	<u>.990</u>	<u>. 995</u>
	4 5 6 7 8 9 10 11		0.219 0.266 0.313 0.359 0.406 0.453 0.500 0.547 0.594	0.299 0.350 0.400 0.449 0.497 0.544 0.590 0.635 0.680	0.345 0.397 0.148 0.497 0.514 0.590 0.636 0.679 0.722	0.384 0.437 0.487 0.536 0.583 0.628 0.672 0.714	0.460 0.512 0.561 0.608 0.653 0.695 0.736 0.774 0.810	0.488 0.539 0.588 0.634 0.677 0.718 0.753 0.795 0.829
22	0 1 2 3 4 5 6 7 8 9 10 11 12 13		0.031 0.075 0.120 0.164 0.209 0.254 0.299 0.343 0.388 0.433 0.478 0.522 0.567 0.612	0.071 0.130 0.185 0.237 0.287 0.336 0.383 0.430 0.476 0.521 0.566 0.610 0.653 0.695	0.099 0.166 0.224 0.279 0.331 0.430 0.477 0.523 0.568 0.611 0.654 0.695 0.736	0.127 0.198 0.259 0.316 0.369 0.420 0.468 0.515 0.561 0.605 0.647 0.689 0.729 0.767	0.189 0.266 0.331 0.389 0.443 0.493 0.541 0.587 0.630 0.672 0.712 0.750 0.786 0.821	0.214 0.292 0.358 0.416 0.470 0.520 0.567 0.612 0.655 0.695 0.734 0.771 0.805 0.838
23	0 1 2 3 4 5 6 7 8 9 10 11 12 13		0.030 0.072 0.115 0.157 0.200 0.243 0.286 0.329 0.371 0.414 0.457 0.500 0.543 0.586	0.068 0.125 0.177 0.227 0.275 0.322 0.368 0.413 0.457 0.501 0.586 0.628 0.669	0.095 0.159 0.215 0.268 0.318 0.366 0.413 0.459 0.503 0.546 0.589 0.630 0.670 0.710	0.122 0.190 0.249 0.304 0.355 0.404 0.451 0.496 0.540 0.583 0.625 0.665 0.704 0.742	0.181 0.256 0.318 0.374 0.427 0.476 0.522 0.567 0.609 0.650 0.689 0.727 0.763 0.797	0.206 0.281 0.345 0.401 0.453 0.502 0.548 0.592 0.634 0.674 0.712 0.748 0.782 0.815

Ñ	F	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>.900</u>	<u>. 950</u>	<u>• 990</u>	<u>. 995</u>
214	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14		0.028 0.069 0.110 0.151 0.192 0.233 0.274 0.315 0.356 0.397 0.438 0.479 0.562 0.603	0.065 0.120 0.170 0.218 0.26h 0.309 0.35h 0.397 0.4h0 0.482 0.523 0.564 0.60h 0.683	0.091 0.153 0.207 0.258 0.306 0.352 0.398 0.412 0.484 0.526 0.567 0.608 0.647 0.685 0.723	0.117 0.183 0.240 0.292 0.342 0.389 0.435 0.479 0.521 0.563 0.603 0.642 0.681 0.718	0.175 0.246 0.307 0.361 0.411 0.459 0.504 0.548 0.589 0.629 0.667 0.704 0.740 01774 0.806	0.198 0.271 0.332 0.387 0.438 0.485 0.530 0.573 0.614 0.653 0.690 0.726 0.760 0.793 0.824
25	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		0.027 0.066 0.106 0.145 0.184 0.224 0.263 0.303 0.342 0.382 0.421 0.461 0.500 0.539 0.579 0.618	0.062 0.115 0.163 0.210 0.254 0.298 0.340 0.382 0.423 0.464 0.504 0.504 0.583 0.621 0.659 0.697	0.088 0.147 0.199 0.248 0.295 0.340 0.383 0.426 0.467 0.508 0.548 0.587 0.625 0.662 0.699 0.735	0.113 0.176 0.231 0.282 0.330 0.375 0.420 0.462 0.504 0.514 0.583 0.621 0.659 0.695 0.730 0.764	0.168 0.237 0.296 0.349 0.398 0.444 0.488 0.531 0.571 0.610 0.648 0.684 0.719 0.752 0.784 0.815	0.191 0.262 0.321 0.374 0.424 0.470 0.514 0.555 0.595 0.633 0.670 0.705 0.739 0.772 0.803 0.832
26	0 1 2 3 4 5 6 7 8 9 10		0.026 0.064 0.102 0.139 0.177 0.215 0.253 0.291 0.329 0.367 0.405	0.060 0.111 0.157 0.202 0.245 0.287 0.328 0.369 0.408 0.408 0.448	0.085 0.142 0.192 0.239 0.284 0.328 0.370 0.411 0.451 0.451	0.109 0.170 0.223 0.272 0.318 0.363 0.405 0.447 0.487 0.526 0.564	0.162 0.229 0.286 0.337 0.385 0.430 0.473 0.514 0.554 0.592 0.628	0.184 0.253 0.310 0.362 0.410 0.455 0.458 0.538 0.578 0.615 0.651

<u>N</u>	F	<u>C</u> ,	.500	.800	<u>. 900</u>	<u>• 950</u>	<u>.990</u>	• 995
,	11 12 13 14 15		0.443 0.481 0.519 0.557 0.595	0.525 0.562 0.600 0.637 0.673	0.567 0.604 0.641 0.676 0.711	0.602 0.638 0.673 0.708 0.742	0.664 0.698 0.731 0.763 0.794	0.686 0.719 0.751 0.782 0.811
27	0 1 2 3 4 5 6 7 8 9 10 11 12 14 15 16		0.025 0.061 0.098 0.134 0.171 0.207 0.244 0.281 0.317 0.354 0.390 0.427 0.463 0.570 0.573 0.610	0.058 0.107 0.152 0.195 0.236 0.277 0.317 0.356 0.394 0.432 0.470 0.507 0.514 0.651 0.686	0.082 0.137 0.185 0.231 0.275 0.317 0.358 0.397 0.436 0.475 0.512 0.549 0.585 0.620 0.655 0.689 0.723	0.105 0.164 0.215 0.263 0.308 0.351 0.392 0.432 0.471 0.509 0.517 0.583 0.618 0.653 0.687 0.720 0.752	0.157 0.222 0.277 0.326 0.373 0.417 0.458 0.498 0.537 0.574 0.610 0.645 0.679 0.711 0.743 0.773 0.802	0.178 0.245 0.300 0.351 0.397 0.441 0.483 0.523 0.561 0.597 0.633 0.667 0.700 0.731 0.762 0.791 0.819
28	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16		0.024 0.059 0.094 0.130 0.165 0.200 0.235 0.271 0.306 0.341 0.377 0.412 0.447 0.482 0.518 0.553 0.588	0.056 0.103 0.147 0.188 0.228 0.268 0.306 0.314 0.381 0.418 0.454 0.490 0.526 0.561 0.596 0.630 0.664	0.079 0.132 0.179 0.223 0.265 0.306 0.346 0.385 0.422 0.459 0.459 0.496 0.532 0.667 0.601 0.635 0.669	0.101 0.159 0.208 0.254 0.298 0.339 0.380 0.419 0.457 0.494 0.530 0.565 0.600 0.634 0.667 0.699	0.152 0.215 0.268 0.316 0.361 0.404 0.145 0.484 0.521 0.558 0.593 0.627 0.660 0.692 0.723 0.753 0.753	0.172 0.237 0.237 0.340 0.385 0.428 0.469 0.508 0.545 0.545 0.616 0.649 0.681 0.713 0.772 0.800

<u>N</u>	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>•950</u>	<u>.990</u>	<u>. 995</u>
29	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17		0.024 0.057 0.091 0.125 0.159 0.159 0.227 0.261 0.296 0.330 0.364 0.398 0.432 0.466 0.500 0.534 0.568 0.602	0.054 0.100 0.142 0.182 0.221 0.259 0.296 0.333 0.369 0.405 0.475 0.509 0.577 0.610 0.643 0.676	0.076 0.128 0.173 0.216 0.257 0.297 0.335 0.372 0.179 0.145 0.181 0.515 0.583 0.616 0.619 0.681 0.712	0.098 0.153 0.202 0.246 0.288 0.329 0.368 0.405 0.443 0.179 0.514 0.549 0.583 0.616 0.648 0.680 0.711 0.741	0.147 0.208 0.260 0.307 0.350 0.392 0.432 0.470 0.507 0.542 0.577 0.610 0.643 0.674 0.705 0.705 0.763 0.791	0.167 0.230 0.282 0.330 0.374 0.416 0.455 0.530 0.565 0.599 0.632 0.664 0.724 0.724 0.781 0.308
30	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18		0.023 0.055 0.088 0.121 0.154 0.187 0.220 0.253 0.253 0.319 0.352 0.418 0.451 0.484 0.516 0.516 0.582 0.615	0.052 0.097 0.137 0.176 0.214 0.251 0.287 0.322 0.358 0.392 0.426 0.460 0.494 0.527 0.559 0.559 0.656 0.656	0.074 0.124 0.168 0.209 0.249 0.287 0.324 0.361 0.397 0.432 0.466 0.500 0.533 0.566 0.599 0.630 0.662 0.692 0.723	0.095 0.149 0.195 0.239 0.280 0.319 0.357 0.430 0.465 0.499 0.533 0.566 0.598 0.630 0.661 0.695 0.721	0.142 0.202 0.252 0.298 0.340 0.381 0.420 0.457 0.527 0.561 0.594 0.626 0.657 0.716 0.715 0.715	0.162 0.223 0.274 0.320 0.363 0.404 0.443 0.480 0.550 0.550 0.616 0.617 0.707 0.735 0.763 0.789 0.815

<u>N</u>	<u>F</u>	<u>C</u>	.500	.800	<u>. 900</u>	<u>. 250</u>	.990	<u>.995</u>
31	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18		0.022 0.054 0.085 0.117 0.149 0.181 0.213 0.245 0.277 0.309 0.372 0.404 0.436 0.468 0.500 0.532 0.564 0.596	0.051 0.094 0.133 0.171 0.207 0.243 0.278 0.317 0.347 0.380 0.413 0.446 0.479 0.511 0.543 0.575 0.606 0.637 0.667	0.072 0.120 0.163 0.203 0.242 0.279 0.315 0.350 0.385 0.419 0.453 0.486 0.518 0.550 0.582 0.613 0.613 0.613 0.703	0.092 0.144 0.189 0.232 0.271 0.310 0.347 0.383 0.418 0.452 0.485 0.518 0.550 0.582 0.613 0.643 0.673 0.703 0.703	0.138 0.196 0.245 0.289 0.330 0.370 0.408 0.414 0.479 0.513 0.546 0.579 0.610 0.610 0.699 0.727 0.751 0.780	0.157 0.216 0.266 0.311 0.353 0.131 0.1467 0.502 0.536 0.569 0.600 0.631 0.661 0.661 0.690 0.718 0.715 0.772
32	0 1 2 3 4 5 6 7 8 9 11 12 13 14 15 16 17 18 19		0.021 0.052 0.083 0.114 0.175 0.206 0.237 0.268 0.299 0.330 0.361 0.392 0.423 0.423 0.454 0.515 0.515 0.516	0.049 0.091 0.129 0.166 0.201 0.236 0.270 0.303 0.303 0.369 0.401 0.433 0.465 0.496 0.527 0.558 0.589 0.619 0.649	0.069 0.116 0.158 0.197 0.234 0.271 0.306 0.340 0.374 0.407 0.440 0.535 0.566 0.596 0.626 0.655 0.684 0.713	0.089 0.139 0.183 0.224 0.263 0.300 0.336 0.371 0.406 0.439 0.472 0.504 0.535 0.566 0.596 0.626 0.625 0.684 0.712 0.740	0.134 0.190 0.238 0.281 0.322 0.360 0.397 0.433 0.467 0.500 0.532 0.564 0.682 0.654 0.682 0.710 0.736 0.763 0.788	0.153 0.210 0.259 0.303 0.314 0.383 0.415 0.455 0.455 0.554 0.555 0.616 0.645 0.674 0.728 0.754 0.754 0.754 0.780

N	E	<u>C</u>	<u>.500</u>	.800	<u>• 900</u>	<u>. 950</u>	.990	<u>. 995</u>
33	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19		0.021 0.050 0.080 0.110 0.140 0.170 0.200 0.230 0.260 0.290 0.320 0.350 0.350 0.410 0.440 0.500 0.500 0.500 0.500 0.590	0.048 0.088 0.125 0.161 0.195 0.262 0.295 0.327 0.359 0.359 0.421 0.452 0.482 0.513 0.513 0.572 0.602 0.631 0.660	0.067 0.112 0.153 0.191 0.228 0.263 0.297 0.331 0.364 0.428 0.459 0.459 0.459 0.551 0.580 0.610 0.638 0.666 0.695	0.087 0.136 0.179 0.219 0.256 0.293 0.328 0.362 0.395 0.428 0.460 0.491 0.522 0.552 0.581 0.611 0.637 0.667 0.695 0.722	0.130 0.135 0.231 0.273 0.313 0.351 0.387 0.421 0.455 0.487 0.519 0.550 0.609 0.638 0.666 0.693 0.720 0.746 0.771	0.148 0.204 0.252 0.295 0.335 0.373 0.409 0.443 0.477 0.509 0.541 0.630 0.658 0.685 0.712 0.738 0.763 0.787
34	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		0.020 0.049 0.078 0.107 0.136 0.165 0.194 0.223 0.252 0.382 0.311 0.340 0.369 0.427 0.456 0.456 0.515 0.515 0.515	0.046 0.086 0.122 0.156 0.190 0.223 0.255 0.286 0.318 0.349 0.410 0.469 0.469 0.499 0.528 0.557 0.586 0.614 0.642 0.670	0.065 0.110 0.149 0.186 0.221 0.256 0.289 0.322 0.354 0.417 0.477 0.507 0.507 0.507 0.565 0.594 0.622 0.650 0.704	0.084 0.132 0.174 0.213 0.249 0.285 0.319 0.352 0.385 0.416 0.148 0.178 0.508 0.508 0.508 0.508 0.508 0.508 0.508 0.508	0.127 0.180 0.225 0.266 0.305 0.312 0.377 0.411 0.443 0.475 0.506 0.537 0.566 0.595 0.623 0.650 0.677 0.704 0.729 0.754	0.11.1 0.199 0.245 0.287 0.326 0.363 0.432 0.465 0.497 0.528 0.558 0.587 0.615 0.696 0.722 0.747 0.794

N	<u>F</u>	C	<u>.500</u>	.800	<u>.900</u>	<u>•950</u>	<u>•990</u>	<u>• 995</u>
35	0 1 2 3 4 5 6 7 8 9 10 11 12 11 15 16 17 18 19 20 21		0.020 0.047 0.076 0.104 0.132 0.160 0.169 0.217 0.245 0.274 0.302 0.330 0.359 0.415 0.415 0.415 0.500 0.528 0.557 0.585 0.613	0.045 0.083 0.118 0.152 0.185 0.217 0.248 0.279 0.309 0.309 0.399 0.428 0.457 0.485 0.514 0.570 0.598 0.626 0.653 0.680	0.064 0.107 0.145 0.181 0.216 0.249 0.282 0.313 0.345 0.406 0.435 0.465 0.494 0.522 0.551 0.579 0.606 0.634 0.660 0.687 0.713	0.082 0.129 0.169 0.207 0.243 0.277 0.311 0.343 0.375 0.406 0.436 0.466 0.496 0.524 0.553 0.581 0.608 0.635 0.688 0.688 0.688	0.123 0.175 0.219 0.259 0.297 0.333 0.367 0.400 0.433 0.464 0.494 0.524 0.553 0.581 0.609 0.636 0.636 0.662 0.688 0.713 0.738 0.762	0.140 0.194 0.239 0.280 0.318 0.354 0.422 0.454 0.485 0.515 0.515 0.629 0.655 0.681 0.706 0.755 0.778
36	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21		0.019 0.046 0.074 0.101 0.129 0.156 0.184 0.211 0.239 0.266 0.294 0.321 0.349 0.349 0.376 0.404 0.431 0.459 0.459 0.569 0.596	0.044 0.081 0.115 0.148 0.180 0.211 0.241 0.271 0.301 0.330 0.359 0.388 0.417 0.445 0.473 0.501 0.528 0.556 0.583 0.610 0.637 0.663	0.062 0.104 0.141 0.176 0.210 0.242 0.274 0.305 0.366 0.366 0.395 0.424 0.453 0.481 0.509 0.537 0.564 0.591 0.618 0.618 0.615 0.671	0.740 0.080 0.125 0.165 0.202 0.236 0.270 0.303 0.334 0.365 0.125 0.1455 0.1455 0.1455 0.1455 0.1455 0.1455 0.1463 0.512 0.510 0.567 0.620 0.617 0.672 0.698 0.723	0.785 0.120 0.171 0.214 0.253 0.290 0.325 0.358 0.391 0.422 0.453 0.512 0.540 0.568 0.595 0.622 0.648 0.673 0.698 0.722 0.746 0.769	0.801 0.137 0.189 0.233 0.273 0.310 0.346 0.379 0.412 0.413 0.504 0.533 0.561 0.588 0.615 0.641 0.667 0.692 0.716 0.763 0.785

N	<u>F</u>	<u>c</u>	<u>.500</u>	.800	.900	<u>.950</u>	<u>.990</u>	<u>. 995</u>
37	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 22 22 22 22 22 22 22 22 22		0.019 0.045 0.072 0.098 0.125 0.152 0.179 0.205 0.232 0.259 0.286 0.313 0.366 0.313 0.366 0.420 0.446 0.473 0.500 0.527 0.554 0.580 0.607	0.043 0.079 0.112 0.114 0.175 0.205 0.235 0.264 0.293 0.350 0.378 0.406 0.434 0.461 0.461 0.515 0.568 0.595 0.621 0.647 0.673	0.060 0.101 0.138 0.172 0.205 0.236 0.267 0.298 0.327 0.357 0.385 0.414 0.442 0.470 0.497 0.524 0.551 0.577 0.604 0.629 0.655 0.680 0.705	0.078 0.122 0.161 0.196 0.231 0.263 0.295 0.326 0.356 0.386 0.415 0.415 0.472 0.500 0.527 0.554 0.580 0.606 0.632 0.657 0.682 0.707 0.730	0.117 0.166 0.208 0.247 0.283 0.317 0.350 0.382 0.412 0.472 0.500 0.528 0.555 0.582 0.608 0.659 0.683 0.707 0.754 0.776	0.133 0.184 0.227 0.266 0.303 0.337 0.371 0.402 0.433 0.463 0.492 0.521 0.548 0.575 0.602 0.627 0.653 0.677 0.701 0.725 0.748 0.770 0.792
38	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18		0.018 0.014 0.070 0.096 0.122 0.148 0.174 0.200 0.226 0.252 0.278 0.304 0.357 0.383 0.409 0.435 0.461 0.487	0.041 0.077 0.109 0.140 0.171 0.200 0.229 0.258 0.286 0.314 0.342 0.369 0.423 0.450 0.450 0.503 0.529 0.556	0.059 0.099 0.134 0.167 0.199 0.261 0.290 0.319 0.318 0.404 0.431 0.458 0.512 0.538 0.564 0.589	0.076 0.119 0.157 0.192 0.225 0.225 0.257 0.288 0.318 0.318 0.318 0.377 0.405 0.405 0.461 0.488 0.515 0.567 0.593 0.618	0.114 0.162 0.203 0.241 0.276 0.310 0.342 0.403 0.403 0.432 0.461 0.489 0.516 0.543 0.569 0.595 0.620 0.615 0.669	0.130 0.180 0.222 0.260 0.296 0.330 0.362 0.393 0.424 0.453 0.482 0.509 0.537 0.563 0.639 0.663 0.663

Ñ	<u>F</u>	<u>c</u>	.500	.800	<u>. 900</u>	<u>.950</u>	<u>. 990</u>	<u>. 995</u>
	19 20 21 22		0.513 0.539 0.565 0.591	0.580 0.606 0.631 0.657	0.615 0.640 0.665 0.689	0.643 0.667 0.691 0.715	0.693 0.716 0.739 0.761	0.710 0.733 0.755 0.777
39	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23		0.018 0.043 0.068 0.093 0.119 0.144 0.170 0.195 0.220 0.246 0.271 0.297 0.322 0.347 0.373 0.398 0.424 0.449 0.475 0.500 0.525 0.576 0.602	0.040 0.075 0.107 0.137 0.166 0.195 0.223 0.251 0.279 0.306 0.333 0.360 0.386 0.413 0.439 0.465 0.413 0.516 0.516 0.511 0.567 0.592 0.617 0.666	0.057 0.096 0.131 0.163 0.195 0.225 0.254 0.283 0.312 0.340 0.367 0.474 0.421 0.474 0.500 0.526 0.551 0.650 0.650 0.650 0.698	0.074 0.116 0.153 0.187 0.220 0.251 0.281 0.311 0.340 0.368 0.423 0.450 0.477 0.503 0.529 0.554 0.579 0.604 0.629 0.653 0.677 0.700 0.723	0.111 0.158 0.199 0.235 0.270 0.303 0.334 0.364 0.394 0.423 0.451 0.478 0.555 0.557 0.583 0.607 0.632 0.655 0.679 0.724 0.768	0.127 0.176 0.217 0.254 0.289 0.322 0.354 0.385 0.414 0.443 0.471 0.499 0.525 0.551 0.626 0.626 0.650 0.674 0.697 0.719 0.762 0.783
40	0 1 2 3 1 2 3 6 7 8 9 10		0.017 0.066 0.066 0.091 0.116 0.165 0.190 0.215 0.260	0.039 0.073 0.104 0.134 0.162 0.190 0.218 0.245 0.272 0.299 0.325	0.056 0.094 0.128 0.159 0.190 0.220 0.248 0.277 0.305 0.332 0.359	0.072 0.113 0.149 0.183 0.214 0.245 0.275 0.304 0.332 0.360 0.387	0.109 0.155 0.194 0.230 0.264 0.296 0.327 0.356 0.385 0.414	0.124 0.172 0.212 0.248 0.283 0.315 0.346 0.376 0.405 0.134 0.161

<u>N</u> .	F	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>•990</u>	<u>.995</u>
	11 12 13 14 15 16 17 18 19 20 21 22 23 24		0.289 0.314 0.339 0.364 0.388 0.413 0.438 0.463 0.463 0.512 0.562 0.587 0.612	0.351 0.377 0.403 0.429 0.454 0.479 0.504 0.529 0.554 0.678 0.627 0.627	0.385 0.412 0.438 0.463 0.489 0.514 0.539 0.563 0.588 0.612 0.636 0.659 0.683 0.706	0.414 0.440 0.466 0.492 0.517 0.542 0.567 0.615 0.639 0.662 0.685 0.708	0.1,68 0.1,91 0.520 0.516 0.570 0.595 0.619 0.665 0.665 0.710 0.732 0.751	0.488 0.514 0.540 0.565 0.590 0.614 0.637 0.661 0.683 0.705 0.727 0.748 0.769 0.790
'n	01234567891011213145161781920122324		0.017 0.041 0.065 0.089 0.113 0.137 0.161 0.186 0.210 0.258 0.258 0.262 0.306 0.331 0.355 0.379 0.403 0.403 0.427 0.403 0.427 0.452 0.500 0.524 0.549	0.038 0.071 0.101 0.130 0.159 0.186 0.213 0.240 0.266 0.292 0.318 0.343 0.369 0.394 0.419 0.468 0.493 0.517 0.565 0.589 0.636 0.659	0.055 0.092 0.125 0.156 0.186 0.215 0.270 0.298 0.351 0.377 0.402 0.453 0.478 0.502 0.575 0.575 0.598 0.622 0.645 0.668 0.691	0.070 0.111 0.146 0.178 0.210 0.239 0.269 0.297 0.325 0.352 0.379 0.405 0.431 0.456 0.481 0.506 0.531 0.555 0.579 0.602 0.626 0.619 0.671 0.694 0.716	0.106 0.151 0.190 0.225 0.258 0.289 0.320 0.319 0.377 0.405 0.432 0.458 0.484 0.510 0.531 0.559 0.583 0.607 0.630 0.652 0.675 0.697 0.718 0.710 0.760	0.121 0.168 0.207 0.243 0.276 0.308 0.339 0.368 0.397 0.424 0.452 0.478 0.504 0.529 0.554 0.602 0.625 0.648 0.670 0.692 0.735 0.755 0.776

<u>N</u>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	.990	. 995
<b>1</b> 42	01234567891011211561789201223145		0.016 0.040 0.063 0.087 0.110 0.134 0.158 0.205 0.228 0.276 0.299 0.346 0.370 0.346 0.370 0.441 0.465 0.488 0.559 0.583 0.606	0.038 0.070 0.099 0.127 0.155 0.182 0.260 0.265 0.311 0.360 0.365 0.365 0.458 0.458 0.505 0.529 0.576 0.576 0.599 0.645 0.668	0.053 0.089 0.122 0.152 0.181 0.210 0.237 0.264 0.291 0.317 0.368 0.394 0.413 0.467 0.492 0.515 0.539 0.563 0.699 0.677 0.699	0.068 0.108 0.142 0.174 0.204 0.234 0.262 0.290 0.317 0.314 0.370 0.396 0.421 0.495 0.519 0.513 0.566 0.589 0.612 0.635 0.657 0.679 0.701 0.723	0.104 0.148 0.185 0.220 0.252 0.283 0.313 0.341 0.369 0.423 0.449 0.474 0.499 0.524 0.548 0.571 0.595 0.617 0.640 0.705 0.726 0.746 0.767	0.119 0.164 0.203 0.238 0.271 0.302 0.332 0.361 0.389 0.416 0.443 0.468 0.494 0.519 0.567 0.567 0.567 0.636 0.636 0.658 0.679 0.701 0.722 0.762 0.782
43	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		0.016 0.039 0.062 0.085 0.108 0.131 0.154 0.177 0.200 0.223 0.246 0.269 0.292 0.315 0.338 0.362	0.037 0.068 0.097 0.125 0.151 0.178 0.203 0.229 0.254 0.279 0.328 0.352 0.376 0.400 0.424	0.052 0.087 0.119 0.149 0.177 0.205 0.232 0.259 0.285 0.310 0.335 0.360 0.385 0.409 0.434 0.458	0.067 0.106 0.139 0.171 0.200 0.229 0.257 0.284 0.311 0.337 0.362 0.388 0.413 0.437 0.461 0.485	0.102 0.145 0.181 0.215 0.247 0.277 0.306 0.334 0.362 0.388 0.414 0.440 0.465 0.489 0.513 0.537	0.116 0.160 0.198 0.233 0.265 0.291 0.325 0.353 0.408 0.434 0.459 0.484 0.509 0.532

N	F	<u>c</u>	<u>.500</u>	<u>.800</u>	<u>• 900</u>	<u>. 950</u>	<u>•990</u>	<u>. 995</u>
	16 17 18 19 20 21 22 23 24 25		0.385 0.408 0.431 0.454 0.477 0.500 0.523 0.546 0.569 0.592	0.448 0.471 0.494 0.518 0.541 0.564 0.586 0.609 0.631 0.654	0.481 0.505 0.528 0.551 0.574 0.596 0.619 0.641 0.663 0.685	0.509 0.532 0.555 0.578 0.601 0.623 0.645 0.667 0.688 0.709	0.560 0.583 0.606 0.628 0.650 0.671 0.692 0.713 0.733	0.579 0.602 0.624 0.646 0.667 0.688 0.709 0.729 0.749 0.768
ήή	012345678910112131451617819012222456		0.016 0.038 0.060 0.083 0.105 0.128 0.150 0.173 0.196 0.218 0.263 0.286 0.308 0.331 0.353 0.376 0.399 0.421 0.466 0.489 0.511 0.556 0.579 0.601	0.036 0.067 0.095 0.122 0.148 0.174 0.199 0.224 0.249 0.273 0.397 0.321 0.345 0.368 0.392 0.415 0.438 0.461 0.507 0.552 0.574 0.596 0.618 0.662	0.051 0.086 0.116 0.116 0.114 0.201 0.227 0.253 0.279 0.304 0.328 0.353 0.377 0.401 0.425 0.448 0.471 0.494 0.517 0.562 0.584 0.606 0.628 0.650 0.671 0.692	0.066 0.103 0.136 0.167 0.196 0.224 0.252 0.278 0.330 0.355 0.380 0.404 0.428 0.452 0.475 0.499 0.521 0.567 0.589 0.611 0.632 0.675 0.696 0.716	0.099 0.142 0.178 0.211 0.242 0.300 0.328 0.354 0.381 0.406 0.431 0.456 0.480 0.504 0.527 0.572 0.572 0.594 0.616 0.638 0.659 0.680 0.700 0.720 0.759	0.113 0.157 0.194 0.228 0.259 0.314 0.373 0.400 0.425 0.450 0.450 0.450 0.568 0.568 0.655 0.676 0.676 0.755 0.774

<u>N</u>	F	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>.950</u>	<u>. 990</u>	<u>•995</u>
145	012345678910112 1145678920 112131456178192012232452627		0.015 0.037 0.059 0.081 0.103 0.125 0.147 0.169 0.191 0.213 0.235 0.257 0.279 0.301 0.324 0.368 0.390 0.412 0.456 0.478 0.500 0.522 0.544 0.566 0.588 0.610	0.035 0.065 0.093 0.113 0.170 0.155 0.219 0.243 0.267 0.314 0.337 0.361 0.361 0.406 0.429 0.451 0.474 0.496 0.518 0.562 0.584 0.666 0.627 0.648 0.670	0.050 0.084 0.114 0.112 0.170 0.196 0.222 0.248 0.273 0.322 0.346 0.369 0.369 0.369 0.462 0.439 0.462 0.507 0.529 0.573 0.616 0.658 0.679 0.699	0.064 0.101 0.133 0.163 0.192 0.220 0.246 0.272 0.298 0.323 0.348 0.372 0.396 0.420 0.443 0.466 0.489 0.511 0.533 0.555 0.577 0.599 0.620 0.641 0.662 0.683 0.723	0.097 0.139 0.174 0.206 0.237 0.266 0.294 0.321 0.347 0.373 0.398 0.423 0.447 0.471 0.494 0.517 0.539 0.562 0.583 0.605 0.626 0.647 0.688 0.708 0.727 0.746 0.765	0.111 0.154 0.190 0.223 0.254 0.312 0.339 0.366 0.417 0.466 0.489 0.5135 0.558 0.558 0.664 0.664 0.703 0.743 0.761 0.780
46	0 1 2 3 4 5 6 7 8 9 10 11 12 13		0.015 0.036 0.058 0.079 0.101 0.122 0.111 0.166 0.107 0.209 0.230 0.252 0.273	0.034 0.064 0.091 0.117 0.142 0.166 0.191 0.215 0.238 0.262 0.285 0.308 0.330 0.353	0.049 0.082 0.112 0.140 0.166 0.192 0.218 0.243 0.267 0.291 0.315 0.339 0.362 0.385	0.063 0.099 0.131 0.160 0.188 0.215 0.241 0.267 0.292 0.317 0.365 0.388 0.411	0.095 0.136 0.170 0.202 0.232 0.261 0.288 0.315 0.341 0.366 0.391 0.415 0.439 0.462	0.109 0.151 0.186 0.219 0.249 0.278 0.306 0.333 0.359 0.369 0.409 0.433 0.457 0.457

<u>N</u>	£	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>• 950</u>	<u>. 990</u>	<u>. 995</u>
	14 15 16 17 18 19 20 21 22 23 24 25 26 27		0.317 0.338 0.360 0.381 0.403 0.424 0.446 0.468 0.489 0.511 0.532 0.554 0.576	0.376 0.398 0.420 0.444 0.464 0.508 0.529 0.551 0.572 0.593 0.615 0.636 0.656	0.408 0.430 0.452 0.475 0.497 0.518 0.561 0.583 0.604 0.625 0.645 0.666	0.434 0.457 0.479 0.501 0.523 0.545 0.566 0.587 0.608 0.629 0.650 0.670 0.690	0.485 0.507 0.529 0.551 0.573 0.594 0.615 0.635 0.656 0.676 0.695 0.715 0.734	0.503 0.526 0.548 0.569 0.591 0.612 0.632 0.653 0.672 0.711 0.730 0.749
47	012345678910112131451617319201222226278		0.015 0.035 0.056 0.078 0.099 0.120 0.162 0.183 0.204 0.225 0.247 0.268 0.289 0.310 0.352 0.373 0.352 0.373 0.458 0.479 0.563 0.563 0.563 0.563	0.034 0.062 0.089 0.114 0.139 0.163 0.163 0.210 0.233 0.256 0.279 0.301 0.324 0.346 0.368 0.390 0.412 0.433 0.455 0.476 0.498 0.519 0.561 0.582 0.602 0.623 0.664 0.664	0.048 0.080 0.109 0.137 0.163 0.188 0.213 0.238 0.262 0.285 0.309 0.332 0.355 0.377 0.399 0.422 0.444 0.465 0.465 0.508 0.551 0.571 0.508 0.653 0.653 0.653 0.653	0.062 0.097 0.128 0.157 0.184 0.211 0.237 0.262 0.286 0.310 0.358 0.381 0.403 0.426 0.448 0.470 0.492 0.513 0.556 0.577 0.618 0.638 0.658 0.678 0.697 0.717	0.093 0.133 0.167 0.198 0.228 0.256 0.283 0.309 0.334 0.359 0.359 0.407 0.430 0.453 0.407 0.498 0.520 0.563 0.664 0.6683 0.703 0.710 0.758	0.107 0.148 0.183 0.215 0.214 0.273 0.300 0.327 0.352 0.377 0.402 0.425 0.494 0.516 0.538 0.559 0.580 0.601 0.661 0.681 0.681 0.700 0.718 0.737 0.755 0.773

			*.				,	
<u>N</u>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>.990</u>	<u>.995</u>
18	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 26 27 28 28 28 29 29 29 29 29 29 29 29 29 29 29 29 29		0.014 0.035 0.055 0.076 0.097 0.117 0.138 0.179 0.200 0.221 0.262 0.283 0.303 0.324 0.345 0.366 0.407 0.428 0.469 0.490 0.510 0.552 0.572 0.593	0.033 0.061 0.087 0.112 0.136 0.160 0.183 0.206 0.229 0.251 0.273 0.295 0.317 0.339 0.361 0.382 0.404 0.425 0.445 0.467 0.488 0.509 0.550 0.570 0.591 0.631 0.651	0.047 0.079 0.107 0.134 0.160 0.185 0.209 0.233 0.257 0.280 0.303 0.325 0.348 0.370 0.392 0.414 0.435 0.456 0.478 0.499 0.561 0.561 0.661 0.661 0.681	0.061 0.095 0.125 0.154 0.181 0.207 0.232 0.257 0.281 0.304 0.328 0.351 0.373 0.396 0.418 0.4461 0.483 0.504 0.525 0.566 0.666 0.666 0.626 0.666 0.685 0.704	0.091 0.130 0.164 0.194 0.223 0.251 0.277 0.303 0.328 0.376 0.400 0.423 0.467 0.489 0.511 0.532 0.553 0.573 0.614 0.633 0.672 0.691 0.710 0.728 0.746	0:105 0:145 0:179 0:210 0:240 0:268 0:295 0:321 0:346 0:370 0:418 0:463 0:463 0:507 0:550 0:550 0:550 0:631 0:650 0:688 0:707 0:743 0:761
149	0 1 2 3 4 5 6 7 8 9 10		0.014 0.034 0.054 0.074 0.095 0.115 0.135 0.155 0.176 0.196 0.216	0.032 0.060 0.085 0.110 0.133 0.157 0.179 0.202 0.224 0.246 0.268	0.046 0.077 0.105 0.131 0.157 0.181 0.205 0.229 0.252 0.274	0.059 0.093 0.123 0.151 0.177 0.203 0.227 0.252 0.275 0.299	0.090 0.128 0.161 0.191 0.219 0.246 0.272 0.297 0.322 0.346 0.369	0.102 0.142 0.176 0.207 0.235 0.263 0.289 0.315 0.340 0.364

<u>N</u>	£	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>•990</u>	<u>•995</u>
	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29		0.237 0.257 0.277 0.297 0.318 0.338 0.358 0.378 0.399 0.419 0.439 0.459 0.459 0.500 0.500 0.520 0.561 0.561 0.581	0.290 0.311 0.333 0.354 0.375 0.396 0.417 0.458 0.479 0.499 0.519 0.539 0.560 0.580 0.600 0.619 0.639 0.659	0.319 0.363 0.363 0.384 0.406 0.427 0.448 0.469 0.489 0.510 0.530 0.550 0.570 0.590 0.610 0.630 0.649 0.668 0.688	0.344 0.366 0.388 0.410 0.432 0.453 0.474 0.515 0.536 0.556 0.556 0.576 0.635 0.635 0.635 0.673 0.692 0.711	0.392 0.415 0.437 0.459 0.481 0.502 0.523 0.543 0.563 0.603 0.603 0.623 0.642 0.661 0.680 0.698 0.716 0.734 0.752	0.410 0.433 0.455 0.477 0.498 0.520 0.540 0.561 0.601 0.620 0.639 0.658 0.677 0.695 0.714 0.731 0.749 0.766
50	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		0.014 0.033 0.053 0.073 0.093 0.113 0.133 0.152 0.172 0.192 0.212 0.232 0.252 0.272 0.291 0.311 0.351 0.351 0.371 0.391	0.032 0.059 0.084 0.108 0.131 0.154 0.176 0.198 0.220 0.241 0.263 0.284 0.305 0.326 0.347 0.368 0.368 0.388 0.409 0.429 0.449	0.045 0.076 0.103 0.129 0.154 0.201 0.224 0.247 0.269 0.291 0.313 0.335 0.356 0.377 0.398 0.419 0.460 0.460 0.480	0.058 0.091 0.121 0.148 0.174 0.199 0.223 0.247 0.270 0.293 0.316 0.338 0.360 0.381 0.403 0.403 0.405 0.465 0.465 0.486 0.506 0.526	0.088 0.126 0.158 0.187 0.215 0.212 0.267 0.292 0.316 0.340 0.363 0.408 0.408 0.451 0.472 0.493 0.514 0.554 0.574	0.101 0.139 0.173 0.203 0.231 0.258 0.204 0.309 0.333 0.357 0.380 0.403 0.425 0.447 0.469 0.511 0.531 0.551 0.591

<u>N</u>	F	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>•995</u>
	21 22 23 24 25 26 27 28 29 30		0.430 0.450 0.470 0.490 0.510 0.530 0.550 0.570 0.589 0.609	0.490 0.510 0.529 0.549 0.561 0.588 0.608 0.627 0.647 0.666	0.521 0.540 0.560 0.580 0.599 0.618 0.638 0.657 0.675	0.546 0.566 0.585 0.605 0.624 0.643 0.662 0.680 0.699	0.593 0.612 0.631 0.650 0.669 0.687 0.705 C.723 0.740	0.610 0.629 0.648 0.666 0.684 0.702 0.720 0.737 c.755 0.771
55	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		0.013 0.030 0.048 0.066 0.084 0.102 0.121 0.139 0.157 0.175 0.193 0.211 0.229 0.247 0.265 0.233	0.029 0.053 0.076 0.098 0.119 0.140 0.160 0.181 0.200 0.220 0.240 0.259 0.279 0.298 0.317 0.336	0.041 0.069 0.094 0.117 0.140 0.162 0.184 0.205 0.226 0.246 0.266 0.286 0.306 0.306 0.326	0.053 0.083 0.110 0.135 0.159 0.182 0.204 0.226 0.247 0.268 0.289 0.309 0.329 0.349 0.369 0.369 0.388	0.080 0.015 0.114 0.171 0.197 0.221 0.245 0.268 0.290 0.312 0.333 0.354 0.375 0.395 0.415 0.434	0.092 0.127 0.158 0.186 0.212 0.237 0.261 0.306 0.306 0.350 0.371 0.391 0.412 0.432 0.451
	16 17 18 19 20 21 22 23 24 25		0.301 0.319 0.337 0.355 0.373 0.391 0.409 0.428 0.446 0.464	0.355 0.373 0.392 0.411 0.429 0.41.7 0.466 0.484 0.502 0.520	0.383 0.402 0.421 0.440	0.408 0.427 0.446 0.465 0.483 0.502 0.520 0.538 0.556 0.574	0.1514 0.1473 0.1492 0.511 0.529 0.517 0.565 0.583 0.601 0.618	0.471 0.490 0.509 0.527 0.546 0.564 0.582 0.599 0.617 0.634

<u>N</u>	F	<u>C</u>	<u>. 500</u> .	.800	<u>. 900</u>	<u>.950</u>	. 990	.995
	21 22 23 24 25 26 27 28 29 30		0.430 0.450 0.470 0.490 0.510 0.530 0.550 0.570 0.589 0.609	0.490 0.510 0.529 0.549 0.561 0.588 0.608 0.627 0.647	0.521 0.540 0.560 0.580 0.599 0.618 0.638 0.657 0.675	0.546 0.566 0.585 0.605 0.621 0.662 0.680 0.699 0.717	0.593 0.612 0.631 0.650 0.669 0.687 0.705 0.723 0.740 0.757	0.610 0.629 0.648 0.666 0.684 0.702 0.720 0.737 0.755 0.771
55	0 1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 19 20 21 22 24 5		0.013 0.030 0.048 0.066 0.084 0.102 0.121 0.139 0.157 0.175 0.193 0.211 0.229 0.247 0.265 0.283 0.301 0.319 0.319 0.355 0.373 0.409 0.428 0.466 0.464	0.029 0.053 0.076 0.098 0.119 0.140 0.160 0.181 0.200 0.220 0.240 0.259 0.279 0.298 0.317 0.355 0.373 0.355 0.373 0.466 0.484 0.502 0.520	0.041 0.069 0.094 0.117 0.140 0.162 0.184 0.205 0.226 0.246 0.266 0.266 0.366 0.366 0.366 0.361 0.383 0.402 0.421 0.4495 0.459 0.459 0.550	0.053 0.083 0.110 0.135 0.159 0.182 0.206 0.247 0.268 0.268 0.289 0.349 0.349 0.369	0.080 0.015 0.114 0.171 0.197 0.221 0.245 0.268 0.290 0.312 0.375 0.375 0.434 0.454 0.454 0.454 0.454 0.451 0.529 0.565 0.583 0.601 0.618	0.092 0.127 0.158 0.186 0.212 0.237 0.261 0.306 0.328 0.350 0.371 0.432 0.451 0.451 0.471 0.490 0.509 0.527 0.564 0.582 0.599 0.517 0.634

<u>N</u>	F	<u>c</u>	.500	.800	<u>. 900</u>	<u>.950</u>	<u>•990</u>	<u>. 995</u>
	11 12 13 14 15 16 17 18 19 20 21 22 23 24		0.179 0.194 0.209 0.225 0.240 0.255 0.270 0.286 0.301 0.316 0.332 0.347 0.362 0.378 0.393	0.221 0.237 0.253 0.270 0.286 0.302 0.318 0.334 0.350 0.366 0.382 0.397 0.413 0.429 0.444	0.244 0.261 0.278 0.285 0.311 0.328 0.344 0.360 0.377 0.393 0.409 0.424 0.446 0.456 0.472	0.265 0.282 0.299 0.316 0.333 0.350 0.366 0.382 0.399 0.415 0.447 0.463 0.478 0.494	0.304 0.322 0.340 0.357 0.374 0.408 0.425 0.4425 0.441 0.457 0.457 0.473 0.489 0.505 0.536	0.319 0.337 0.355 0.373 0.390 0.407 0.424 0.440 0.457 0.473 0.489 0.505 0.521 0.536
70	01234567891011213456781901223245		0.010 0.024 0.038 0.052 0.066 0.081 0.095 0.109 0.123 0.137 0.152 0.166 0.180 0.194 0.209 0.223 0.237 0.251 0.265 0.280 0.322 0.337 0.351 0.365	0.023 0.042 0.060 0.077 0.094 0.111 0.127 0.143 0.159 0.174 0.190 0.205 0.221 0.236 0.251 0.266 0.281 0.266 0.311 0.326 0.311 0.356 0.370 0.385 0.399 0.414	0.032 0.054 0.074 0.093 0.111 0.128 0.146 0.162 0.179 0.195 0.212 0.228 0.213 0.259 0.275 0.290 0.306 0.306 0.351 0.366 0.361 0.366 0.381 0.366 0.111 0.425 0.440	0.042 0.066 0.087 0.107 0.126 0.144 0.162 0.180 0.197 0.214 0.230 0.247 0.263 0.279 0.295 0.311 0.326 0.342 0.357 0.372 0.388 0.403 0.418 0.4132 0.447 0.462	0.064 0.091 0.115 0.136 0.157 0.177 0.196 0.214 0.232 0.250 0.267 0.284 0.301 0.318 0.350 0.366 0.382 0.397 0.413 0.428 0.458 0.473 0.488 0.502	0.073 0.101 0.126 0.148 0.169 0.189 0.209 0.227 0.246 0.264 0.261 0.299 0.315 0.397 0.349 0.365 0.381 0.397 0.412 0.428 0.443 0.458 0.503 0.518

N	F	<u>C</u>	<u>.500</u>	<u>. 800</u>	<u>. 900</u>	<u>. 950</u>	<u>.990</u>	.995
75	0123456789101121145167189201222145		0.009 0.022 0.035 0.049 0.062 0.075 0.089 0.102 0.115 0.128 0.142 0.155 0.168 0.181 0.195 0.208 0.221 0.235 0.248 0.261 0.274 0.288 0.301 0.327 0.314	0.021 0.039 0.056 0.072 0.088 0.103 0.119 0.133 0.148 0.163 0.177 0.192 0.206 0.221 0.235 0.249 0.263 0.277 0.291 0.305 0.319 0.332 0.346 0.360 0.374 0.388	0.030 0.051 0.069 0.087 0.104 0.120 0.136 0.152 0.167 0.183 0.198 0.213 0.228 0.243 0.257 0.272 0.286 0.300 0.315 0.329 0.343 0.357 0.371 0.385 0.399 0.412	0.039 0.062 0.082 0.100 0.118 0.135 0.152 0.168 0.184 0.200 0.216 0.231 0.246 0.261 0.276 0.291 0.306 0.320 0.335 0.349 0.363 0.378 0.378 0.378 0.392 0.406 0.420 0.433	0.060 0.085 0.107 0.128 0.147 0.166 0.183 0.201 0.218 0.251 0.267 0.283 0.298 0.314 0.329 0.314 0.359 0.373 0.388 0.402 0.417 0.431 0.459 0.473	0.068 0.095 0.118 0.139 0.159 0.177 0.196 0.213 0.247 0.264 0.280 0.296 0.312 0.328 0.313 0.358 0.373 0.388 0.402 0.417 0.431 0.446 0.460 0.474 0.487
80	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		0.009 0.021 0.033 0.046 0.058 0.071 0.083 0.095 0.108 0.120 0.133 0.115 0.158 0.170 0.183 0.195	0.020 0.037 0.053 0.068 0.083 0.097 0.111 0.125 0.139 0.153 0.167 0.180 0.194 0.207 0.221	0.028 0.048 0.065 0.082 0.097 0.113 0.128 0.143 0.157 0.172 0.186 0.200 0.214 0.228 0.242 0.256	0.037 0.058 0.077 0.094 0.111 0.127 0.143 0.158 0.173 0.188 0.203 0.217 0.232 0.216 0.260 0.274	0.056 0.080 0.101 0.120 0.138 0.156 0.173 0.189 0.205 0.221 0.236 0.251 0.266 0.281 0.295 0.310	0.064 0.089 0.111 0.131 0.149 0.167 0.184 0.201 0.217 0.233 0.249 0.264 0.279 0.294 0.309 0.323

N	£	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>. 990</u>	<u>.995</u>
	16 17 18 19 20 21 22 23 24 25		0.207 0.220 0.232 0.245 0.257 0.270 0.282 0.295 0.307 0.320	0.247 0.260 0.273 0.287 0.300 0.313 0.326 0.338 0.351 0.364	0.269 0.283 0.296 0.309 0.323 0.336 0.319 0.362 0.375 0.388	0.288 0.302 0.315 0.329 0.342 0.356 0.369 0.382 0.395 0.408	0.324 0.338 0.352 0.366 0.380 0.393 0.407 0.420 0.433 0.446	0.338 0.352 0.366 0.380 0.394 0.407 0.421 0.434 0.447
85	012345678910123156789012223		0.008 0.020 0.031 0.043 0.055 0.066 0.078 0.090 0.102 0.113 0.125 0.137 0.118 0.160 0.172 0.184 0.160 0.172 0.184 0.195 0.207 0.219 0.230 0.242 0.254 0.266 0.277	0.019 0.035 0.050 0.064 0.079 0.105 0.105 0.118 0.157 0.170 0.183 0.195 0.208 0.221 0.233 0.245 0.258 0.270 0.283 0.295 0.307 0.319	0.027 0.045 0.061 0.077 0.092 0.106 0.121 0.135 0.148 0.162 0.175 0.189 0.202 0.215 0.28 0.215 0.267 0.279 0.292 0.305 0.317 0.330 0.342	0.035 0.055 0.072 0.089 0.104 0.120 0.135 0.149 0.163 0.177 0.191 0.205 0.219 0.232 0.245 0.259 0.272 0.285 0.298 0.311 0.323 0.349 0.361	0.053 0.076 0.095 0.113 0.147 0.163 0.178 0.194 0.208 0.223 0.237 0.252 0.266 0.279 0.266 0.279 0.306 0.320 0.333 0.346 0.359 0.372 0.385 0.398	0.060 0.084 0.105 0.123 0.141 0.158 0.174 0.190 0.205 0.235 0.250 0.264 0.278 0.320 0.320 0.333 0.346 0.360 0.373 0.386 0.398 0.411
	21 <sub>1</sub> 25		0.289	0.331 0.344	0.354	0.374	0.410	0.424

N	F	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>. 9</u> 00	<u>. 950</u>	<u>.990</u>	995
90	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25		0.008 0.019 0.030 0.041 0.052 0.063 0.074 0.085 0.096 0.107 0.118 0.129 0.140 0.151 0.162 0.173 0.185 0.196 0.207 0.218 0.209 0.240 0.251 0.262 0.273 0.284	0.018 0.033 0.047 0.060 0.074 0.086 0.099 0.112 0.124 0.136 0.149 0.161 0.173 0.185 0.197 0.209 0.220 0.232 0.244 0.256 0.279 0.290 0.302 0.302 0.314 0.325	0.025 0.043 0.058 0.073 0.087 0.101 0.114 0.127 0.140 0.153 0.166 0.179 0.191 0.204 0.216 0.228 0.240 0.252 0.265 0.276 0.288 0.300 0.312 0.324 0.336 0.347	0.033 0.052 0.068 0.084 0.099 0.113 0.127 0.141 0.155 0.168 0.181 0.207 0.220 0.232 0.245 0.257 0.270 0.282 0.294 0.306 0.318 0.330 0.342 0.354 0.366	0.050 0.071 0.090 0.107 0.124 0.139 0.154 0.169 0.183 0.198 0.211 0.225 0.238 0.252 0.265 0.278 0.291 0.303 0.316 0.328 0.311 0.353 0.365 0.377 0.389 0.401	0.057 0.080 0.099 0.117 0.133 0.149 0.165 0.180 0.195 0.209 0.223 0.237 0.250 0.264 0.277 0.290 0.303 0.316 0.329 0.341 0.366 0.378 0.391 0.403 0.415
95	0 1 2 3 4 5 6 7 8 9 10		0.007 0.018 0.028 0.039 0.019 0.059 0.070 0.080 0.091 0.101 0.112	0.017 0.031 0.045 0.057 0.070 0.082 0.094 0.106 0.118 0.129 0.141	0.024 0.040 0.055 0.069 0.082 0.095 0.108 0.121 0.133 0.145 0.158	0.031 0.049 0.065 0.080 0.094 0.107 0.121 0.134 0.147 0.159	0.047 0.068 0.086 0.102 0.117 0.132 0.147 0.161 0.174 0.188 0.201	0.054 0.076 0.094 0.111 0.127 0.142 0.157 0.171 0.185 0.199 0.212

N	<u>F</u>	<u>c</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>.995</u>
	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25		0.122 0.133 0.143 0.154 0.164 0.175 0.185 0.196 0.206 0.217 0.227 0.238 0.248 0.259 0.269	0.152 0.164 0.175 0.187 0.198 0.209 0.220 0.231 0.243 0.254 0.265 0.275 0.287 0.298 0.309	0.170 0.181 0.193 0.205 0.217 0.228 0.240 0.251 0.263 0.274 0.285 0.296 0.308 0.319 0.330	0.184 0.197 0.209 0.221 0.233 0.245 0.268 0.268 0.280 0.391 0.302 0.314 0.325 0.337 0.348	0.214 0.227 0.239 0.252 0.264 0.276 0.289 0.301 0.312 0.324 0.336 0.348 0.359 0.371 0.382	0.225 0.238 0.251 0.264 0.276 0.288 0.301 0.313 0.325 0.337 0.349 0.360 0.372 0.383 0.395
100	012345678910112314561781902122345		0.007 0.017 0.027 0.037 0.047 0.057 0.066 0.076 0.086 0.106 0.116 0.126 0.136 0.146 0.156 0.166 0.176 0.186 0.196 0.206 0.216 0.226 0.226 0.236 0.246 0.256	0.016 0.030 0.012 0.0514 0.066 0.078 0.089 0.101 0.112 0.123 0.134 0.145 0.156 0.167 0.177 0.188 0.199 0.210 0.220 0.231 0.252 0.262 0.273 0.283 0.294	0.023 0.038 0.052 0.066 0.078 0.091 0.103 0.115 0.127 0.138 0.150 0.161 0.173 0.184 0.195 0.206 0.217 0.228 0.239 0.250 0.261 0.271 0.282 0.293 0.303 0.314	0.030 0.047 0.062 0.076 0.089 0.102 0.115 0.127 0.140 0.152 0.164 0.176 0.187 0.199 0.210 0.222 0.233 0.214 0.255 0.266 0.277 0.288 0.299 0.310 0.321 0.331	0.045 0.065 0.081 0.097 0.112 0.126 0.140 0.153 0.166 0.179 0.191 0.204 0.216 0.228 0.240 0.252 0.263 0.275 0.263 0.275 0.287 0.298 0.309 0.309 0.320 0.332 0.343 0.365	0.052 0.072 0.089 0.105 0.121 0.135 0.149 0.163 0.176 0.189 0.202 0.215 0.227 0.239 0.251 0.263 0.275 0.287 0.298 0.310 0.321 0.355 0.366 0.377

<u>N</u>	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>.995</u>
	26 27 28 29 31 33 31 35 37 38 39 41 42 41 44 45 45 45 45 45 45 46 47 48 49 40 40 40 40 40 40 40 40 40 40 40 40 40		0.266 0.276 0.286 0.296 0.306 0.316 0.326 0.336 0.355 0.375 0.375 0.395 0.415 0.425 0.425 0.425 0.425 0.425 0.455 0.455 0.455	0.304 0.314 0.325 0.335 0.345 0.356 0.366 0.366 0.406 0.417 0.427 0.427 0.437 0.457 0.457 0.457 0.457 0.457 0.527 0.537 0.537	0.325 0.335 0.346 0.356 0.366 0.377 0.387 0.408 0.418 0.428 0.438 0.449 0.459 0.469 0.469 0.479 0.499 0.509 0.519 0.519 0.559 0.559	0.342 0.353 0.363 0.374 0.384 0.395 0.405 0.415 0.426 0.436 0.4467 0.467 0.467 0.467 0.467 0.467 0.507 0.507 0.517 0.527 0.557 0.567	0.375 0.386 0.397 0.408 0.418 0.429 0.439 0.450 0.460 0.470 0.481 0.501 0.511 0.521 0.531 0.531 0.551 0.561 0.561 0.571 0.581 0.590 0.600 0.610 0.619	0.388 0.399 0.409 0.420 0.431 0.452 0.462 0.462 0.493 0.503 0.534 0.553 0.534 0.553 0.563 0.573 0.563 0.563 0.602 0.622 0.631
110	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		0.006 0.015 0.024 0.033 0.042 0.051 0.060 0.070 0.079 0.087 0.097 0.106 0.115 0.124 0.133 0.142	0.015 0.027 0.038 0.050 0.060 0.071 0.081 0.092 0.102 0.122 0.122 0.132 0.142 0.152 0.162 0.162	0.021 0.035 0.048 0.060 0.071 0.083 0.094 0.105 0.115 0.126 0.137 0.147 0.157 0.168 0.178 0.188	0.027 0.042 0.056 0.069 0.081 0.093 0.105 0.116 0.127 0.138 0.149 0.160 0.171 0.181 0.192 0.202	0.041 0.059 0.074 0.088 0.102 0.115 0.127 0.140 0.152 0.163 0.175 0.186 0.197 0.208 0.219 0.230	0.047 0.066 0.082 0.096 0.110 0.123 0.136 0.149 0.161 0.173 0.185 0.196 0.208 0.219 0.230 0.241

<u>N</u>	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>•990</u>	<u>. 995</u>
N	16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 33 33 35 36 37 38 39 40 41 42 42 42 42 42 42 42 42 42 42 42 42 42		0.151 0.160 0.169 0.178 0.187 0.196 0.205 0.215 0.224 0.251 0.260 0.269 0.278 0.287 0.296 0.305 0.314 0.350 0.360 0.360 0.369 0.378 0.387	.800 0.181 0.191 0.201 0.210 0.220 0.229 0.239 0.249 0.258 0.268 0.277 0.286 0.296 0.305 0.315 0.315 0.324 0.333 0.343 0.352 0.361 0.371 0.380 0.389 0.398 0.408 0.417 0.426	.900 0.198 0.208 0.218 0.228 0.238 0.248 0.257 0.267 0.277 0.287 0.296 0.306 0.315 0.305 0.325 0.335 0.315 0.363 0.372 0.382 0.391 0.410 0.419 0.428 9,438 0.417	0.213 0.223 0.223 0.233 0.243 0.253 0.263 0.273 0.283 0.303 0.313 0.322 0.351 0.361 0.361 0.380 0.389 0.389 0.408 0.418 0.427 0.436 0.418	-990 0.241 0.252 0.262 0.262 0.273 0.283 0.293 0.303 0.314 0.324 0.334 0.354 0.364 0.373 0.364 0.373 0.405 0.422 0.431 0.450 0.460 0.469 0.469 0.488 0.497	995 0.262 0.365 0.
	43 44 45 46 47 48 49 50		0.396 0.405 0.414 0.423 0.432 0.445 0.450 0.459	0.435 0.444 0.454 0.463 0.472 0.481 0.490 0.499	0.456 0.465 0.475 0.484 0.493 0.502 0.511 0.520	0.474 0.483 0.492 0.501 0.510 0.519 0.528 0.537	0.506 0.515 0.524 0.533 0.543 0.552 0.561 0.569	0.518 0.527 0.536 0.545 0.554 0.563 0.572 0.581
120	0 1 2 3 4 5		0.006 0.014 0.022 0.031 0.038 0.047	0.013 0.025 0.035 0.045 0.055 0.065	0.019 0.032 0.014 0.055 0.066 0.076	0.025 0.039 0.052 0.063 0.075 0.086	0.038 0.054 0.068 0.081 0.094 0.106	0.043 0.060 0.075 0.088 0.101 0.113

				•				
<u>N</u>	<u>F</u>	. <u>Č</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
•	6		0.055	0.075	0.086	0.096	0.117	0.125
	7		0.064	0.084	0.096	0.107	0.128	0.137
	8		0.072	0.093	0.107	0.117	0.139	0.148
	9		0.080	0.103	0.116	0.127	0.150	0.159
	10		0.089	0.112	0.125	0.137	0.161	0.170
	11 ·		0.097	0.121	0.135	0.147	0.171	0.181
	12	,	0.105	0.130	0.145	0.157	0.182	0.191
	13		0.114	0.139	0.154	0.167	0.192	0.202
	14	•	0.122	0.148	0.163	0.176	0.202	0.212
	15		0.130	0.157	0.173	0.186	0.212	0.222
	16		0.139	0.166	0.182	0.195	0.222	0.232
	17		0.147	0.175	0.191	0.205	0.232	0.242
	18,		0.155	0.184	0.200	0.214	0.241	0.252
	19		0.163	0.193	0.210	0.224	0.251	0.262
	20		0.172	0.202	0.219	0.233	0.261	0.271
	21		0.180	0.211	0.228	0.242	0.270	0.281
	22		0.188	0.220	0.237	0.251	0.280	0.290
•	. 23		0.197	0.228	0.246	0.260	0.289	<b>0.3</b> 00
	5Ħ		0.205	0.237	0.255	0.270	0.298	0.309
	25		0.213	0.5/16	0.264	0.279	0.308	0.319
	26		0.222	0.254	0.272	0.288	0.317	0.328
	27		0.230	0.263	0.281	0.297	0.326	0.337
	28		0.238	0.272	0.290	0.306	0.335	0.346
	29		0.247	0.281	0.299	0.315	0- 3ليلا	0.356
	30		0.255	0.289	0.308	0.323	0.354	0.365
	31		0.263	0.298	0.317	0.332	0.363	0.374
	. 32		0.271	0.306	0.325	0.341	0.372	0.383
	33		0.280	0.315	0.334	0.350	0 <b>.3</b> 80	0.392
	1 3ft		0.288	0.324	0.343	0.359	0.389	0.401
	35 36		0.296	0.332	0.351	0.368	0.398	0.410
	37		0.305	0.341	0.360	0.376	0.407	0.418
•	38 ·	•	0.313	0.349	0.369	0.385	0.416	0.427
	39		0.321	0.358	0.377	0.394	0.425	0.436
	10		0.330 0.338	0.366	0.386	0.402	0.433	0.445
	41		0.346	0.375	0.394	0.411	0.1415	0.453
	412		0.355	10.383	0.403 0.412	0.419	0.451	0.462
	43	•	0.363	0.392 0.400	0.412	0.428	0.459	0.471
	ر با ارارا		0.371	0.400	0.429	0.437 0.445	0.468 0.476	0.479
	145 145		0.380	0.417	0.427	0.454	0.475	0.488
	46		0.388	0.426	0.416	0.462		0.496 0.505
•	47		0.396	0.434	0.454	0.402	0.493 0.502	0.505
	48		6.404	0.142	0.462	0.471	0.502	0.522
	49		0.412	0.151	0.471	0.479	0.510	0.522
	50		0.421	0.459	0.1479	0.407 0.496	0.527	
	, ,		~ · · · · ·	COR MAJOR A	0.417	0.470	い・フェイ	0.538

N	<u>F</u>	<u>c</u>	.500	.800	<u>.900</u>	<u>. 950</u>	<u>• 990</u>	<u>. 995</u>
<u>N</u> 130	01234567891011213156789012234567890132	<u>C</u>	0.005 0.013 0.021 0.028 0.036 0.044 0.051 0.059 0.067 0.074 0.082 0.090 0.097 0.105 0.113 0.120 0.128 0.136 0.143 0.151 0.159 0.166 0.174 0.182 0.189 0.197 0.205 0.212 0.220 0.228 0.235 0.251	0.012 0.023 0.033 0.042 0.051 0.060 0.069 0.078 0.086 0.095 0.104 0.120 0.129 0.137 0.146 0.154 0.154 0.178 0.178 0.178 0.178 0.178 0.195 0.203 0.211 0.219 0.227 0.235 0.251 0.251 0.251 0.267 0.275 0.283	0.018 0.030 0.040 0.051 0.061 0.070 0.080 0.089 0.098 0.107 0.116 0.125 0.134 0.142 0.151 0.160 0.168 0.177 0.185 0.194 0.202 0.211 0.219 0.227 0.236 0.244 0.252 0.260 0.269 0.277 0.285 0.293 0.301	0.023 0.036 0.048 0.059 0.069 0.079 0.089 0.108 0.118 0.127 0.136 0.145 0.154 0.163 0.172 0.181 0.190 0.198 0.207 0.216 0.224 0.233 0.211 0.250 0.258 0.267 0.275 0.283 0.291 0.300 0.308 0.315	0.035 0.050 0.063 0.075 0.087 0.098 0.108 0.119 0.129 0.139 0.149 0.159 0.168 0.178 0.168 0.178 0.206 0.215 0.224 0.233 0.242 0.251 0.259 0.268 0.277 0.268 0.277 0.268 0.277 0.268 0.277 0.286 0.294 0.303 0.311 0.320 0.328 0.337 0.345	0.040 0.056 0.069 0.082 0.094 0.105 0.116 0.127 0.137 0.147 0.157 0.167 0.167 0.167 0.196 0.206 0.215 0.224 0.243 0.252 0.261 0.269 0.278 0.261 0.269 0.278 0.305 0.313 0.322 0.330 0.338 0.347 0.355
	32	-	0.251	0.283 0.291	0.309	0.324	0.353	0.363
	33 34 35 36 37 38 39	,	0.266 0.274 0.281 0.289 0.297 0.304	0.299 0.307 0.315 0.323 0.331 0.339	0.317 0.325 0.333 0.341 0.349 0.357	0.333 0.341 0.349 0.357 0.365 0.373	0.362 0.370 0.378 0.386 0.394 0.403	0.372 0.380 0.388 0.397 0.405 0.413
	40		0.312	0.347	0.365	0.381	0.411	0.421

N	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>• 950</u>	<u>• 990</u>	<u>•995</u>
	41 42 43 44 45 46 47 48 49 50		0.320 0.327 0.335 0.343 0.350 0.358 0.366 0.373 0.381 0.389	0.355 0.363 0.370 0.378 0.386 0.394 0.402 0.409 0.417 0.425	0.373 0.381 0.389 0.397 0.405 0.413 0.421 0.429 0.436 0.444	0.389 0.397 0.405 0.413 0.421 0.429 0.437 0.444 0.452 0.460	0.419 0.427 0.435 0.443 0.451 0.459 0.467 0.474 0.482 0.490	0.429 0.437 0.445 0.453 0.461 0.469 0.477 0.485 0.493 0.501
140	012345678910112131456178920122345678930		0.005 0.012 0.019 0.026 0.033 0.040 0.055 0.062 0.069 0.076 0.083 0.090 0.097 0.105 0.112 0.119 0.126 0.133 0.140 0.147 0.154 0.162 0.169 0.176 0.183 0.190 0.197 0.204 0.211 0.219	0.011 0.021 0.030 0.039 0.048 0.056 0.064 0.072 0.080 0.088 0.096 0.104 0.112 0.120 0.128 0.135 0.143 0.151 0.158 0.166 0.174 0.181 0.189 0.196 0.204 0.211 0.219 0.226 0.234 0.241 0.219	0.016 0.027 0.038 0.047 0.056 0.056 0.065 0.074 0.083 0.091 0.100 0.108 0.116 0.124 0.133 0.141 0.149 0.157 0.165 0.173 0.180 0.188 0.196 0.204 0.212 0.250 0.250 0.258 0.265	0.021 0.033 0.044 0.054 0.064 0.074 0.083 0.092 0.101 0.110 0.118 0.127 0.135 0.144 0.152 0.160 0.168 0.177 0.185 0.192 0.201 0.209 0.217 0.225 0.201 0.209 0.217 0.225 0.218 0.256 0.264 0.272 0.279	0.032 0.046 0.059 0.070 0.081 0.091 0.101 0.120 0.130 0.139 0.148 0.157 0.166 0.174 0.183 0.192 0.200 0.209 0.217 0.225 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.266 0.274 0.282 0.298 0.298 0.306	0.037 0.052 0.065 0.076 0.087 0.098 0.108 0.118 0.128 0.137 0.147 0.156 0.165 0.174 0.183 0.192 0.200 0.209 0.218 0.226 0.235 0.243 0.251 0.260 0.268 0.276 0.284 0.292 0.300 0.308 0.316

N	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>•995</u>
	31 32 33 35 36 37 38 39 41 41 41 41 41 41 41 41 41 41 41 41 41		0.226 0.233 0.240 0.247 0.254 0.261 0.268 0.276 0.283 0.290 0.297 0.304 0.311 0.318 0.325 0.333 0.340 0.347 0.354 0.361	0.256 0.264 0.271 0.278 0.286 0.293 0.301 0.308 0.315 0.323 0.337 0.345 0.352 0.359 0.367 0.367 0.381 0.388 0.396	0.273 0.280 0.288 0.296 0.303 0.311 0.318 0.325 0.333 0.340 0.348 0.355 0.363 0.370 0.377 0.385 0.392 0.399 0.407 0.414	0.287 0.295 0.302 0.310 0.317 0.325 0.333 0.340 0.348 0.355 0.363 0.370 0.378 0.385 0.385 0.392 0.400 0.407 0.414 0.422 0.429	0.314 0.322 0.330 0.337 0.345 0.353 0.361 0.368 0.376 0.383 0.391 0.398 0.406 0.414 0.421 0.428 0.436 0.4451 0.458	0.324 0.332 0.340 0.348 0.355 0.363 0.371 0.379 0.386 0.394 0.401 0.409 0.417 0.424 0.432 0.439 0.446 0.461 0.469
150	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		0.005 0.011 0.018 0.024 0.031 0.038 0.044 0.051 0.058 0.064 0.071 0.078 0.084 0.091 0.098 0.104 0.111 0.118 0.124 0.131 0.137	0.011 0.020 0.028 0.036 0.044 0.052 0.060 0.067 0.075 0.082 0.090 0.097 0.105 0.112 0.119 0.126 0.134 0.141 0.141 0.148 0.155 0.162	0.015 0.026 0.035 0.044 0.053 0.061 0.069 0.077 0.085 0.093 0.101 0.109 0.116 0.124 0.131 0.139 0.146 0.154 0.161 0.169 0.176	0.020 0.031 0.041 0.051 0.060 0.069 0.077 0.086 0.094 0.102 0.110 0.118 0.126 0.134 0.142 0.150 0.157 0.165 0.173 0.180 0.188	0.030 0.043 0.055 0.065 0.075 0.085 0.094 0.104 0.112 0.121 0.130 0.138 0.147 0.155 0.163 0.171 0.179 0.187 0.195 0.203 0.211	0.035 0.048 0.060 0.071 0.082 0.091 0.131 0.120 0.128 0.128 0.155 0.163 0.171 0.180 0.188 0.196 0.204 0.212

<u>N</u>	£	C	<u>.500</u>	.800	<u>.900</u>	<u>. 950</u>	.990	<u>• 995</u>
	21 22 23 24 25 26 27 28 29 33 33 33 33 33 33 44 44 45 46 78 49 49		0.114 0.151 0.157 0.164 0.171 0.177 0.184 0.191 0.197 0.204 0.211 0.217 0.224 0.231 0.251 0.257 0.264 0.271 0.277 0.264 0.277 0.284 0.290 0.297 0.310 0.317 0.324 0.330	0.169 0.176 0.183 0.191 0.198 0.205 0.212 0.219 0.226 0.233 0.246 0.253 0.260 0.267 0.274 0.281 0.288 0.295 0.302 0.309 0.315 0.322 0.329 0.336 0.356 0.356 0.363	0.183 0.191 0.196 0.205 0.212 0.220 0.227 0.241 0.248 0.255 0.262 0.269 0.269 0.276 0.283 0.291 0.298 0.305 0.311 0.318 0.325 0.311 0.318 0.325 0.339 0.316 0.353 0.360 0.367 0.373 0.381	0.195 0.203 0.210 0.218 0.225 0.232 0.240 0.261 0.269 0.276 0.283 0.290 0.297 0.304 0.311 0.318 0.326 0.333 0.340 0.347 0.354 0.361 0.368 0.374 0.381 0.388 0.395	0.21.9 0.22.7 0.23.4 0.24.2 0.24.9 0.25.7 0.26.5 0.27.2 0.27.9 0.28.7 0.29.4 0.30.2 0.30.2 0.30.3 0.31.6 0.32.4 0.33.1 0.35.2 0.36.0 0.36.7 0.36.0 0.36.7 0.36.0 0.36.7 0.36.0 0.36.7 0.36.0 0.36.7 0.36.0 0.36.7 0.36.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.228 0.236 0.213 0.251 0.259 0.266 0.274 0.281 0.289 0.296 0.304 0.311 0.319 0.326 0.333 0.341 0.348 0.355 0.362 0.377 0.384 0.391 0.398 0.405 0.419 0.426 0.433
160	50 ·		0.337	0.370	0.387	0.402	0.430	0.1710
100	1 2 3 4 5		0.004 0.010 0.017 0.023 0.029 0.035	0.010 0.019 0.027 0.034 0.042 0.049	0.014 0.024 0.033 0.041 0.049	0.019 0.029 0.039 0.048 0.056 0.065	0.028 0.011 0.051 0.061 0.071 0.080	0.033 0.046 0.057 0.067 0.077 0.086

6	N	<u>F</u>	· <u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>.990</u>	.925
8 0.05¼ 0.070 0.080 0.088 0.106 0.112 9 0.060 0.077 0.087 0.096 0.11¼ 0.121 10 0.067 0.08½ 0.095 0.10¼ 0.122 0.129 11 0.073 0.091 0.102 0.111 0.130 0.137 12 0.079 0.098 0.109 0.119 0.138 0.1½5 13 0.085 0.105 0.116 0.126 0.1¼6 0.153 1¼ 0.091 0.112 0.123 0.133 0.153 0.161 15 0.098 0.119 0.130 0.1¼1 0.161 0.169 16 0.10¼ 0.125 0.137 0.1¼8 0.169 0.177 17 0.110 0.132 0.1¼¼ 0.155 0.176 0.18¼ 18 0.166 0.139 0.151 0.162 0.13¼ 0.192 19 0.123 0.1¼6 0.158 0.169 0.191 0.192 19 0.123 0.1¼6 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.21¼ 22 0.1¼1 0.166 0.179 0.190 0.213 0.222 23 0.1¼8 0.172 0.186 0.197 0.220 0.229 2½ 0.15¼ 0.15½ 0.159 0.193 0.20¼ 0.227 0.236			•						
9 0.060 0.077 0.087 0.096 0.114 0.121 10 0.067 0.084 0.095 0.104 0.122 0.129 11 0.073 0.091 0.102 0.111 0.130 0.137 12 0.079 0.098 0.109 0.119 0.138 0.145 13 0.085 0.105 0.116 0.126 0.146 0.153 14 0.091 0.112 0.123 0.133 0.153 0.161 15 0.098 0.119 0.130 0.141 0.161 0.169 16 0.104 0.125 0.137 0.148 0.169 0.177 17 0.110 0.132 0.144 0.155 0.176 0.184 18 0.166 0.139 0.151 0.162 0.184 0.192 19 0.123 0.146 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236		7	•						
10 0.067 0.08\(\psi\$ 0.095 0.10\(\psi\$ 0.122 0.129\) 11 0.073 0.091 0.102 0.111 0.130 0.137\) 12 0.079 0.098 0.109 0.119 0.138 0.1\(\psi\$ 13 0.085 0.105 0.116 0.126 0.1\(\psi\$ 6 0.15\) 14 0.091 0.112 0.123 0.133 0.153 0.161\) 15 0.098 0.119 0.130 0.1\(\psi\$ 1 0.161 0.169\) 16 0.10\(\psi\$ 0.125 0.137 0.1\(\psi\$ 8 0.169 0.177\) 17 0.110 0.132 0.1\(\psi\$ 1 0.155 0.176 0.18\(\psi\$ 18 0.166 0.139 0.151 0.162 0.18\(\psi\$ 19 0.123 0.123 0.146 0.158 0.169 0.191 0.192\) 19 0.123 0.1\(\psi\$ 6 0.158 0.169 0.191 0.199\) 20 0.129 0.152 0.165 0.176 0.198 0.207\) 21 0.135 0.159 0.172 0.183 0.206 0.21\(\psi\$ 22 0.1\(\psi\$ 1 0.166 0.179 0.190 0.213 0.222\) 23 0.1\(\psi\$ 8 0.172 0.186 0.197 0.220 0.229\) 2\(\psi\$ 0.15\(\psi\$ 0.179 0.193 0.20\(\psi\$ 0.227 0.236\)		Ö							
11 0.073 0.091 0.102 0.111 0.130 0.137 12 0.079 0.098 0.109 0.119 0.138 0.145 13 0.085 0.105 0.116 0.126 0.146 0.153 14 0.091 0.112 0.123 0.133 0.153 0.161 15 0.098 0.119 0.130 0.141 0.161 0.169 16 0.104 0.125 0.137 0.148 0.169 0.177 17 0.110 0.132 0.144 0.155 0.176 0.184 18 0.166 0.139 0.151 0.162 0.184 0.192 19 0.123 0.146 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236	•								
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14 0.091 0.112 0.123 0.133 0.153 0.161 15 0.098 0.119 0.130 0.141 0.161 0.169 16 0.104 0.125 0.137 0.148 0.169 0.177 17 0.110 0.132 0.144 0.155 0.176 0.184 18 0.166 0.139 0.151 0.162 0.184 0.192 19 0.123 0.146 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236									
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17 0.110 0.132 0.144 0.155 0.176 0.184 18 0.166 0.139 0.151 0.162 0.184 0.192 19 0.123 0.146 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236		16							
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19 0.123 0.146 0.158 0.169 0.191 0.199 20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236									
20 0.129 0.152 0.165 0.176 0.198 0.207 21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236									
21 0.135 0.159 0.172 0.183 0.206 0.214 22 0.141 0.166 0.179 0.190 0.213 0.222 23 0.148 0.172 0.186 0.197 0.220 0.229 24 0.154 0.179 0.193 0.204 0.227 0.236									
22 0.1\(\bar{1}\) 0.166 0.179 0.190 0.213 0.222 23 0.1\(\bar{1}\)8 0.172 0.186 0.197 0.220 0.229 2\(\bar{1}\) 0.15\(\bar{1}\) 0.179 0.193 0.20\(\bar{1}\) 0.227 0.236									
23 0.11/8 0.172 0.186 0.197 0.220 0.229 21/4 0.151/4 0.179 0.193 0.201/4 0.227 0.236									
24 0.154 0.179 0.193 0.204 0.227 0.236									
		211			0.179				
		25		0.160	0.185	0.199	0.211	0.235	0.243
26 0.16' 0.192 0.206 0.218 0.242 0.251					0.192	0.206		0.242	0.251
27 0.173 0.199 0.213 0.225 0.249 0.258						0.213			
28 0.179 0.205 0.220 0.232 0.256 0.265							0.232		
29 0.185 0.212 0.226 0.239 0.263 0.272	•						0.239		
30 0.191 0.218 0.233 0.216 0.270 0.279									
31 0.198 0.225 0.240 0.252 0.277 0.286									
32 0.204 0.231 0.246 0.259 0.284 0.293									
33 0.210 0.238 0.253 0.266 0.291 0.365 34 0.216 0.244 0.260 0.273 0.298 0.307		رر 1.							
34 0.216 0.244 0.260 0.273 0.298 0.307 35 0.222 0.251 0.266 0.279 0.304 0.314					0.244				
36 0.229 0.257 0.273 0.286 0.311 0.321		36			0.257	0.273			
37 0.235 0.264 0.280 0.293 0.318 0.328				0.235					
38 0.241 0.270 0.286 0.299 0.325 0.334		38	•			0.286			
39 0.247 0.277 0.293 0.306 0.332 0.311	•								
40 0.254 0.283 0.299 0.313 0.338 0.348									
41 0.260 0.290 0.306 0.319 0.345 0.355			'	0.260	0.290				
42 0.266 0.296 0.312 0.326 0.352 0.362		42		0.266		0.312	0.326	0.352	
43 0.272 0.303 0.319 0.332 0.359 0.368		43							
Ш 0.279 0.309 0.325 0.339 0.365 0.375		Щ.							
45 0.285 0.315 0.332 0.346 0.372 0.382									
1.6 0.291 0.322 0.338 0.352 0.378 0.388									
47 0.297 0.328 0.345 0.359 0.385 0.395									
48 0.304 0.335 0.351 0.365 0.392 0.401 49 0.310 0.341 0.358 0.372 0.398 0.408			.,						
49 0.310 0.311 0.358 0.372 0.398 0.408 50 0.316 0.347 0.364 0.378 0.405 0.415	•								

N	£	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>.990</u>	<u>.995</u>
170	0.		0.004	0.009	0.013	0.017	0.027	0.031
•	1		0.010	0.018	0.023	0.028	0.038	0.043
	2		0.016	0.025	0.031	0.037	0.049	0.053
	2 3 4 5 6		0.022	0.032	0.039	0.045	0.058 0.069	0.063
,	4		0.027	0.039	0.046	0.053	0.009	0.072 0.081
	6		0.033	0.046 0.053	0.054 0.061	0.061 0.068	0.084	0.090
	7		0.045	0.060	0.068	0.076	0.004	0.098
	7		0.051	0.066	0.075	0.083	0.100	0.106
	9		0.057	0.003	0.013	0.091	0.107	0.114
	ío		0.063	0.079	0.089	0.098	0.115	0.122
	11		0.069	0.086	0.096	0.105	0.123	0.129
	12		0.074	0.092	0.103	0.112	0.130	0.137
	13		0.080	0.099	0.110	0.119	0.137	0.145
	14		0.086	0.105	0.116	0.126	5رار.0	0.152
	15		0.092	0.112	0.123	0.133	0.154	0.159
	16		0.098	0.118	0.130	0.139	0.159	0.167
	17		0.104	0.124	0.136	0.146	0.166	0.174
•	18		0.110	0.131	0.143	0.153	0.173	0.181
	19		0.115	0.137	0.149	0.160	0.180	0.188
	20		0.121	0.143	0.156	0.166	0.187	0.195
	21		0.127	0.150	0.162	0.173	0.194	0.202
	22		0.133	0.156	0.169	0.180	0.201	0.209
	23 2 <u>4</u>		0.139 0.145	0.162 0.168	0.175 0.182	0.186 0.193	0.208 0.215	0.216 0.223
	25		0.151	0.105	0.102	0.199	0.21	0.230
	26		0.157	0.181	0.194	0.206	0.228	0.237
	27		0.162	0.187	0.201	0.212	0.235	0.243
	28		0.168	0.193	0.207	0.219	0.242	0.250
	29		0.174	0.199	0.213	0.225	0.248	0.257
•	30		0.180	ó.206	0.220	0.232	0.255	0.264
•	31	•	0.186	0.212	0.226	0.238	0.261	0.270
	32		0.192	0.218	0.232	0.244	0.268	0.277
	33		0.198	0.22Li	0.239	0.251	0.275	0.283
	34	,	0.204	0.230	0.245	0.257	0.281	0.290
	35		0.209	0.236	0.251	0.264	0.288	0.296
	36		0.215	0.243	0.257	0.270	0.294	0.303
	37		0.221	0.249	0.264	0.276	0.300	0.310
	38		0.227	0.255	0.270	0.282	0.307	0.316
	39		0.233	0.261	0.276	0.259	0.313	0.322
	40		0.239	0.267	0.282	0.295	0.320	0.329

<u>N</u>	F	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>. 995</u>
	41 42 43 44 45 46 47 48 49 50		0.245 0.250 0.256 0.262 0.268 0.27li 0.280 0.280 0.292	0.273 0.279 0.285 0.291 0.297 0.303 0.309 0.315 0.321	0.288 0.295 0.301 0.307 (.313 0.319 0.325 0.331 0.344	0.301 0.308 0.314 0.320 0.326 0.332 0.339 0.345 0.351	0.326 0.332 0.339 0.345 0.351 0.358 0.364 0.370 0.376 0.383	0.335 0.342 0.348 0.354 0.361 0.367 0.373 0.380 0.386 0.392
180	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17		0.004 0.009 0.015 0.020 0.026 0.031 0.037 0.043 0.048 0.054 0.059 0.065 0.070 0.076 0.081 0.087 0.092	0.009 0.017 0.024 0.030 0.037 0.044 0.050 0.056 0.063 0.069 0.075 0.081 0.087 0.093 0.100 0.106 0.112	0.013 0.021 0.029 0.037 0.044 0.051 0.058 0.065 0.071 0.078 0.084 0.091 0.097 0.104 0.110 0.116 0.122 0.129	0.017 0.026 0.035 0.043 0.050 0.058 0.065 0.072 0.079 0.086 0.092 0.099 0.106 0.112 0.119 0.125 0.132	0.025 0.036 0.046 0.054 0.063 0.071 0.079 0.087 0.094 0.102 0.109 0.116 0.123 0.130 0.137 0.144 0.151	0.029 0.041 0.050 0.060 0.068 0.077 0.085 0.093 0.100 0.108 0.115 0.122 0.130 0.137 0.144 0.151 0.158
	18 19 20 21 22 23 24 25 26 27		0.104 0.109 0.115 0.120 0.126 0.131 0.137 0.142 0.148 0.153	0.124 0.130 0.136 0.141 0.147 0.153 0.159 0.165 0.171	0.129 0.135 0.141 0.147 0.153 0.160 0.166 0.172 0.178 0.184	0.135 0.151 0.157 0.164 0.170 0.176 0.182 0.189 0.195 0.201	0.164 0.171 0.177 0.184 0.190 0.197 0.203 0.210 0.216 0.222	0.171 0.178 0.185 0.191 0.198 0.205 0.211 0.218 0.224 0.231

<u>N</u>	£	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>.900</u>	<u>. 950</u>	<u>.990</u>	<u>•995</u>
	28 29 33 33 33 35 37 38 39 44 44 44 44 49 50 48 49 50		0.159 0.165 0.170 0.176 0.181 0.187 0.192 0.198 0.203 0.209 0.214 0.220 0.226 0.231 0.237 0.242 0.248 0.253 0.259 0.264 0.270 0.275 0.281	0.183 0.189 0.194 0.200 0.206 0.212 0.218 0.224 0.229 0.235 0.241 0.252 0.258 0.264 0.270 0.275 0.281 0.287 0.293 0.298 0.304 0.310	0.196 0.202 0.208 0.211 0.220 0.226 0.238 0.213 0.219 0.255 0.261 0.267 0.273 0.279 0.281 0.290 0.296 0.308 0.311 0.319 0.325	0.207 0.213 0.219 0.225 0.231 0.237 0.243 0.249 0.255 0.261 0.267 0.273 0.279 0.285 0.291 0.297 0.303 0.309 0.315 0.320 0.326 0.332 0.338	0.229 0.235 0.241 0.248 0.254 0.260 0.266 0.272 0.278 0.285 0.291 0.297 0.303 0.309 0.315 0.327 0.333 0.339 0.345 0.351 0.357 0.363	0. 237 0. 243 0. 250 0. 256 0. 262 0. 268 0. 275 0. 281 0. 287 0. 299 0. 306 0. 312 0. 318 0. 324 0. 330 0. 342 0. 348 0. 354 0. 360 0. 366 0. 372
190	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		0.004 0.009 0.014 0.019 0.025 0.035 0.040 0.056 0.051 0.056 0.067 0.072 0.072 0.077 0.082 0.088 0.093 0.098 0.103 0.109	0.008 0.016 0.022 0.029 0.035 0.041 0.047 0.053 0.059 0.065 0.071 0.077 0.083 0.089 0.094 0.100 0.106 0.112 0.117 0.123 0.129	0.012 0.020 0.028 0.035 0.042 0.048 0.055 0.061 0.067 0.074 0.080 0.086 0.092 0.098 0.104 0.110 0.116 0.122 0.128 0.134 0.140	0.016 0.025 0.033 0.040 0.048 0.055 0.061 0.068 0.075 0.081 0.088 0.094 0.100 0.107 0.113 0.119 0.125 0.131 0.137 0.143 0.149	0.024 0.034 0.044 0.052 0.060 0.068 0.075 0.082 0.089 0.096 0.103 0.110 0.117 0.123 0.130 0.136 0.143 0.149 0.156 0.162 0.168	0.028 0.038 0.048 0.057 0.065 0.073 0.080 0.088 0.095 0.109 0.116 0.123 0.130 0.136 0.143 0.150 0.163 0.169 0.175

Й	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	21 22 23 24 25 26 27 28 29 20 21 21 21 21 21 21 21 21 21 21 21 21 21		0.114 0.119 0.124 0.130 0.135 0.140 0.145 0.151 0.156 0.161 0.166 0.172 0.177 0.182 0.187 0.193 0.203 0.208 0.214 0.219 0.224 0.229 0.235 0.240 0.256 0.266	0.134 0.145 0.145 0.157 0.162 0.167 0.173 0.179 0.184 0.190 0.195 0.201 0.206 0.212 0.217 0.223 0.228 0.234 0.239 0.245 0.250 0.256 0.267 0.277 0.283 0.288 0.294	0.146 9.151 0.157 0.163 0.169 0.174 0.180 0.186 0.191 0.197 0.203 0.208 0.214 0.220 0.225 0.231 0.237 0.242 0.248 0.253 0.259 0.264 0.270 0.275 0.281 0.292 0.298 0.303 0.309	0.155 0.161 0.167 0.173 0.179 0.185 0.191 0.196 0.202 0.208 0.214 0.220 0.225 0.231 0.237 0.242 0.248 0.254 0.259 0.265 0.271 0.276 0.282 0.288 0.293 0.299 0.304 0.310 0.315 0.321	0.174 0.181 0.187 0.193 0.199 0.205 0.211 0.217 0.223 0.229 0.235 2.41 0.247 0.253 0.259 0.265 0.270 0.282 0.288 0.293 0.299 0.305 0.311 0.316 0.322 0.328 0.328 0.333 0.339 0.315	0.182 0.188 0.194 0.200 0.207 0.213 0.219 0.225 0.231 0.237 0.243 0.249 0.255 0.261 0.267 0.273 0.279 0.285 0.290 0.296 0.302 0.308 0.314 0.319 0.325 0.331 0.318 0.314
200	0 1 2 3 4 5 6 7 8 9 10		0.003 0.008 0.013 0.018 0.023 0.028 0.033 0.043 0.043 0.048	0.008 0.015 0.021 0.027 0.033 0.039 0.045 0.051 0.056 0.062	0.011 0.019 0.026 0.033 0.040 0.046 0.052 0.058 0.064 0.070	0.015 0.023 0.031 0.038 0.045 0.052 0.058 0.065 0.071 0.077	0.023 0.033 0.041 0.049 0.057 0.064 0.071 0.078 0.085 0.092 0.098	0.026 0.037 0.046 0.054 0.062 0.069 0.075 0.084 0.090 0.097

<u>N</u>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>•990</u>	.995
	11 12 11 13 14 15 16 17 18 19 20 21 22 22 22 23 23 23 23 23 23 23 23 23 23		0.058 0.063 0.068 0.073 0.078 0.083 0.088 0.093 0.108 0.103 0.108 0.113 0.128 0.128 0.138 0.143 0.148 0.153 0.158 0.168 0.173 0.168 0.173 0.168 0.193 0.198 0.203 0.208 0.213 0.208 0.213 0.228 0.233 0.228 0.233 0.248 0.253	0.073 0.079 0.084 0.090 0.095 0.101 0.106 0.111 0.122 0.128 0.133 0.138 0.144 0.149 0.159 0.165 0.170 0.175 0.181 0.186 0.191 0.196 0.202 0.217 0.222 0.217 0.222 0.218 0.233 0.248 0.254 0.259 0.279	0.082 0.088 0.093 0.099 0.105 0.110 0.116 0.122 0.127 0.133 0.138 0.144 0.149 0.155 0.160 0.166 0.171 0.177 0.182 0.188 0.193 0.198 0.204 0.209 0.214 0.220 0.225 0.230 0.216 0.216 0.252 0.257 0.262 0.267 0.273 0.278 0.283 0.288 0.294	0.089 0.095 0.101 0.107 0.113 0.119 0.125 0.131 0.136 0.142 0.148 0.153 0.159 0.164 0.170 0.176 0.181 0.187 0.192 0.198 0.203 0.209 0.214 0.225 0.231 0.225 0.231 0.252 0.258 0.258 0.274 0.279 0.284 0.290 0.295 0.305	0.105 0.111 0.117 0.124 0.130 0.136 0.142 0.148 0.154 0.160 0.166 0.172 0.178 0.184 0.189 0.195 0.201 0.207 0.212 0.218 0.224 0.229 0.235 0.211 0.216 0.252 0.257 0.263 0.269 0.274 0.280 0.296 0.301 0.307 0.312 0.318 0.323 0.328	0.111 0.117 0.124 0.130 0.136 0.142 0.149 0.155 0.161 0.167 0.173 0.179 0.185 0.191 0.197 0.203 0.208 0.214 0.220 0.237 0.243 0.249 0.254 0.260 0.265 0.271 0.277 0.282 0.288 0.293 0.299 0.304 0.310 0.315 0.326 0.331 0.337

<u>N</u>	F	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>.990</u>	<u>.995</u>
210	0		0.003	0.008	0.011	0.014	0.022	0.025
	1		0.008	0.014	0.018	0.022	0.031	0.035
	1 2 3 4 5 6		0.013	0.020	0.025	0.030	0.039	0.043
	3		0.017	0.026	0.032	0.037	0.047	0.051
	. 4		0.022	0.032	0.038	0.043	0.054	0.059
	5		0.027	0.037	0.077	0.049	0.061	0.066
	6		0.032	0.043	0.050	0.056	0.068	0.073
ė	7	,	0.036	0.048	0.055	0.062	0.075	0.080
	8	,	0.041	0.054	0.061	0.068	0.081	0.086 0.091
	9		0.046	0.059	0.067	0.074	0.087	0.091
	10		0.051	0.064	0.072	0.079	0.094	0.105
	11 12		0.055	0.070	0.078	0.085	0.100	0.112
			0.060	0.075	0.084	0.091 0.037	0.106 0.112	0.112
	13	1	0.065	0.080 0.085	0.089	0.102	0.112	0.110
	14 15		0.070 0.074	0.005	0.094 0.100	0.102	0.124	0.130
	16		0.079	0.091	0.105	0.103	0.130	0.136
	17		0.079	0.090	0.105	0.119	0.135	0.142
	18		0.089	0.106	0.116	0.124	0.141	0.148
	19		0.094	0.111	0.121	0.130	0.147	0.154
	20		0.098	0.116	0.127	0.135	0.153	0.159
	21		0.103	0.122	0.132	0.141	0.158	0.165
	22		0.108	0.127	0.137	0.146	0.164	0.171
	23		0.113	0.132	0.142	0.152	0.170	0.176
	24		0.117	0.137	0.147	0.157	0.175	0.182
	. 25		0.122	0.142	0.153	0.162	0.181	0.188
	26		0.127	0.147	0.158	0.168	0.186	0.193
	27	•	0.132	0.152	0.163	0.173	0.192	0.199
	28		0.136	0.157	0.168	0.178	0.197	0.204
	29		0.141	0.162	0.174	0.183	0.203	0.210
•	, 30		0.146	0.167	0.179	0.189	0.208	0.216
•	31		0.151	0.172	0.184	0.194	0.214 0.219	0.221 0.226
	32		0.155	0.177	0.189 0.194	0.199 0.204	0.219	0.232
	33 34		0.160 0.165	0.182 0.187	0.194	0.204	0.230	0.237
	35 35		0.109	0.107	0.204	0.210	0.235	0.243
	36	•	0.174	0.192	0.204	0.220	0.240	0.248
•	37		0.179	0.202	0.215	0.225	0.246	0.253
	38		0.184	0.207	0.220	0.230	0.251	0.259
	39		0.189	0.212	0.225	0.235	0.256	0.264
	110		0.193	0.217	0.230	0.241	0.262	0.269

N	F	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>. 950</u>	<u>.990</u>	<u>•995</u>
	41		0.198	0.222	0.235	0.246	0.267	0:275
	42		0.203	0.227	0.240	0.251	0.272	0.280
	43		0.208	0.232	0.245	0.256	0.277	0.285
	44		0.212	0.237	0.250	0.261	0.282	0.291
•	45		0.217	0.242	0.255	0.266	0.288	0.296
	46	,	0.222	0.247	0.260	0.271	0.293	0.301
	47		0.227	0.252	0.265	0.276	0.298	0.306
	48		0.231	0.256	0.270	0.281	0.303	0.311
	49		0.236	0.261	0.275	0.286	0.308	0.317
	50		0.241	0.266	0.280	0.291	0.313	0.322
220	0		0.003	0.007	0.010	0.014	0.021	0.024
	1		0.008	0.013	0.018 (	0.021	0.030	0.033
	2		0.012	0.019	0.024	0.028	0.038	0.041
	ر ا.		0.017	0.025	0.030	0.035	0.045	0.049
	4		0.021	0.030	0.036	0.041	0.052	0.056
	. 6		0.026	0.036	0.042	0.047	0.058	0.063
	2 3 4 5 6 7	,	0.030 0.035	0.041	0.047	0.053	0.065	0.070
	8		0.039	0.046	0.053	0.059	0.071	0.076
	9		بلباه.٥	0.051 0.056	0.058	0.065	0.077	0.082
	ío		0.048	0.050	0.064	0.070	0.083	0.089
	11		0.053	0.067	0.069 0.074	0.076	0.089	0.095
	12		0.057	0.072	0.080	0.081	0.095	0.7.01
	13		0.062	0.077	0.085	0.087 0.092	0.101	0.107
	14	. :	0.067	0.082	0.090	0.092	0.107	0.113
	15		0.071	0.087	0.095	0.103	0.113 0.118	0.118
	16		0.076	0.092	0.101	0.108	0.124	0.124
	17		0.080	0.096	0.106	0.114	0.130	0.130 0.136
	18	•	0.085	0.101	0.111	0.119	0.135	0.150
	19		0.089	0.106	0.116	0.124	0.141	0.147
	20		0.094	0.111	0.121	0.129	0.146	0.152
	21		0.098	0.116	0.126	0.135	0.151	0.158
	22		0.103	0.121	0.131	0.140	0.157	0.163
	23		0.107	0.126	0.136	0.145	0.162	0.169
	21 <sub>1</sub>		0.112	0.131	0.141	0.150	0.168	0.174
	26		0.116	0.135	0.146	0.155	0.173	0.180
	27		0.121	0.140	0.151	0.160	0.178	0.185
	<b>4</b> i		0.126	0.145	0.156	0.165	0.183	0.190

<u>N</u>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>•950</u>	.990	• 995
	28 29 31 32 33 33 33 33 33 34 44 44 44 45 46 47 48 49 50		0.130 0.135 0.139 0.148 0.153 0.157 0.162 0.166 0.171 0.175 0.180 0.185 0.189 0.194 0.198 0.203 0.207 0.212 0.216 0.221	0.150 0.155 0.160 0.164 0.169 0.174 0.179 0.183 0.188 0.193 0.198 0.202 0.207 0.212 0.207 0.212 0.226 0.231 0.236 0.240 0.215 0.250 0.254	0.161 0.166 0.171 0.176 0.181 0.186 0.190 0.195 0.200 0.205 0.210 0.215 0.220 0.224 0.229 0.224 0.239 0.214 0.239 0.214 0.253 0.258 0.263 0.268	0.170 0.175 0.180 0.185 0.190 0.195 0.200 0.205 0.210 0.215 0.220 0.225 0.235 0.240 0.245 0.250 0.250 0.250 0.259 0.264 0.269 0.274	0.189 0.194 0.199 0.204 0.209 0.215 0.220 0.225 0.230 0.235 0.240 0.215 0.250 0.255 0.260 0.265 0.270 0.275 0.280 0.290	0.196 0.201 0.206 0.211 0.217 0.222 0.227 0.232 0.237 0.248 0.253 0.258 0.263 0.268 0.273 0.278 0.288 0.283 0.288 0.293 0.298 0.303
230	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18		0.003 0.007 0.012 0.016 0.020 0.025 0.029 0.033 0.038 0.042 0.046 0.051 0.055 0.055 0.059 0.064 0.068 0.072 0.077	0.007 0.013 0.019 0.024 0.029 0.034 0.039 0.044 0.059 0.054 0.059 0.064 0.069 0.073 0.078 0.083 0.088 0.092	0.010 0.017 0.023 0.029 0.034 0.040 0.045 0.051 0.056 0.061 0.066 0.071 0.076 0.081 0.086 0.091 0.096 0.101 0.106	0.279 0.013 0.020 0.027 0.033 0.039 0.045 0.051 0.056 0.062 0.067 0.073 0.078 0.083 0.088 0.094 0.099 0.104 0.109 0.114	0.300 0.020 0.029 0.036 0.043 0.050 0.056 0.062 0.068 0.074 0.000 0.086 0.091 0.097 0.102 0.108 0.113 0.119 0.124 0.129	0.308 0.023 0.032 0.040 0.047 0.054 0.060 0.067 0.073 0.079 0.085 0.091 0.097 0.102 0.108 0.113 0.119 0.124 0.130 0.135

N	E	<u>c</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	19 20 21 22 21 25 26 27 28 29 30 31 32 33 33 33 33 34 44 44 44 45 46 47 48		0.085 0.090 0.094 0.098 0.103 0.107 0.111 0.116 0.120 0.124 0.129 0.133 0.137 0.142 0.146 0.155 0.159 0.164 0.155 0.169 0.168 0.172 0.181 0.185 0.190 0.194 0.198 0.203 0.207 0.211	0.102 0.106 0.111 0.116 0.120 0.125 0.130 0.134 0.148 0.153 0.157 0.162 0.166 0.171 0.176 0.180 0.185 0.189 0.194 0.198 0.203 0.207 0.212 0.216 0.221 0.225 0.230 0.234	0.111 0.116 0.121 0.125 0.130 0.135 0.140 0.154 0.159 0.164 0.168 0.173 0.168 0.173 0.182 0.187 0.192 0.196 0.201 0.206 0.215 0.219 0.229 0.233 0.212 0.214	0.119 0.124 0.129 0.134 0.139 0.144 0.145 0.153 0.158 0.168 0.168 0.173 0.178 0.182 0.187 0.192 0.197 0.201 0.206 0.211 0.206 0.211 0.216 0.225 0.230 0.234 0.239 0.244 0.253 0.258	0.135 0.140 0.145 0.150 0.155 0.160 0.166 0.171 0.176 0.181 0.196 0.201 0.206 0.211 0.225 0.220 0.225 0.245 0.245 0.254 0.254 0.259 0.269 0.273 0.278	0.141 0.156 0.151 0.156 0.162 0.167 0.172 0.177 0.182 0.198 0.203 0.208 0.213 0.218 0.223 0.213 0.218 0.223 0.217 0.252 0.257 0.262 0.266 0.271 0.276 0.281 0.286
240	49 50 0		0.216 0.220 0.003 0.007	0.239 0.243 0.007 0.012	0.252 0.256 0.010 0.016	0.262 0.267 0.012 0.020	0.283 0.287 0.019 0.027	0.290 0.295 0.022 0.031
	3 4 5 6 7 8 9		0.011 0.015 0.019 0.02h 0.028 0.032 0.036 0.040	0.018 0.023 0.028 0.033 0.038 0.042 0.047 0.052 0.056	0.022 0.028 0.033 0.038 0.043 0.049 0.054 0.059	0.026 0.032 0.038 0.043 0.049 0.054 0.059 0.065	0.035 0.011 0.018 0.051 0.060 0.065 0.071 0.077	0.038 0.045 0.052 0.058 0.064 0.070 0.076 0.081

<u>N</u>	<u>F</u>	<u>c</u>	<u>. 500</u>	.800	.900	<u>. 950</u>	<u>.99</u> 0	<u>•995</u>	
	11		0.049	0.061	0.068	0.075	0.088	0.093	
	12	•	0.053	0.066	0.073	0.080	0.093	0.098	
	13		0.057	0.070	0.078	0.085	0.098	0.103	
	14		0.061	0.075	0.083	0.090	0.104	0.109	
	15		0.065	0.079	0.088	0.095	0.109	0.114	
	16		0.069	0.084	0.092	0.099	0.114	0.119	
	17	•	0.074	0.088	0.097	0.104	0.119	0.125	
	18		0.078	0.093	0.102	0.109	0.124	0.130	
	. 19		0.082	0.098	0.106	0.114	0.129	0.135	
	20		0.086	0.102	0.111	0.119	0.13կ	0.140	
	21		0.090	0.106	0.116	0.124	0.139	0.145	
	22	r	0.094	0.111	0.120	0.128	0. 1իկ	0.150	
	. 23		0.098	0.115	0.125	0.133	0.149	0.155	
	- 211		0.103	0.120	0.129	0.138	0.154	0.160	
	25		0.107	0.124	0.134	0.142	0.159	0.165	
	26		0.111	0.129	0.139	0.147	0.164	0.170	
	27		0.115	0.133	0.143	0.152	0.169	0.175	
	28		0.119	0.138	0.148	0.156	0.173	0.180	
	29		0.123	0.142	0.152	0.161	0.178	0.185	
	30		0.128	0.11.6 0.150	0.157	0.167	0.183 0.188	0.190 0.194	
	31		0.132	0.150	0.161 0.166	0.170 0.175	0.100	0.199	
•	32		0.136 0.140	0.155 0.160	0.100	0.175	0.197	0.204	
	33		0.140	0.164		0.184	0.202	0.204	
	3H		0.144	0.168	0.179	0.189	0.207	0.214	
	35 . 36		0.153	0.173	0.184	0.193	0.211	0.218	
	37		0.157	0.177	0.188	0.198	0.216	0.223	
	,38 ,38		0.161	0.181	0.193	0.202	0.221	0.228	
	.50 39		0.165	0.186	0.197	0.207	0.226	0.233	
	40	1	0.169	0.190	0.202	0.211	0.230	0.237	
	41		0.173	0.195	0.206	0.216	0.235	0.242	
	42	1	0.178	0.199	0.211	0.220	0.239	0.247	
	43	ï	0.182	0.203	0.215	0.225	0.244	0.251	
	111		0.186	0.208	0.219	0.229	0.249	0, 256	_
	15		0.190	0.212	0.224	0.234	0.253	0.260	
	145 46		0.194	0.216	0.228	0.238	0.258	0.265	
•	47		0.198	0.221	0.233	0.243	0.262	0.270	
	48		0.203	0.225	0.237	0.247	0.267	0.274	
	49	•	0.207	0.229	0.241	0.252	0.271	0.279	
	50	,	0.211	0.234	0.246	0.256	0.276	0.283	
250	0	•	0.003	0.006	0.009	0.012	0.018	0.021	
	1		0.007	0.012	0.015	0.019	0.026	0.029	
	. 2		0.011	0.017	0.021	0.025	0.033	0-037	
	3	•	0.015	0.022	0.027	0.031	0.040	0.043	
	՝ <u>ի</u>		0.019	0.027	0.032	0.036	0.046	0.050	

5 0.023 0.031 0.037 0.042 0.052 0 6 0.027 0.036 0.042 0.047 0.057 0 7 0.031 0.041 0.047 0.052 0.063 0 8 0.035 0.045 0.051 0.057 0.068 0 9 0.039 0.050 0.056 0.062 0.074 0 10 0.043 0.054 0.061 0.067 0.079 0 11 0.047 0.059 0.066 0.072 0.084 0 12 0.051 0.063 0.070 0.077 0.089 0 13 0.055 0.068 0.075 0.081 0.094 0 14 0.059 0.072 0.080 0.086 0.099 0 15 0.063 0.076 0.084 0.091 0.104 0 16 0.067 0.081 0.089 0.096 0.109 0.104 0 17 0.071 0.085 0.093 0.100 0.114 0.19 0.194 0.194 0.192 0.194 0.192 0.194 0.192 0.194 0.195 0.194 0.195 0.194 0.195 0.194 0.195 0.195 0.194 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.195 0.195 0.196 0.195 0.196 0.193 0.195 0.195 0.195 0.196 0.193 0.196 0.195 0.195 0.196 0.193 0.196 0.195 0.195 0.196 0.195 0.196 0.195 0.196 0.195 0.196 0.195 0.196 0.196 0.195 0.196 0.195 0.196 0.196 0.195 0.196 0.196 0.196 0.196 0.195 0.196 0.1
31

K	£	5	<u>.5co</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>•990</u>	<u>. 995</u>
300	0		0.002	0.005	0.008	0.010	0.015	0.018
	1		0.006	0.010	0.013	0.016	0.013	0.015
	2345678		0.009	0.014	0.018	0.021	0.022	0.025
	3	•	0.012	0.018	0.022	0.026	0.020	0.036
	4		0.016	0.022	0.026	0.030	0.038	0.041
	5		0.019	0.026	0.031	0.035	0.043	0.041
	6	•	0.022	0.030	0.035	0.039	0.048	0.051
	7	1	0.026	0.034	0.039	0.043	0.053	0.056
	8		0.029	0.038	0.043	0.048	0.057	0.061
	9		0.032	0.041	0.047	0.052	0.062	0.065
	10		0.036	0.045	0.051	0.056	0.066	0.009
	11		0.039	0.049	0.055	0.060	0.070	0.074
	12		0.042	0.053	0.059	0.064	0.075	0.079
1	13		0.046	0.056	0.063	0.068	0.079	0.083
	14		0.049	0.060	0.066	0.072	0.083	0.088
	15		0.052	0.064	0.070	0.076	0.087	0.092
	16		0.055	0.067	0.074	0.080	0.092	0.096
	17		0.059	0.071	0.078	0.084	0.096	0.100
	- 18		0.062	0.075	0.082	0.088	0.100	0.104
	19 20		0.065	0.078	0.085	0.092	0.104	0.109
	21		0.069	0.082	0.089	0.095	0.108	0.113
	22		0.072 0.075	0.085	0.093	0.099	0.112	0.117
	23	<b>.</b>	0.079	0.089	0.097	0.103	0.116	0.121
	24		0.082	0.093	0.100	0.107	0.120	0.125
	25		0.085	0.096 0.100	0.104	0.111	0.124	0.129
	26		0.089	0.103	0.108	0.114	0.128	0.133
	27		0.009	0.103	0.111	0.118	0.132	0.137
	28	*	0.095	0.110	0.115 0.119	0.122	0.136	0.141
•	29	,	0.099	0.114	0.122	0.126 0.129	0.140	0.145
	30		0.102	0.117	0.126	0.129	0.11/1 0.11/7	0.149
	31		0.105	0.121	0.129	0.137	0.147 0.151	0.153
	. 32		0.109	0.124	0.133	0.141	0.155	0.157 0.161
	33	•	0.112	0.128	0.137	0.144	0.159	0.165
	34		0.115	0.132	0.140	0.148	0.163	0.168
	3i1 35		0.119	0.135	0.144	0.152	0.167	0.172
	· 36		0.122	0.139	0.148	0.155	0.170	0.176
•	37		0.125	0.142	0.151	0.159	0.174	0.180
•	38		0.129	0.146	0.155	0.163	0.178	0.184
	39		0.132	0.149	0.158	0:166	0.182	0.188
	40		0.135	0.153	0.162	0.170	0.186	0.191
	41		0.139	0.156	0.166	0.174	0.189	0.195
	42		0.142	0.160	0.169	0.177	0.193	0.199

N	F	<u>c</u> _	۲oo	000			•	
•••	•	<u> </u>	<u>-500</u>	<u>. 800</u>	<u>.900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	43	•	0.145	0.163	0.173	0.181	0.197	0.203
	145 145		0.149	0.167	0.176	0.185	0.201	0.207
	46		0.152	0.170	0.180	0.188	0.204	0.210
	47		0.155	0.174	0.183	0.192	0.208	0.214
1	48		0.159	0.177	0.187	0.195	0.212	0.218
	40 49		0.162	0.180	0.190	0.199	0.215	0.222
	50		0.165	0.184	0.194	0.203	0.219	0.225
	50		0.169	0.187	0.198	0.206	0.223	0.229
350	0	i	0.002	0.005	0.007	0.009	0.013	۰ مار
	1 2 3 4 5 6		0.005	0.009	0.011	0.013		0.015
	2		0.008	0.012	0.015	0.013	0.019	0.021
	3		0.010	0.016	0.019	0.022	0.024	0.026
	4		0.013	0.019	0.023	0.026	0.028	0.031
	5		0.016	0.022	0.026	0.030	0.033	0.036
	6		0.019	0.026	0.030	0.034	0.037 0.041	0.040
	7		0.022	0.029	0.033	0.037	0.045	0.014
•	8		0.025	0.032	0.037	0.041	0.049	0.048
	9		0.028	0.036	0.040	0.011	0.053	0.052
	10		0.030	0.039	0. Clil	0.048	0.057	0.056
	11		0.033	0.042	0.047	0.051	0.060	0.060 0.064
	12		0.036	0.045	0.050	0.055	0.064	0.068
	13		0.039	0.048	0.054	0.058	0.068	0.050
	14	•	0.042	0.051	0.057	0.062	0.072	0.075
	15 16	•	0.045	0.055	0.060	0.065	0.075	0.079
	16 17		0.048	0.058	0.064	0.069	0.079	0.079
	18		0.050	0.061	0.067	0.072	0.083	0.086
,			0.053	0.064	0.070	0.075	0.086	0.000
	19 20		0.056	o.067	0.073	0.079	0.089	0.093
	21		0.059	0.070	0.076	0.082	0.093	0.097
	55	1	0.062	0.073	0.080	0.085	0.096	0.101
	23		0.065	0.076	0.083	0.089	0.100	0.104
	2 <u>1</u>		0.068	0.079	0.086	0.092	0.103	0.108
	25		0.070	0.082	0.089	0.095	0.107	0.111
	26		0.073	0.086	0.092	0.098	0.110	0.114
	27		0.076	0.089	0.096	0.102	0.113	0.118
	28		0.079	0.092	0.099	0.105	0.117	0.121
	29		0.082	0.095	0.102	0.108	0.120	0.125
	30		0.085	0.098	0.105	0.111	0.124	0.128
	31		0.088	0.101	0.108	0.114	0.127	0.132
	<i></i>		0.090	0.104	0.111	0.118	0.130	0.135

<u>N</u> .	<u>F</u> <u>C</u>	<u>-500</u>	.300	<u>.900</u>	<u>. 950</u>	<u>.990</u>	<u>• 995</u> .
	32	0.093	0.107	0.114	0.121	0.134	0.138
	33	0.096	0.110	0.118	0.124	0.137	0.142
	34	0.099	0.113	0.121	0.127	0.140	0.145
*	35	0.102	0.116	0.124	0.130	0.143	0.148
	96	0.105	0.119	0.127	0.134	0.147	0.152
	37	0.108	0.122	0.130	0.137	0.150	0.155
	38	0.110	0.125	0.133	0.140	0.153	0.158
	39	0.113	0.128	0.136	0.143	0.156	0.162
	ГО	0.116	0.131	0.139	0.146	0.160	0.165
	41	0.119	0.134	0.142	9. عليه	0.163	0.168
1	42	0.122	0.137	0.145	0.152	0.166	0.171
r	.43	0.125	0.140	0.148	0.156	0.169	0.175
	गिर्ग	0.128	0.143	0.151	0.159	0.173	0.178
	45	0.130	0.146	0.155	0.162	0.176	0.181
•	46	0.133	0.149	0.158	0.165	0.179	0.184
	47	0.136	0.152	0.161	0.168	0.182	0.188
	48	0.139	0.155	0.164	0.171	0.185	0.191
	49	0.142	0.158	0.167	0.174	0.189	0.194
	50	0.145	0.161	0.170	0.177	0.192	0.197
400	0	0.002	0.004	0.006	0.007	0.011	. 0.013
1,	1	0.004	0.007	0.010	0.012	0.016	0.018
	2	0.007	0.011	0.013	0.016	0.021	0.023
	3	0.009	0.014	0.017	0.019	0.025	0.027
	4	0.012	0.017	0.020	0.023	0.029	0.031
	1 2 3 4 5 6	0.014	0.020	0.023	0.026	0.032	0.035
	6	0.017	0.023	0.026	0.029	0.036	0.039
	7	0.019	0.025	0.029	0.033	0.040	0.042
	8	0.022	0.028	0.032	0.036	0.043	0.046
	9	0.024	0.031	0.035	0.039	0.046	0.049
	10	0.027	0.034	0.038	0.042	0.050	0.053
	11	0.029	0.037	0.011	0.045	0.093	0.056
*	12	0.032	0.040	0.044	0.048	0.056	o <b>o59</b>
	13	0.034	0.042	0.047	0.051	0.060	0.063
,	14	0.037	0.045	0.050	0.054	0.063	0.066
	15	0.039	0.043	0.053	0.057	0.066	0.069
	16	0.042	0.051	0.056	0.060	0.069	0.072
.•	17	0.014	0.053	0.059	0.063	0.072	0.076
	18	0.047	0.056	0.061	0.066	0.075	0.079
•	19 .	0.049	0.059	0.064	0.069	0.078	0.082
*	20	0.052	0.061	0.067	0.072	0.081	0.085

N	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>. 950</u>	<u>.990</u>	<u>.995</u>
	21 22 32 45 66 78 99 30 132 334 55 66 738 99 44 14 14 14 14 14 14 14 14 14 14 14 14		0.054 0.057 0.059 0.062 0.064 0.067 0.069 0.072 0.074 0.077 0.079 0.082 0.084 0.087 0.089 0.092 0.094 0.097 0.099 0.102 0.104 0.107 0.119 0.112 0.114 0.117	0.064 0.067 0.070 0.072 0.075 0.078 0.080 0.083 0.086 0.091 0.094 0.096 0.099 0.102 0.104 0.107 0.109 0.115 0.115 0.123 0.123 0.128 0.123 0.128 0.131 0.136 0.138 0.131	0.070 0.073 0.075 0.078 0.081 0.081 0.087 0.089 0.095 0.095 0.098 0.100 0.103 0.106 0.108 0.111 0.111 0.111 0.112 0.125 0.125 0.127 0.130 0.135 0.138 0.111 0.111 0.114 0.116 0.119	0.075 0.078 0.080 0.083 0.086 0.089 0.092 0.095 0.100 0.103 0.106 0.109 0.112 0.114 0.117 0.120 0.123 0.125 0.128 0.131 0.136 0.131 0.136 0.131 0.136 0.137 0.156	0.084 0.087 0.091 0.097 0.099 0.105 0.105 0.108 0.111 0.117 0.120 0.123 0.126 0.129 0.132 0.137 0.140 0.143 0.146 0.149 0.152 0.157 0.160 0.163 0.166 0.168	0.088 0.091 0.097 0.100 0.103 0.106 0.110 0.115 0.118 0.121 0.124 0.127 0.130 0.133 0.136 0.139 0.145 0.145 0.145 0.150 0.150 0.150 0.162 0.165 0.168 0.171 0.173
<b>ь</b> 50	012345678910		0.002 0.004 0.006 0.008 0.010 0.013 0.015 0.017 0.019 0.021	0.004 0.007 0.009 0.012 0.015 0.018 0.020 0.023 0.025 0.028 0.030	0.005 0.009 0.012 0.015 0.018 0.021 0.023 0.026 0.029 0.031	0.007 0.010 0.011 0.017 0.020 0.023 0.026 0.029 0.032 0.035 0.037	0.010 0.015 0.019 0.022 0.026 0.029 0.032 0.035 0.035 0.011	0.012 0.016 0.020 0.024 0.028 0.031 0.034 0.038 0.041 0.047

<u>N</u>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	11		0.026	0.033	0.037	0.040	0.047	0.050
	12		0.028	0.035	0.039	0.043	0.050	0.053
	13		0.030	0.038	0.042	0.046	0.053	0.056
	14	1	0.033	0.040	0.0	0.048	0.056	0.059
	15		0.035	0.043	0.047	0.051	0.059	0.052
	16	-	0.037	0.01.5	0.050	0.054	0.061	0.065 0.067
٠	17		0.039	0.047	0.052	0.056	0.064	
	18		0.041	0.050	0.055	0.059	0.067	0.070 0.073
	19		0.014	0.052	0.057	0.061	0.070 0.072	0.076
	20		0.046	0.055	0.060	0.064	0.075	0.079
	21		0.048	0.057	0.062 0.065	0.067 0.069	0.078	0.081
	22		0.050	0.059 0.062	0.067	0.009	0.070	0.084
	23 24		0.053 0.055	0.064	0.057	0.074	0.083	0.087
•	25		0.057	0.067	0.070	0.077	0.086	0.089
	26 .		0.059	0.069	0.075	0.079	0.089	0.092
	27		0.061	0.071	0.077	0.082	0.091	0.095
	28	1	0.064	0.074	0.079	0.084	0.094	0.098
	29		0.066	0.076	0.082	0.087	0.097	0.100
	30		0.068	0.079	0.084	0.089	0.099	0.103
	31		0.070	0.081	0.087	0.092	0.102	0.106
	32		0.073	0.083	0.089	0.094	0.104	0.108
	33		0.075	0.086	0.092	0.097	0.107	0.111
	34		0.077	0.088	0.094	0.099	0.110	0.113
	35		0.079	0.090	0.097	0.102	0.112	0.116
	36		0.081	0.093	0.099	0.104	0.115	0.119
	37		0.084	0.095	0.101	0.107	0.117	0.121
	38		0.086	0.097	0.104	0.109	0.120	0.124
	79		0.088	0'.100	0.106	0.112	0.122	0.126 0.129
•	40		0.090	0.102	0.109 0.111	0.114 0.117	0.125 0,128	0.129
	42		0.093 0.095	0.104 0.107	0.111	0.117	0.120	0.134
	43		0.097	0.107	0.116	0.119	0.133	0.137
	717		0.099	0.111	0.118	0.124	0.135	0.139
	45		0.101	0.114	0.121	0.126	0.138	0.11,2
	46		0.104	0.116	0.123	0.129	0.140	0.144
•	47		0.106	0.118	0.125	0.131	0.143	0.147
	48		0.108	0.121	0.128	0.134	0.145	0.150
•	48 49	•	0.110	0.123	0.130	0.136	0.148	0.152
	50		0.113	0.125	0.133	0.139	0.150	0.155
500	0		0.001	0.003	0.005	0.006	0.009	0.011
	1		0.003	0.006	0.008	0.009	0.013	0.015
	2		0.005	0.009	0.011	0.013	0.017	0.018

3	<u>N</u>	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>.990</u>	.995
8		3							
8		4							
8		2							
8	,	7							
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114									
15									
16									
17		16							
18						0.01.7			
19						0.019	0.053		
20							0.055		
21		20				0.054	0.058		
22						0.056			
0.047				0.045					
2h         0.0h9         0.058         0.063         0.067         0.075         0.078           25         0.051         0.060         0.065         0.069         0.077         0.081           26         0.053         0.062         0.067         0.071         0.080         0.083           27         0.055         0.064         0.069         0.07h         0.082         0.086           28         0.057         0.066         0.072         0.076         0.085         0.088           29         0.059         0.069         0.07h         0.078         0.087         0.090           30         0.061         0.071         0.076         0.081         0.089         0.093           31         0.063         0.073         0.078         0.083         0.092         0.095           32         0.065         0.075         0.080         0.085         0.09h         0.096           33         0.067         0.077         0.083         0.087         0.096         0.100           34         0.069         0.079         0.085         0.090         0.099         0.102           35         0.071         0.081         0.087	. •				0.056				
25					0.058	0.063			
27						0.065	0.069		
28									
29									
30									
31									
32		30							
33		31							
36 0.073 0.083 0.089 0.094 0.103 0.107 37 0.075 0.086 0.091 0.096 0.106 0.109 38 0.077 0.088 0.093 0.098 0.108 0.112 39 0.079 0.090 0.096 0.101 0.110 0.114 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		32 22							
36 0.073 0.083 0.089 0.094 0.103 0.107 37 0.075 0.086 0.091 0.096 0.106 0.109 38 0.077 0.088 0.093 0.098 0.108 0.112 39 0.079 0.090 0.096 0.101 0.110 0.114 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		33 31,							
36 0.073 0.083 0.089 0.094 0.103 0.107 37 0.075 0.086 0.091 0.096 0.106 0.109 38 0.077 0.088 0.093 0.098 0.108 0.112 39 0.079 0.090 0.096 0.101 0.110 0.114 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		35 24							
37 0.075 0.086 0.091 0.096 0.106 0.109 38 0.077 0.088 0.093 0.098 0.108 0.112 39 0.079 0.090 0.096 0.101 0.110 0.114 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		36							
38 0.077 0.088 0.093 0.098 0.108 0.112 39 0.079 0.090 0.096 0.101 0.110 0.111 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126									
39 0.079 0.090 0.096 0.101 0.110 0.1114 40 0.081 0.092 0.098 0.103 0.113 0.116 41 0.083 0.094 0.100 0.105 0.115 0.119 42 0.085 0.096 0.102 0.107 0.117 0.121 43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		38							
40       0.081       0.092       0.098       0.103       0.113       0.116         41       0.083       0.094       0.100       0.105       0.115       0.119         42       0.085       0.096       0.102       0.107       0.117       0.121         43       0.087       0.098       0.104       0.110       0.120       0.123         44       0.089       0.100       0.107       0.112       0.122       0.126	. '								
1									
12		. 41							
43 0.087 0.098 0.104 0.110 0.120 0.123 44 0.089 0.100 0.107 0.112 0.122 0.126		42							
14 0.089 0.100 0.107 0.112 0.122 0.126	•	43							
		بليا	*						
		45	•						

						•	•	
N	<u> </u>	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>. 950</u>	<u>•990</u>	<u>. 995</u>
,	46		0.093	0.105	0.111	0.116	0.126	0.130
	47		0.095	0.107	0.113	0.118	0.129	0.133
	48	•	0.097	0.109	0.115	0.120	0.131	0.135
	49		0.099	0.111	0.117	0.123	0.133	0.137
	50		0.101	0.113	0.119	0.125	0.135	0.139
	51		0.103	0.115	0.122	0.127	0.138	0.142
	52		0.105	0.117	0.124	0.129	0.170	0.144
	53		0.107	0.119	0.126	0.131	0.142	0.146
	54		0.109	0.121	0.128	0.134	0.144	0.149
	55	,	0.111	0.123	0.130	0.136	0.147	0.151
	56		0.113	0.126	0.132	0.138	0.149	0.153
	57		0.115	0.128	0.134	0.140	0.151	0.155
	58		0.117	0.130	0.137	0.142	0.153	0.158
	59		0.119	0.132	0.139	0.144	0.156	0.160
•	60		0.121	0.134	0.141	0.147	0.158	0.162
*	61		0.123	0.136	0.143	0.149	0.160 0.162	0.164 0.167
	62		0.125	0.138	0.145	0.151 0.153	0.165	0.169
	63 64		0.127 0.129	0.140 0.142	0.147 0.149	0.155	0.167	0.171
	65		0.129	0.144	0.151	0.157	0.169	0.173
	66 <sub>.</sub>		0.133	0.146	0.154	0.160	0.171	0.176
	67		0.135	0.148	0.156	0.162	0.173	0.178
	68		0.137	0.151	0.158	0.164	0.176	0.180
	69		0.139	0.153	0.160	0.166	0.178	0.182
	70		0.141	0.155	0.162	0.168	0.180	0.184
	71		0.143	0.157	0.164	0.170	0.182	0.187
	72		0.145	0.159	0.166	0.172	0.184	0.189
	73		0.147	0.161	0.168	0.175	0.187	0.191
1	74		0.149	0.163	0.170	0.177	0.188	0.193
	75		0.151	0.165	0.173	0.179	0.191	0.195 0.198
	76		0.153 0.155	0.167 0.169	0.175 0.177	0.181 0.183	0.193 0.195	0.200
	77 78		0.157	0.109	0.179	0.105	0.197	0.202
	79		0.157	0.173	0.181	0.187	0.200	0.204
•	86		0.161	0.175	0.183	0.189	0.202	0.206
	.81		0.163	0.177	0.185	0.192	0.204	0.209
	82		0.165	0.180	0.187	0.194	0.206	0.211
	83		0.167	0.182	0.189	0.196	0.208	0.213
	84		0.169	0.18և	0.191	0.198	0.211	0.215
	. 85		0.171	0.186	0.194	0.200	0.213	0.217
	86		0.173	0.188	0.196	0.202	0.215	0.220
	87		0.175	0.190	0.198	0.204	0.217	0.222
	88		0.177	0.192	0.200	0.206 0.209	0.219 0.221	0.22h 0.226
	- 89		0.179	0.194	0.202	0.407	U. 221	0.420

Ŋ	F	Ċ	<u>.500</u>	<u>. 800</u>	<u>. 900</u>	<u>.95</u> 0	<u>. 990</u>	<u>.995</u>
	90 91 92 93 94 95 96 97		0.181 0.183 0.185 0.187 0.189 0.191 0.193 0.195	0.196 0.198 0.200 0.202 0.204 0.206 0.208 0.210	0.204 0.206 0.208 0.210 0.212 0.214 0.216 0.219	0.211 0.213 0.215 0.217 0.219 0.221 0.223 0.225	0.223 0.226 0.228 0.230 0.232 0.234 0.236 0.239	0.228 0.230 0.233 0.235 0.237 0.239 0.241 0.243
550	01234567890112131561789012232562789901323		0.001 0.003 0.005 0.005 0.005 0.001 0.016 0.018 0.019 0.021 0.023 0.025 0.025 0.034 0.036 0.036 0.036 0.045 0.056 0.056 0.058 0.059 0.059	0.003 0.005 0.008 0.010 0.012 0.014 0.016 0.019 0.021 0.023 0.025 0.027 0.029 0.031 0.033 0.035 0.035 0.045 0.045 0.045 0.051 0.053 0.055 0.055 0.057 0.058 0.060 0.062 0.064 0.066	0.004 0.007 0.010 0.012 0.014 0.017 0.021 0.026 0.028 0.030 0.032 0.034 0.036 0.038 0.043 0.043 0.049 0.055 0.055 0.057 0.067 0.069 0.075 0.075	0.005 0.009 0.011 0.014 0.017 0.021 0.026 0.028 0.031 0.035 0.035 0.040 0.040 0.048 0.050 0.050 0.050 0.055 0.057 0.059 0.063 0.063 0.063 0.063 0.069 0.071 0.073 0.077	0.008 0.012 0.015 0.018 0.021 0.026 0.029 0.031 0.036 0.039 0.043 0.043 0.046 0.055 0.057 0.057 0.057 0.066 0.068 0.077 0.079 0.081 0.086 0.088	0.010 0.013 0.017 0.020 0.023 0.026 0.028 0.031 0.033 0.043 0.046 0.051 0.053 0.055 0.058 0.060 0.062 0.064 0.067 0.069 0.073 0.078 0.080 0.082 0.081 0.089 0.091

N	<u>F</u> <u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>.990</u>	.995
	E 345678890123454789012345678901234566666669777777777777777777777777777777	.500 0.063 0.065 0.067 0.068 0.070 0.072 0.074 0.076 0.078 0.079 0.081 0.083 0.085 0.087 0.088 0.090 0.092 0.093 0.096 0.099 0.101 0.103 0.105 0.107 0.108 0.110 0.112 0.114 0.116 0.119 0.121 0.127 0.128 0.130 0.132 0.134	.800 0.072 0.074 0.076 0.076 0.078 0.080 0.082 0.084 0.086 0.087 0.099 0.091 0.093 0.095 0.097 0.099 0.101 0.103 0.105 0.107 0.109 0.110 0.116 0.118 0.120 0.121 0.126 0.127 0.129 0.131 0.135 0.137 0.139 0.143 0.145 0.146 0.148	900 0.077 0.079 0.081 0.085 0.085 0.087 0.089 0.091 0.093 0.095 0.097 0.101 0.103 0.105 0.107 0.113 0.115 0.116 0.120 0.121 0.126 0.128 0.120 0.121 0.126 0.138 0.130 0.132 0.131 0.135 0.136 0.138 0.140 0.145 0.149 0.151 0.153	.250 0.081 0.083 0.086 0.088 0.090 0.092 0.094 0.096 0.100 0.102 0.104 0.106 0.106 0.112 0.114 0.116 0.118 0.120 0.121 0.128 0.128 0.130 0.128 0.137 0.137 0.137 0.147 0.149 0.151 0.153 0.157 0.159 0.161	-990 0.090 0.092 0.094 0.096 0.098 0.101 0.103 0.105 0.107 0.109 0.111 0.113 0.115 0.117 0.119 0.121 0.123 0.125 0.127 0.130 0.138 0.140 0.148 0.140 0.148 0.150 0.152 0.158 0.160 0.160 0.160 0.160 0.160 0.170 0.172	995 0.093 0.095 0.097 0.100 0.102 0.104 0.106 0.108 0.110 0.112 0.113 0.125 0.127 0.129 0.131 0.133 0.135 0.137 0.139 0.144 0.146 0.148 0.150 0.151 0.156 0.158 0.160 0.166 0.168 0.170 0.171 0.176

Ŋ	F	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>.990</u>	<u>. 995</u>
600	, <b>O</b>		0.001	0.003	0.004	0.005	0.008	0.009
	1		0.003	0.005	0.006	0.008	0.011	0.012
	1 2 3 4 5 6 7 8		0.001	0.007	0.009	0.010	0.017	0.015
	3		0.006	0.009	0.011	0.013	0.017	0.018
	7		0.008	0.011	0.013	0.015	0.019	0.021
	5		0.009	0.013	0.015 0.017	0.017 0.020	0.021 0.022	0.023 0.026
	. 7		0.011 0.013	0.015 0.017	0.017	0.020	0.024	0.028
	Ŕ		0.014	0.019	0.022	0.024	0.029	0.020
	9		0.016	0.021	0.024	0.026	0.031	0.033
	ío	1	0.018	0.023	0.026	0.028	0.033	0.035
	11		0.019	0.025	0.028	0.030	0.036	0.038
	12		0.021	0.026	0.029	0.032	0.038	0.010
	13		0.023	0.028	0.031	0.034	0.040	0.042
•	14		0.024	0.030	0.033	0.036	0.042	· 0.0//
	15		0.026	0.032	0.035	0.038	٥٠٥١٨١	0.046
	16	1	0.028	0.034	0.037	0.010	0.046	0.073
	17 18	•	0.029 0.031	0.036 0.037	0.039	0.042	0.078	0.051
	19		0.033	0.037	0.041 0.043	0.0hh 0.0h6	0.050 0.053	0.053 0.055
	20		0.034	0.041	0.045	0.048	0.055	0.057
	21		0.036	0.043	0.047	0.050	0.057	0.059
	22		0.038	0.045	0.049	0.052	0.059	0.061
	23		0.039	0.046	0.050	0.054	0.061	0.063
	24		0.041	0.048	0.052	0.056	0.063	0.065
	25		0.043	0.050	0.054	0.058	0.065	0.067
	26 27		0.014	0.052	0.056	0.060	0.067	0.069
	28	-	0.046 0.048	0.054 0.055	0.058 0.060	0.062 0.063	0.069	0.071
	29		0.049	0.057	0.062	0.065	0.071 0.073	0.074 0.076
	30		0.051	0.059	0.063	0.067	0.075	0.078
	31		0.053	0.061	0.065	0.069	0.077	0.080
*	32	ı	0.054	0.063	0.067	0.071	0.079	0.082
	- 33		0.056	0.064	c.069	0.073	0.081	0.084
	34 35		0.058	0.066	0.071	0.075	0.083	0.086
•	35	•	0.059	0.068	0.073	0.077	0.085	0.088
· · · · · · · · · · · · · · · · · · ·	36 37		0.061 0.063	0.070	0.074	0.078	0.086	0.089
	38		0.064	0.071 0.073	0.076 0.078	0.080 0.082	0.088 0.090	0.091
	39		0.066	0.075	0.080	0.084	0.092	0.093 0.095
	40		0.068	0.077	0.082	0.086	0.094	0.097
	41		0.069	0.078	0.083	0.088	0.096	0.099

N	F	<u>C</u>	<u>.500</u>	<u>. 800</u>	<u>.900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	42		0.071	0.080	0.085	0.090	0.098	0.101
	43		0.073	0.082	0.087	0.091	0.100	0.103
	ŢŢŢ		0.074	0.084	0.089	0.093	0.102	0.105
	45		0.076	0.086	0.091	0.095	0.104	0.107
	46		0.078	0.087	0.093	0.097	0.106	0.109
	47		0.079	0.089	0.094	0.099	0.108	0.111
	48		0.081	0.091	0.096	0.101	0.109	0.113
,	49		0.083	0.093	0.098	0.102	0.111	0.115
	<del>3</del> 6	·	0.084	0.094	0.100	0.104	0.113	0.117
	śĭ		0.086	0.096	0.101	0.106	0.115	0.119
	52		0.088	0.098	0.103	0.108	0.117	0.120
	52 53		0.089	0.100	0.105	0.110	0.119	0.122
	54		0.091	0.101	0.107	0.112	0.121	0.124
	र्दर		0.093	0.103	0.109	0.113	0.123	0.126
	55 56		0.094	0.105	0.110	0.115	0.125	0.128
	57		0.096	0.106	0.112	0.117	0.326	0.130
	58	•	0.098	0.108	0.114	0.119	0.128	0.132
	59		0.099	0.110	0.116	0.121	0.130	0.134
	60		0.101	0.112	0.118	0.122	0.132	0.136
	61		0.103	0.113	0.119	0.124	0.134	0.138
	62		0.104	0.115	0.121	0.126	0.136	0.139
	63		0.106	0.117	0.123	0.128	0.138	0.141
	64		0.108	0.119	0.125	0.130	0.139	0.143
	65		0.109	0.120	0.126	0.131	0.141	0.145
•	66	•	0.111	0.122	0.128	0.133	0.143	0.147
	670.11	3	0.113	0.124	0.130	0.135	0.145	0.149
	68		0.114	0.126	0.132	0.137	0.147	0.151
	69	1	0.116	0.127	0.133	0.138	0.149	0.152
	70		0.118	0.129	0.135	0.140	0.151	0.15և
	71	·	0.119	0.131	0.137	0.142	0.152	0.156
	72	•	0.121	0.133	0.139	بلبلة ٥٠	0.154	0.158
	73		0.123	0.134	0.141	6.146	0.156	0.160
650	0		0.001	0.002	0.004	0.005	0.007	0.008
			0.003	0.005	0.006	0.007	0.010	0.011
•	2		0.004	0.007	0.008	0.010	0.013	0.014
	3		0.006	0.008	0.010	0.012	0.015	0.017
	, I		0.007	0.010	0.012	0.014	0.018	0.019
	5		0.009	0.012	0.014	0.016	0.020	0.022

N	<u>F</u>	<u>c</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>. 990</u>	<u>.995</u>
	6		0.010	0.014	0.016	0.018	0.022	0.024
	7	•	0.012	0.016	0.018	0.020	0.024	0.026
	8		0.013	0.017	0.019	0.022	0.027	0.028
	9		0.015	0.019	0.022	0.024	0.029	0.031
	10		0.016	0.021	0.024	0.026	0.031	0.033
	11		0.018	0.023	0.025	0.028	0.033	0.035
	12		0.019	0.024	0.027	0.030	0.035	0.037
	13		0.021	0.026	0.029	0.032	0.037	0.039
	14		0.023	0.028	0.031	0.033	0.039	0.041
	15		0.024	0.029	0.033	0.035	0.041	0.043
	16	1 .	0.026	0.031	0.034	0.037	0.043	0.045
	17		0.027	0.033	0.036	0.039	0.045	0.047
	18		0.029	0.035	0.038	0.041	0.047	0.049
	19		0.030	0.036	0.040	0.043	0.049	0.051
,	20		0.032	0.038	0.041	0.044	0.050	0.053
	21		0.033	0.040	0.043	0.046	0.052	0.055
•	22		0.035	0.041	0.01.7	0.048	0.054	0.057
	23		0.036	0.043	0.047	0.050	0.056	0.059
	24		0.038	0.045	0.048	0.052	0.058	0.060
	25		0.039	0.046	0.050	0.053	0.060	0.062
	26 <sup>.</sup>		0.041	0.048	0.052	0.055	0.062	0.064
	27	•	0.043	0.050	0.053	0.057	0.064	0.066
	28		0.011	0.051	0.055	0.059	0.065	0.068
	29		0.046	0.053	0.057	0.060	0.067	0.070
	30		0.047	0.054	0.059	0.062	0.069	0.072
	31		0.049	0.056	0.060	0.064	0.071	0.074
	32		0.050	0.058	0.062	0.066	0.073	0.075
	33		0.052	0.059	0.06H	0.067	0.074	0.077
	34		0.053	0.061	0.065	0.069	0.076	0.079
	35		0.055	0.063	0.067	0.071	0.078	0.081
•	36		0.056	0.064		0.072	0.080	0.083
	37		0.058	0.066	0.070	0.074	0.082	0.085
	38		0.059	0.068	0.072	0.076	0.083	0.086
	39	•	0.061	0.069	0.074	0.078	0.085	0.088
	40		0.063	0.071	0.075	0.079	0.087	0.090
	41		0.061	0.072	0.077	0.081	0.089	0.092
•	42		0.065	0.074	0.079	0.083	0.091	0.094
,	43		0.067	0.076	0.080	0.084	0.092	0.095
•	<u>ш</u>	•	0.069	0.077	0.082	0.086	0.094	0.097
•	115		0.070	0.079	0.084	0.088	0.096	0.099
	46		0.072	0.081	0.085	0.090	0.098	0.101
	47	•	0.073	0.082	0.087	0.091	0.099	0.103
	48 1.0		0.075	0.084	0.089	0.093	0.101	0.104
•	49		0.076	0.085	0.090	0.095	0.103	0.106
	50		0.078	0.087	0.092	0.096	0.105	0.108

. <u>N</u>	F	Ç	.500	<u>.800</u>	<u>.900</u>	<u>. 950</u>	<u>•990</u>	<u>. 995</u>
	51 52 51 55 55 55 55 55 55 55 55 56 61 62 63 64 65 66 66 70		0.079 0.081 0.083 0.084 0.086 0.087 0.089 0.090 0.092 0.093 0.095 0.096 0.097 0.099 0.101 0.103 0.104 0.106 0.107 0.109	0.089 0.090 0.092 0.094 0.095 0.097 0.098 0.100 0.103 0.105 0.106 0.108 0.110 0.111 0.113 0.114 0.116 0.118	0.094 0.095 0.097 0.099 0.100 0.102 0.104 0.105 0.107 0.109 0.110 0.112 0.114 0.115 0.117 0.118 0.120 0.122 0.123	0.098 0.100 0.101 0.103 0.105 0.106 0.108 0.110 0.111 0.113 0.115 0.117 0.118 0.120 0.122 0.123 0.125 0.126 0.128 0.130	0.106 0.108 0.110 0.112 0.113 0.115 0.117 0.119 0.120 0.122 0.124 0.125 0.127 0.129 0.131 0.132 0.134 0.136 0.137 0.139	0.110 0.111 0.113 0.115 0.117 0.118 0.120 0.122 0.124 0.125 0.127 0.129 0.131 0.132 0.134 0.136 0.138 0.138
700	012345678910112134561781901223456		0.001 0.002 0.003 0.005 0.007 0.008 0.010 0.011 0.012 0.014 0.015 0.017 0.018 0.020 0.021 0.022 0.021 0.025 0.027 0.028 0.030 0.031 0.035 0.037 0.038	0.002 0.004 0.006 0.008 0.010 0.013 0.015 0.015 0.016 0.018 0.019 0.021 0.023 0.024 0.026 0.027 0.029 0.031 0.032 0.035 0.035 0.037 0.038 0.040 0.043 0.043	0.003 0.006 0.008 0.010 0.013 0.015 0.015 0.015 0.020 0.022 0.024 0.025 0.027 0.029 0.030 0.035 0.035 0.035 0.036 0.040 0.042 0.043 0.046 0.048	0.004 0.007 0.009 0.011 0.013 0.015 0.017 0.019 0.021 0.022 0.024 0.026 0.028 0.029 0.031 0.033 0.035 0.036 0.038 0.040 0.041 0.043 0.045 0.048 0.050 0.051	0.007 0.009 0.012 0.014 0.016 0.019 0.021 0.025 0.027 0.029 0.030 0.032 0.034 0.036 0.038 0.040 0.042 0.043 0.043 0.049 0.050 0.050 0.050 0.057	0.008 0.011 0.013 0.016 0.018 0.020 0.022 0.024 0.026 0.028 0.030 0.032 0.031 0.036 0.038 0.010 0.012 0.015 0.017 0.019 0.056 0.058 0.058

N	E	<u>C</u>	<u>.500</u>	<u>.800</u>	.900	<u>.950</u>	<u>. 990</u>	.995
	27		0.040	0.046	0.050	0.053	0.059	0.061
	28	•	0.041	0.048	0.051	0.054	0.061	0.063
	29 <b>3</b> 0		0.042	0.049	0.053	0.056	0.062	0.065
	31		0.0112 0.0111	0.051	0.054	0.058	0.064	0.067
	32		0.043	0.052 0.054	0.056	0.059	0.066	0.068
	33		0.048	0.055	0.058	0.061	0.068	0.070
	رر بلا		0.050	0.057	0.059 0.061	0.063	0.069	0.072
	34 35		0.051	0.057	0.062	0.064	0.071	0.073
	36		0.052	0.060	0.064	0.066 0.067	0.073	0.075
	. 36 37		0.054	0.061	0.065	0.069	0.074	0.077
	38		0.055	0.063	0.067	0.009	0.076 0.078	0.079
	39	•	0.057	0.064	0.069	0.072	0.079	0.080 0.082
	40		0.058	0.066	0.070	0.074	0.081	0.002
	41		0.059	0.067	0.072	0.075	0.083	0.085
•	42		0.061	0.069	0.073	0.077	0.084	0.087
	43		0.062	0.070	0.075	0.079	0.086	0.089
	بلبل		0.064	0.072	0.076	0.080	0.088	0.090
	45		0.065	0.073	0.078	0.082	0.089	0.092
	46		0.067	0.075	0.079	0.083	0.091	0.094
	47		0.068	0.076	0.081	0.085	0.092	0.095
	48		0.069	0.078	0.082	0.086	0.094	0.097
	49		0.071	0.079	0.084	0.088	0.096	0.099
	50		0.072	0.081	0.086	0.090	0.097	0.100
	51 52		0.074	0.082	0.087	0.091	0.099	0.102
	72 52	•	0.075	0.084	0.089	0.093	0.101	0.104
	53 54		.0.077 0.078	0.085	0.090	0.097	0.102	0.105
	55		0.079	0.087 0.088	0.092	0.096	0.104	0.107
	55 56 57	•	0.081	0.000	0.093 0.095	0.097	0.105	0.108
	57		0.082	0.091	0.096	0.099 0.100	0.107 0.109	0.110
	58		0.084	0.093	0.098	0.102	0.109	0.112 0.113
	59		0.085	0.094	0.099	0.104	0.112	0.115
	60		0.087	0.096	0.101	0.105	0.113	0.117
•	61		0.088	0.097	0.102	0.107	0.115	0.118
	62		0.089	0.099	0.104	0.108	0.117	0.120
•	63		0.091	0.100	0.105	0.110	0.113	0.121
	64		0.092	0.102	0.107	0.111	0.120	0.123
	65	•	0.094	0.103	0.109	0.113	0.121	0.125
	66		0.095	0.105	0.110	0.114	0.123	0.126
	67		0.097	0.106	0.112	0.116	0.125	0.128

			•		•			
N	. <u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	<u>.950</u>	<u>•990</u>	<u>.995</u>
750	0		0.001	0.002	0.003	0.004	0.006	0.007
	1		0.002	0.004	0.005	0.006	0.009	0.010
	2 3 4 5 6		0.004	0.006	0.007	0.008	0.011	0.012
	3		0.005	0.007	0.009	0.010	0.013	0.015
	. 4		0.006	0.009	0.011	0.012	0.015	0.017
	5		0.008	0.011	0.012	0.014	0.017	0.019
	7		0.009	0.012	0.014	0.016	0.019	0.021
	8		0.010	0.014 0.015	0.016	0.017	0.021	0.023
	9		0.012	0.013	0.017 0.019	0.019 0.021	0.023	0.025
	ío		0.014	0.018	0.019	0.021	0.025 0.027	0.026 0.028
	11	* *	0.016	0.020	0.022	0.024	0.027	0.020
	12		0.017	0.021	0.024	0.026	0.020	0.032
	13		0.018	0.023	0.025	0.027	0.032	0.034
	14		0.020	0.024	0.027	0.029	0.034	0.035
	15		0.021	0.026	0.028	0.031	0.035	0.037
	16 17	•	0.022	0.027	0.030	0.032	0.037	0.039
	18		0.024 0.025	0.029 0.030	0.031	0.031	0.039	0.041
	19		0.025	0.030	0.033 0.034	0.035 0.037	0.040 0.042	0.042 0.044
	20		0.028	0.033	0.036	0.037	0.011	0.046
	21		0.029	0.034	0.037	0.040	0.045	0.047
I.	22		0.030	0.036	0.039	0.042	0.047	0.049
	23		0.032	0.037	0.010	0.043	0.049	0.051
	5/1		0.033	0.039	0.042	0.045	0.050	0.052
	, 25 26		0.034 0.036	0.040	0.043	0.046	0.052	0.054
	27		0.037	0.042 0.043	0.045 0.046	0.049 0.048	0.054	0.056
	28	,	0.038	0.011	0.048	0.049	0.055 0.057	0.057 0.059
	29		0.040	0.046	0.049	0.052	0.058	0.059
	30		0.041	0.047	0.051	0.054	0.060	0.052
	31		0.042	0.049	0.052	0.055	0.061	0.064
	32		0.0	0.050	0.054	0.057	0.063	0.065
	33 34		0.015	0.052	0.055	0.058	0.065	0.067
	35		0.046 0.048	0.053 0.054	0.057	0.060	0.066	0.069
	36		0.049	0.056	0.058 0.060	0.061	0.068	0.070
•	37	,	0.050	0.057	0.061	0.063 0.064	0.069 0.071	0.072 0.073
	38		0.052	0.059	0.063	0.066	0.072	0.075
• :	39		0.053	0.060	0.064	0.067	0.074	0.077
	ĬΦ		0.054	0.061	0.065	0.069	0.076	0.078
	41		0.056	0.063	0.067	0.070	0.077	0.080

N	E	C	.500	.800	<u>. 900</u>	<u>. 950</u>	<u>•990</u>	. 995
	42		0.057	0.064	0.068	0.072	0.079	0.081
	43	* •	0.058	0.066	0.070	0.073	0.080	0.083
	172 171		0.060	0.067	0.071	0.075	0.082	0.084
	45		0.061	0.068	0.073	0.076	0.083	0.086
	43 47		0.062	0.070	0.074	0.078	0.085	0.087
	48	,	0.064	0.071	0.076	0.079	0.086	0.089
	49		0.065 0.066	0.073	0.077	0.081	0.088	0.091
	50	•	0.068	0.074	0.078	0.082	0.089	0.092
	51		0.069	0.076	0.080	0.084	0.091	0.094
	52		0.070	0.077	0.081	0.085	0.092	0.095
	53		0.072	0.078 0.080	0.083	0.087	0.094	0.097
	53 54		0.073	0.081	0.084 0.086	0.088	0.095	0.098
	55		0.074	0.083	0.087	0.089	0.097	0.100
	56	=	0.076	0.084	0.088	0.091	0.098	0.101
	57		0.077	0.086	0.090	0.092 0.094	0.100	0.103
	58		0.078	0.087	0.091	0.095	0.102	0.104
	59		0.030	0.089	0.093	0.097	0.103	0.106
	60 51		0.081	0.089	0.094	0.098	0.105 0.106	0.107
	51		0.082	0.091	0.096	0.100	0.108	0.109 0.110
	62		0.084	0.092	0.097	0.101	0.109	0.110
	63		0.085	0.094	0.098	0.103	0.110	0.113
	64		0.086	0.095	0.100	0.104	0.112	0.115
	65		0.088	0.096	0.101	0.105	0.113	0.117
800	0	•	0.001	0.002	0.003	0.004	0.006	0.007
_	1		0.002	0.004	0.005	0.006	0.008	0.007
	2		0.003	0.005	0.007	0.008	0.010	0.012
	3 4 5 6		0.005	0.007	0.008	0.010	0.013	0.014
	4		0.006	0.008	0.010	0.011	0.014	0.016
	. 2		0.007	0.010	0.012	0.013	0.016	0.018
	. 7		0.008	0.011	0.013	0.015	0.018	0.019
	7 8	ч	0.010	0.013	0.015	0.016	0.020	0.021
	9		0.011	0.014	0.016	0.018	0.021	0.023
: .	10		0.012	0.016	0.018	0.020	0.023	0.025
	ü	•	0.013 0.015	0.017	0.019	0.021	0.025	0.027
	12		0.015	0.018	0.021	0.023	0.026	0.028
	13		0.017	0.020	0.022	0.024	0.028	0.030
	14		0.017	0.021	0.024	0.026	0.029	0.032
			0.010	0.023	0.025	0.027	0.031	0.033

<u>N</u>	F	<u>C</u>	<u>.500</u>	<u>.800</u>	<u>. 900</u>	<u>. 950</u>	<u>.990</u>	<u>- 995</u>
±	15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33	¥	0.020 0.021 0.022 0.023 0.025 0.025 0.026 0.027 0.028 0.030 0.031 0.032 0.033 0.035 0.036 0.037 0.038 0.040 0.041	0.02l4 0.025 0.027 0.028 0.029 0.031 0.032 0.03k 0.035 0.036 0.036 0.038 0.040 0.040 0.042 0.043 0.044 0.046 0.047 0.048	0.027 0.028 0.029 0.031 0.032 0.034 0.035 0.036 0.038 0.041 0.042 0.043 0.045 0.046 0.048 0.049 0.050 0.052	0.029 0.030 0.032 0.035 0.035 0.036 0.038 0.039 0.040 0.042 0.043 0.045 0.046 0.048 0.049 0.051 0.052 0.053	0.033 0.034 0.036 0.037 0.039 0.041 0.042 0.044 0.045 0.050 0.051 0.053 0.056 0.057 0.059 0.060	0.035 0.037 0.038 0.040 0.043 0.045 0.045 0.048 0.049 0.051 0.055 0.055 0.055 0.059 0.058 0.060 0.061
	34 35		0.043 0.045	0.050 0.051	0.053 0.055	0.056 0.058	0.062	0.064 0.066
	36 37		0.046 0.047	0.052 0.054	0.056 0.057	0.058 0.060	0.065	0.067
	38 39	,	0.048 0.050	0.055 0.056	0.059 0.060	0.062 0.063	0.067 0.069	0.070 0.072
	40	:	0.051 0.052	0.058 0.059	0.061 0.063	0.065 0.066	0.070 0.072	0.073 0.075
• ,	42		0.053	0.060 0.062	0.06L 0.065	0.067 0.069	0.073	0.076
ı	143 143	4	0.056	0.063	0.067	0.070	0.076	0.079
	115 146		0.057 0.058	0.064 0.066	0.068	0.072 0.072	0.078 0.079	0.081 0.082
	47		0,060	0.067	0.071	0.074	0.081	0.084
	48 49	•	0.061	0.068 0.069	0.072 0.073	0.076 0.077	0.082 0.083	0.085 0.086
	50		0.063	0.009	0.075	0.078	0.085	0.088
	51	•	0.065	0.072	0.076	0.080	0.087	0.089
	52		0.066	0.073	0.078	0.081	0.088	0.091
•	53. 54		0.067 0.068	0.075 0.076	0.079 0.080	0.083 0.084	0.090 0.091	0.092 0.094
	55		0.000	0.077	0.082	0.085	0.092	0.095
	. 56		0.070	0.079	0.083	0.037	0.094	0.097
	57		0.072	0.080	0.084	0.088	0.095	0.098
	58		0.073	0.081	0.086	0.089	0.097	0.099
	59		0.075	0.083	0.087	0.091	0.098	0.101

N	F	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>.950</u>	<u>.990</u>	<u>. 995</u>
	43 45 45 45 55 55 55 55 55 55 56 61 62		0.050 0.051 0.053 0.054 0.055 0.056 0.057 0.058 0.060 0.061 0.062 0.063 0.064 0.065 0.065 0.067 0.068 0.069 0.070 0.071 0.073 0.071	0.057 0.058 0.059 0.060 0.062 0.063 0.064 0.065 0.067 0.068 0.069 0.070 0.071 0.072 0.075 0.075 0.077 0.078 0.079 0.080 0.081	0.060 0.062 0.063 0.064 0.065 0.067 0.068 0.069 0.071 0.072 0.073 0.074 0.076 0.077 0.078 0.079 0.081 0.082 0.083 0.084	0.063 0.065 0.066 0.067 0.069 0.070 0.071 0.073 0.074 0.075 0.076 0.078 0.079 0.080 0.082 0.083 0.084 0.085 0.087	0.070 0.071 0.072 0.074 0.075 0.076 0.078 0.079 0.080 0.082 0.083 0.084 0.086 0.087 0.088 0.090 0.091 0.092 0.095 0.096	0.072 0.073 0.075 0.076 0.077 0.079 0.080 0.081 0.083 0.084 0.086 0.087 0.088 0.090 0.091 0.092 0.091 0.095 0.098 0.099
900	0 1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 19		0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.019 0.020 0.020	0.002 0.003 0.004 0.006 0.007 0.009 0.010 0.013 0.014 0.015 0.016 0.018 0.019 0.020 0.021 0.023 0.024 0.025 0.026	0.003 0.004 0.006 0.007 0.009 0.010 0.012 0.013 0.014 0.016 0.017 0.018 0.020 0.021 0.022 0.021 0.025 0.025 0.027	0.003 0.005 0.007 0.009 0.010 0.012 0.013 0.015 0.016 0.017 0.019 0.020 0.022 0.023 0.024 0.026 0.027 0.028 0.030 0.031	0.005 0.007 0.009 0.011 0.013 0.014 0.016 0.018 0.019 0.021 0.022 0.024 0.025 0.025 0.027 0.028 0.030 0.031 0.032	0.006 0.008 0.010 0.012 0.014 0.016 0.017 0.019 0.021 0.022 0.024 0.025 0.027 0.028 0.030 0.031 0.035 0.035 0.037

F	<u>C</u>	.500	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>. 995</u>
201234567890123456789014444444445555555555555555555555555555	<u>C</u>	0.023 0.024 0.025 0.025 0.027 0.029 0.030 0.031 0.032 0.033 0.035 0.035 0.035 0.036 0.037 0.040 0.041 0.042 0.043 0.045 0.045 0.045 0.050 0.050 0.050 0.051 0.055 0.055 0.056 0.056 0.060 0.061 0.062 0.063 0.064	0.027 0.029 0.030 0.031 0.032 0.035 0.035 0.035 0.037 0.043 0.043 0.045 0.045 0.045 0.050 0.051 0.050 0.055 0.056 0.057 0.058 0.059 0.059 0.062 0.063 0.063 0.065 0.068 0.069 0.070	0.030 0.031 0.032 0.034 0.036 0.037 0.039 0.040 0.041 0.045 0.045 0.047 0.050 0.051 0.053 0.053 0.053 0.053 0.059 0.063 0.065 0.065 0.065 0.065 0.065 0.065 0.065	0.032 0.033 0.035 0.035 0.037 0.039 0.042 0.042 0.045 0.045 0.045 0.050 0.050 0.051 0.055 0.055 0.055 0.065	0.037 0.038 0.039 0.041 0.043 0.045 0.045 0.050 0.051 0.055 0.055 0.055 0.058 0.059 0.062 0.063 0.063 0.068 0.068 0.070 0.071 0.072 0.073 0.075 0.070 0.071 0.072	995 0.038 0.040 0.041 0.043 0.045 0.045 0.052 0.055 0.055 0.055 0.057 0.059 0.063 0.065 0.065 0.067 0.068 0.069 0.072 0.073 0.076 0.077 0.078 0.081 0.082 0.088
59 60		0.066 0.067	0.073 0.075	0.077 0.07 <del>9</del>	0.081 0.082	0.087 0.089	0.090 0.091
	20123456789012345678904234567890123456789	20 21 22 22 23 24 25 26 27 28 29 30 31 31 33 33 33 34 44 44 44 45 45 55 55 55 55 55 55 55 55	20	20	20	20	20

<b>n</b>	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>. 995</u>
950	0123456789111214567890122345678901234567890423		0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009 0.010 0.012 0.013 0.014 0.015 0.016 0.018 0.020 0.021 0.025 0.026 0.027 0.028 0.027 0.028 0.029 0.030 0.031 0.035 0.031 0.035 0.036 0.039 0.031 0.035 0.036 0.039 0.040 0.041 0.042 0.043 0.046	0.002 0.003 0.004 0.006 0.007 0.008 0.010 0.012 0.013 0.014 0.016 0.017 0.018 0.019 0.020 0.021 0.025 0.025 0.025 0.025 0.025 0.026 0.027 0.028 0.029 0.031 0.035 0.036 0.037 0.038 0.036 0.037 0.038 0.040 0.041 0.042 0.043 0.045 0.046 0.047 0.045 0.050 0.051 0.052	0.002 0.004 0.006 0.007 0.008 0.010 0.011 0.012 0.014 0.015 0.016 0.017 0.020 0.021 0.022 0.024 0.025 0.026 0.025 0.026 0.027 0.028 0.030 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.031 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035	0.003 0.005 0.007 0.008 0.010 0.011 0.012 0.014 0.015 0.016 0.018 0.019 0.020 0.022 0.023 0.021 0.025 0.027 0.028 0.027 0.028 0.027 0.038 0.039 0.040 0.043 0.045 0.045 0.050 0.051 0.052 0.053	0.005 0.007 0.009 0.011 0.012 0.013 0.017 0.018 0.020 0.021 0.022 0.025 0.027 0.028 0.027 0.028 0.029 0.031 0.032 0.033 0.035 0.035 0.040 0.041 0.045 0.047 0.049 0.047 0.049 0.055 0.066 0.062 0.063	0.006 0.008 0.010 0.012 0.013 0.015 0.016 0.018 0.019 0.021 0.025 0.027 0.028 0.029 0.021 0.025 0.031 0.038 0.040 0.043 0.044 0.045 0.057 0.058 0.059 0.057 0.058 0.066 0.066

N	<u>F</u>	<u>C</u>	<u>.500</u>	.800	<u>.900</u>	. <u>•950</u>	<u>. 990</u>	<u>.995</u>
	山 山 山 山 山 山 山 山 山 山 山 山 山 山 山 り り り り り		0.047 0.048 0.049 0.050 0.051 0.052 0.053 0.054	0.053 0.054 0.055 0.056 0.057 0.059 0.060	0.056 0.057 0.059 0.060 0.061 0.062 0.063	0.059 0.060 0.061 0.063 0.064 0.065 0.066	0.065 0.066 0.067 0.068 0.070 0.071 0.072 0.073	0.067 0.068 0.069 0.071 0.072 0.073 0.074 0.075
1000	0123456789101121156789012222456789031		0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.021 0.022 0.023 0.021 0.025 0.026 0.027 0.028 0.029 0.030 0.031 0.032	0.002 0.003 0.004 0.006 0.007 0.00 0.010 0.011 0.012 0.014 0.015 0.016 0.017 0.018 0.019 0.020 0.021 0.022 0.024 0.025 0.026 0.027 0.028 0.029 0.030 0.031 0.032 0.031 0.032 0.033	0.002 0.004 0.005 0.007 0.008 0.009 0.011 0.012 0.013 0.014 0.015 0.017 0.018 0.019 0.020 0.021 0.022 0.024 0.025 0.026 0.027 0.028 0.029 0.030 0.031 0.035 0.036 0.037 0.038 0.039	0.003 0.005 0.006 0.008 0.009 0.010 0.012 0.013 0.014 0.016 0.017 0.018 0.019 0.021 0.022 0.023 0.021 0.025 0.027 0.028 0.029 0.030 0.031 0.032 0.031 0.035 0.035 0.036 0.037 0.038 0.039 0.040 0.042	0.005 0.007 0.008 0.010 0.012 0.013 0.015 0.016 0.017 0.019 0.020 0.021 0.023 0.024 0.025 0.027 0.028 0.029 0.030 0.032 0.032 0.035 0.035 0.035 0.037 0.038 0.035 0.037 0.038 0.037 0.038 0.037 0.038 0.039 0.040 0.041 0.045 0.045	0.005 0.007 0.009 0.011 0.013 0.014 0.016 0.017 0.018 0.020 0.021 0.023 0.024 0.025 0.027 0.028 0.029 0.031 0.032 0.031 0.032 0.031 0.036 0.037 0.038 0.039 0.041 0.046 0.047 0.048

N	F	<u>c</u>	<u>.500</u>	.800	<u>. 900</u>	<u>. 950</u>	<u>. 990</u>	<u>. 995</u>
	32		0.033	0.038	0.040	0.043	0.047	0.049
	33		0.034	0.039	0.041	0.014	0.049	0.050
•	37		0.035	0.040	0.043	0.045	0•050	0.052
	35		0.036	0.071	0.011	0.046	0.051	0.053
	36		0.037	0.042	0.045	0.047	0.052	0.054
	37		0.038	0.043	0.046	o.048	0.053	0.055
	38		0.039	٥٠٥إبار	0.047	0.050	0.055	0.056
	39		0.040	0.045	0.048	0.051	0.056	0.058
	40		0.041	0.046	0.049	0 <b>.05</b> 2	0.057	0.059
	41		0.042	0.047	0.050	0.053	0.058	0.060
	42		0.043	0.048	0.051	0.054	0.059	0.061
	43		0.011	0.049	0.052	0.055	0.060	0.062
	111		0.045	0.050	0.054	0.056	0.061	0.064
	45		0.046	0.051	0.055	0.057	0.063	0.065
	46		0.047	0.052	0.056	0.058	0.064	0.066
	47		0.048	0.054	0.057	0.060	0.065	0.067
	48		0.049	0.055	0.058	0.061	0.066	0.068
	719		0.050	0.056	0.059	0.062	0.067	0.069
	50		0.051	0.057	0.060	0.063	0.068	0.071

#### **APPENDIX 3B**

Table 2
TWO-SIDED 90% CONFIDENCE LIMITS ON BINOMIAL CONFIDENCE LIMITS FOR DEFECTS

n	1	2	3	4	5
0 1 3 4 5	.000 .950 .050 1.600	.000 .776 .025 .975 .224 1.000	.000 .631 .017 .865 .135 .983 .369 1.000	.000 .527 .013 .751 .098 .902 .249 .987 .473 1.600	.000 .451 .010 .658 .076 .811 .189 .924 .342 .990 .549 1.000

n	6	7	. 8	9	10
0 1 2 3 4 5	.000 .393 .009 .582 .063 .729 .153 .847 .271 .937 .418 .991	.000 .348 .007 .521 .053 .659 .129 .775 .225 .871 .341 .947	.000 .312 .006 .470 .046 .600 .111 .711 .193 .807 .289 .889	.0C0 .263 .0C6 .429 .041 .550 .098 .655 .169 .749 .251 .831	.000 .259 .005 .394 .037 .507 .087 .607 .150 .696 .223 .777
6 7 8 9 10	.607 1.000	.479 .993 .652 1.000	.400 .954 .530 .994 .688 1.660	.345 .902 .450 .959 .571 .994 .717 1.CCO	.304 .850 .393 .913 .493 .963 .606 .995 .741 1.000

APPENDIX 3B

Table 2 (Continued)

x	11	12	13	14	15
0 1 2 3 5 6 7 8 9 10 11 12 13 14	.000 .238 .005 .365 .033 .470 .079 .564 .135 .650 .200 .729 .271 .800 .350 .865 .436 .921 .530 .967 .635 .995	.000 .221 .004 .339 .030 .438 .072 .527 .123 .609 .181 .684 .245 .755 .316 .819 .391 .877 .473 .928 .562 .970 .661 .996 .779 1.000	.CCC .206 .CC4 .317 .C28 .410 .O66 .495 .113 .572 .166 .645 .224 .713 .287 .776 .355 .E34 .428 .EE7 .505 .934 .590 .972 .6E3 .996 .794 1.00C	.0CC .193 .CC4 .297 .026 .386 .061 .466 .104 .540 .153 .609 .206 .675 .264 .736 .325 .794 .301 .847 .460 .896 .534 .939 .614 .974 .703 .996 .807 1.000	.000 .181 .003 .279 .024 .363 .057 .440 .097 .511 .142 .578 .191 .640 .244 .700 .360 .756 .360 .809 .422 .858 .489 .903 .560 .943 .637 .976 .721 .997
15		<u>'.                                    </u>		1.000	.619 1.000

Example: Conserved from sample 5/10. The 90% confidence limits for the population are .213 and .777.

x	16	17	18	19	20
1 2 3 4 5	.000 .171 .003 .264 .023 .344 .053 .417 .090 .484 .132 .549	.000 .162 .003 .250 .021 .326 .050 .396 .085 .461 .124 .522	.000 .153 .003 .238 .020 .310 .047 .377 .080 .439 .116 .498	.000 .146 .003 .226 .019 .296 .044 .359 .075 .419	.000 .139 .003 .216 .018 .282 .042 .344 .071 .401 .104 .455
6 7 8 9 10	.178 .608 .227 .667 .279 .721 .333 .773 .392 .822	.166 .580 .212 .636 .260 .629 .311 .740 .364 .788	.156 .554 .199 .608 .244 .659 .291 .709 .341 .756	.147 .529 .188 .582 .229 .632 .274 .679 .321 .726	.139 .507 .177 .558 .217 .606 .259 .653 .302 .698
11 12 13 14 15	.451 .868 .516 .910 .583 .947 .656 .977 .736 .997	.420 .834 .478 .876 .539 .915 .604 .950 .674 .979	.392 .801 .446 .844 .502 .884 .561 .920 .622 .953	.368 .771 .418 .£12 .471 .£53 .524 .£90 .581 .925	.347 .741 .394 .783 .442 .823 .493 .861 .545 .896
16 17 18 19 20	.829 1.0CJ	.750 .997 .838 1.000	.690 .980 .762 .997 .847 1.000	.641 .956 .704 .981 .774 .997 .854 1.000	.599 .929 .656 .958 .718 .982 .784 .997 .861 1.000

Example: Observed from sample 10/20. The 90% confidence limits for the population are .302 and .698.

APPENDIX 3B

Table 2 (Continued)

n					ı
z \	22	- 24	26 .	28	30
0	.000 .127	.000 .117	.000 ,109	.000 .101	.000 .095
1 2 3 4 5	.002 .198 .016 .260 .038 .316 .065 .370 .094 .420	.002 .183 .015 .240 .035 .292 .059 .342 .086 .389	.002 .170 .014 .223 .032 .272 .054 .318 .079 .362	.002 .158 .013 .208 .03C .254 .050 .297 .073 .339	.0C2 .149 .012 .196 .028 .238 .047 .280 .068 .319
6 7 8 9 10	.124 .468 .160 .515 .196 .561 .233 .605 .271 .647	.115 .435 .146 .479 .178 .522 .211 .563 .246 .603	.106 .406 .134 .447 .163 .487 .194 .526 .226 .564	.098 .379 .124 .419 .151 .457 .179 .493 .208 .531	.091 .357 .115 .394 .140 .429 .166 .466 .193 .499
11 12 13 14 15	.311 .689 .353 .729 .395 .767 .439 .804 .485 .840	.282 .643 .319 .661 .357 .718 .397 .754 .437 .789	.259 .602 .292 .638 .327 .673 .362 .708 .398 .741	.238 .565 .270 .600 .301 .633 .333 .667 .367 .699	.221 .533 .249 .567 .279 .597 .308 .630 .339 .661
16 17 18 19 20	.532 .876 .580 .906 .630 .935 .684 .962 .740 .984	.478 .822 .521 .854 .565 .885 .611 .914 .658 .941	.436 .774 .474 .806 .513 .837 .553 .866 .594 .894	.400 .730 .435 .762 .469 .792 .507 .821 .543 .849	.370 .692 .403 .721 .433 .751 .467 .779 .501 .£07
21 22 23 24 25	.802 .998 .873 1.000	.708 .965 .760 .985 .817 .998 .883 1.000	.638 .921 .682 .946 .728 .968 .777 .986 .830 .998	.5E1 .876 .621 .902 .661 .927 .703 .950 .746 .970	.534 .834 .571 .860 .606 .885 .643 .909 .681 .932
26 27 26 29 30			.891 1.000	.792 .987 .842 .996 .£99 1.000	.720 .953 .762 .972 .804 .988 .851 .998 .905 1.000

Example: Observed from sample 6/30. The 90% confidence limits for the population are .091 and .357.

#### **APPENDIX 3B**

Table 2

TWO-SIDED 90% CONFIDENCE LIMITS ON BINOMIAL p

x	35		40	x	35	40
0	.000 .0	82 .000	.072			
1 2 3 4 5	.010 .1 .024 .2 .040 .2	28 .001 69 .009 06 .021 43 .035 77 .051	.149 .183 .215	26 27 28 29 30	.595 .659 .626 .381 .657 .902 .689 .922 .723 .942	.508 .774 .534 .796 .559 .816 .586 .338 .613 .858
6 7 8 9 10	.078 .3 .098 .3 .119 .3 .141 .4 .163 .4	43 .085 74 .103 05 .123	.304 .331 .360	31 32 33 34 35	.757 .960 .794 .976 .831 .990 .372 .999 .918 1.000	.640 .877 .669 .897 .696 .915 .725 .933 .755 .949
11 12 13 14 15	.187 .4 .211 .4 .235 .5 .261 .5 .286 .5	96 .134 24 .204 53 .226	441	36 37 38 39 40		.785 .965 .817 .979 .851 .991 .887 .999 .928 1.000
16 17 18 19 20	.311 .6 .337 .6 .364 .6 .391 .6 .419 .7	36 .292 63 .314 89 .338	.567 .592 .615	41 42 43 44 45		
21. 22 23 24 25	.447 .7 .476 .7 .504 .7 .533 .8 .564 .8	65 .408 89 .433 13 .457	.686 .708 .731	46 47 48 49 50		

Example: Observed from sample 35/50. The 90% confidence limits for the population are .576 and .805.

APPENDIX 3B
Table 2 (Continued)

x	n	45		50	x		45	1	50
0	.000	.064	.000	.058		1		+	
1 2 3 4 5	.001 .008 .018 .031 .045	.101 .133 .163 .192 .220	.001 .007 .017 .028 .040	.091 .120 .148 .174 .199	26 27 28 29 30	.445 .467 .488 .511 .533	.704 .723 .742 .762 .782	•395 •414 •435 •455 •475	.643 .662 .680 .698
6 7 8 9 10	.060 .075 .092 .108 .126	.246 .273 .297 .323 .348	.054 .067 .082 .097 .113	.223 .247 .270 .293 .316	31 32 33 34 35	.558 .581 .603 .628 .652	.801 .820 .838 .856 .874	.494 .514 .536 .556 .576	•734 •753 •771 •788 •805
11 12 13 14 15	.144 .162 .180 .199 .218	.372 .397 .419 .442 .467	.129 .145 .161 .178 .195	•337 •359 •381 •403 •424	36 37 38 39 40	.677 .703 .727 .754 .780	.892 .908 .925 .940	•597 •619 •641 •663 •684	.822 .839 .855 .871 .887
16 17 18 19 20	.238 .258 .277 .296 .317	.489 .512 .533 .555 .576	.212 .229 .247 .266 .282	.444 .464 .486 .506 .525	41 42 43 44 45	.808 .837 .867 .899	.969 .982 .992 .999	.707 .730 .753 .777 .801	.903 .918 .933 .946 .960
21 23 24 25	•337 •359 •379 •402 •424	.598 .621 .641 .663 .683	• 302 • 320 • 338 • 357 • 375	.545 .565 .586 .605	46 47 48 49 50			.826 .852 .880 .909	.972 .983 .993 .999

Example: Observed from sample 35/50. The 90% confidence limits for the population are .576 and .805.

APPENDIX 3B

## Table 2 (Continued)

## TWO-SIDED 90% CONFIDENCE LIMITS ON BINOMIAL P

х		
C .	.000	•049
1 2 3 4 5	.001 .006 .014 .023 .033	.076 .101 .124 .146 .167
6 7 8 9 10	.045 .056 .068 .080	.187. .208 .228 .248 . <b>2</b> 66
11 12 13 14 15	.106 .120 .133 .147 .161	.285 .304 .323 .341 .358

n = 60								
x	$n - \alpha$							
16 17 18 19 20	.175 .189 .204 .218	.376 .394 .412 .429 .445						
21 22 23 24 25	.248 .263 .278 .292 .309	.463 .481 .498 .515						
26 27 28 29 30	.323 .340 .357 .374 .387	.547 .563 .581 .597 .613						

x		
31 32 33 34 35	.403 .419 .437 .453 .470	.628 .643 .660 .677
36	.485	.708
37	.502	.722
38	.519	.737
39	.537	.752
40	.555	.767
41	.571	.782
42	.588	.796
43	.606	.811
44	.624	.825
45	.642	.839

X	
46 .659 .853	3
47 .677 .867	
48 .696 .880	
49 .715 .894	_
50 .734 .90	
)	•
51 .752 .920	٠.
52 .772 .93	
53 .792 .94	4
54 .813 .95	5
55 .833 .96'	7
.56 .854 .57	
.9898	
56 .699 .99	
59 .924 .99	
60 .951 1.00	С

**APPENDIX 3B** 

#### Table 2 (Continued)

n = EC

				$n = \epsilon 0$							
х			х			x		1	x		
G	.000	.037	,					. ·			
12345	.001 .004 .010 .017 .025	.058 .077 .094 .111 .127	21' 22 23 24 25	.183 .194 .205 .216 .228	.356 .368 .382 .395 .408	41 42 43 44 45	.414 .428 .440 .452 .465	.610 .621 .633 .644 .657	61 62 63 64 65	.672 .685 .698 .712	.838 .849 .860 .870 .881
6 7 8 9	.033 .042 .051 .060 .069	.143 .158 .173 .188 .203	26 27 28 29 30	.24C .250 .262 .274 .284	.422 .436 .447 .460 .472	46 47 48 49 50	.477 .490 .503 .515	.669 .680 .692 .703 .716	66 67 68 69 70	.741 .754 .768 .783 .797	.891 .901 .911 .921 .931
11 12 13 14 15	.079 .089 .099 .109	.217 .232 .246 .259 .274	31 32 33 34 35	.297 .308 .320 .331 .343	.485 .497 .510 .523 .535	51 52 53 54 55	.54C .553 .564 .57E .592	.726 .738 .750 .760 .772	71 72 73 74 75	.812 .227 .842 .857 .873	.940 .949 .958 .967 .975
16 17 18 19 20	.130 .140 .151 .162 .172	.288 .302 .315 .328 .343	36 37 38 39 40	.356 .367 .379 .390 .402	.548 .560 .572 .586 .598	56 57 58 59 60	.605 .618 .632 .644	.784 .795 .806 .817 .828	76 77 78 79 EC	.906 .923 .942 .963	.983 .990 .996 .999

Example: Observed from sample 50/80. The 90% confidence limits for the population are .528 and .716.

APPENDIX 3B

## Table 2 (Continued)

n = 100

			n = 100	
х		х	x	x
Ü	.000 .030			
1 2 2 4 5	.CC1 .C47	26 .190 .343	51 .423 .596	76 .679 .828
	.CC4 .O61	27 .198 .353	52 .433 .605	77 .690 .838
	.CCE .O75	28 .207 .364	53 .443 .615	78 .702 .846
	.C14 .CE9	29 .215 .973	54 .453 .616	79 .712 .854
	.OLC .1C2	30 .224 .384	55 .462 .635	80 .723 .863
6	.027 1115	31 .234 .395	56 .472 .645	EJ .734 .E72
7	.033 .127	32 .244 .405	57 .482 .654	E2 .745 .EE1
8	.040 .140	33 .252 .415	58 .492 .665	E2 .756 .EC9
9	.048 .152	34 .262 .426	59 .503 .674	E4 .767 .E97
<b>1</b> 0	.055 .164	35 .271 .437	60 .513 .683	E5 .779 .905
11	.063 .176	36 .281 .446	61 .523 .692	£6 .79C .914
12	.071 .187	37 .289 .456	62 .534 .702	£7 .£01 .921
13	.079 .199	38 .298 .466	63 .544 .711	£8 .£13 .929
14	.086 .210	39 .308 .477	64 .554 .719	£9 .£24 .937
15	.095 .221	40 .317 .487	65 .563 .729	90 .£36 .945
16	.103 .233	41 .326 .497	66 .574 .738	91 .648 .952
17	.111 .244	42 .335 .508	67 .585 .748	92 .860 .960
18	.119 .255	43 .346 .518	68 .595 .756	93 .873 .967
19	.126 .266	44 .355 .528	69 .605 .766	94 .885 .973
20	.137 .277	45 .365 .538	70 .616 .776	95 .898 .980
21	.146 .268	46 .374 .547	71 .627 .785	96 .911 .986
22	.15498	47 .385 .557	72 .636 .793	57 .925 .992
23	.162 .310	48 .395 .567	73 .647 .802	98 .939 .996
24	.172 .321	49 .404 .577	74 .657 .810	99 .953 .999
25	.181 .331	50 .414 .586	75 .669 .819	100 .970 1.000

example: Observed from sample 50/100. The 90% confidence limits for the population are .414 and .586.

#### **APPENDIX 3B**

#### Table 2 (Continued)

#### TWO-SIDED 95% CONFIDENCE INTERVALS FOR BINOMIAL DISTRIBUTION

The following lists the 95% confidence interval for the binomial distribution. These tables are similar to the 90% tables.

#### TWO-SIDED 95% CONFIDENCE LIMITS FOR DEFECTS

x	1		2		3			4 .	5	
0	•000	•975	.000	.842	.000	.708	•000	•602	.000	.522
1 2 3 4 5	•025	1.000	.013 .158	.937 1.000	.008 .094 .292	.906 .992 1.000	.006 .068 .194 .398	.306 .932 .994 1.000	.005 .053 .147 .284 .478	.716 .853 .947 .995 1.000

x	. 6		. 7			8		9	10	
0	.000	•459	.000	.410	.000	•369	.000	.336	.000	.308
1 2 3 4 5	.004 .043 .118 .223	.641 .777 .882 .957	.004 .037 .099 .184 .290	.579 .710 .816 .901	.003 .032 .085 .157 .245	.527 .651 .755 .843	.003 .028 .075 .137 .212	.483 .600 .701 .788 .863	.003 .025 .067 .122 .187	.445 .556 .652 .738 .813
6 7 8 9 10		1.000	.421 .590	.996 1.000	.349 .473 .631	.968 .997 1.000	.299 .400 .517 .664	.925 .972 .997 1.000	.262 .348 .444 .555 .692	.878 .933 .975 .997 1.000

APPENDIX 3B

Table 2 (Continued)

X	11		12	12		13		14		15
0	.000	.285	.000	.265	.000	.247	.000	.232	.000	.218
1 2 3 4 5 6 7 8 9	.002 .023 .060 .109 .167 .234 .308 .390	.413 .518 .610 .692 .766 .833 .391 .940 .977	.002 .021 .055 .099 .151 .211 .277 .349	.385 .484 .572 .651 .723 .789 .349 .901	.002 .019 .050 .091 .139 .192 .251 .316 .386	.360 .454 .538 .614 .684 .749 .208 .861 .909	.002 .018 .047 .084 .128 .177 .230 .289 .351	.339 .428 .508 .581 .649 .711 .770 .823 .872	.002 .017 .043 .078 .118 .163 .213 .266 .323	.319 .405 .481 .551 .616 .677 .734 .787
10 11 12 13 14 15	.587 .715	.998 1.000	.516 .615 .735	979 998 1.000	.462 .546 .640 .753	.950 .981 .998 1.000	.419 .492 .572 .661 .768	.916 .953 .982 .998 1.000	.384 .449 .519 .595 .631 .782	.882 .922 .557 .983 .998 1.000

Example: Observed from sample 5/10. The 95% confidence limits for the population are .187 and .813.

APPENDIX 3B
Table 2 (Continued)

x	16		17	17		18		19		
0	•000	.206	.000	.195	•000	.185	.000	.176	.000	.156
1 2 3 4 5	.002 .016 .040 .073 .110	.302 .383 .456 .524 .587	.001 .015 .038 .068 .103	.287 .364 .434 .499 .560	.001 .014 .036 .064 .097	.273 .347 .414 .476 .535	.001 .013 .034 .061 .091	.260 .331 .3% .456 .512	.001 .012 .032 .057 .037	.249 .317 .379 .437 .491
6 7 8 9 10	.152 .198 .247 .299 .354	.646 .701 .753 .802 .848	.142 .184 .230 .278 .329	.617 .671 .722 .770 .816	.133 .173 .215 .260 .308	.590 .643 .692 .740 .785	.126 .163 .203 .244 .289	.565 .616 .665 .711 .756	.119 .154 .191 .231 .272	.543 .592 .639 .685
11 12 13 14 15	.413 .476 .544 .617 .698	.890 .927 .960 .984 .998	.383 .440 .501 .566 .636	.858 .897 .932 .962 .985	.357 .410 .465 .524 .586	.827 .867 .903 .936 .964	.335 .384 .435 .388 .544	.797 .837 .874 .909 .939	.315 .361 .408 .457 .509	.769 .809 .846 .881
16 17 18 19 20	•794	1.000	.713 .805		.653 .727 .815	.986 .999 1.000	.604 .669 .740 .824	.966 .987 .999	.563 .621 .583 .751 .832	.943 .963 .063 .999 1.000

APPENDIX 3B

Table 2 (Continued)

n n	<u> </u>	22		22				1 35		
X "		21	2	2 ,		23	4	4		25
0	.000	.161	.000	.154	.000	.148	•000	.142	•000	.137
1 2	.001 .012	.238 .304	.001	.229 .292	.001	.219	.001	.211	.001	.203
2 3	.030	.363	.029	•349	.028	.336	.027	323	.025	.312
4 5	.054 .082	.419 .471	.052	.403 .453	.050	.388 .436	.047	.374 .421	•068	.407
6 7 8 9 10	.113 .146 .101 .218 .257	.522 .570 .616 .660 .702	.107 .139 .172 .207 .244	.502 .549 .593 .636 .678	.102 .132 .164 .197 .232	.484 .529 .573 .615	.098 .126 .156 .188 .221	.467 .512 .553 .594 .634	.094 .121 .149 .180	.451 .494 .525 .575 .614
11 12 13 14 15	.298 .340 .384 .430 .478	.743 .782 .819 .854 .867	.282 .322 .364 .407 .451	.718 .756 .793 .828 .861	.268 .306 .345 .385 .427	.694 .732 .768 .803	.256 .291 .328 .366 .406	.672 .709 .744 .779 .812	.244 .278 .313 .349 .386	.651 .687 .722 .756 .789
16 17 18 10 20	.529 .581 .637 .696 .762	.918 .946 .970 .988 .999	.498 .547 .597 .651 .708	.893 .922 .948 .971 .989	.471 .516 .564 .612 .664	.868 .898 .925 .950	.447 .488 .533 .579 .626	.844 .874 .902 .929	.425 .465 .506 .549 .593	.820 .851 .879 .906
21 22 23 24 25	<b>.</b> 839	1.000	.771 .846	.999 1.000	.719 .761 .852	•989 •999 1.000	.677 .730 .789 .858	•973 •990 •999 <b>1.000</b>	.688 .797 .863	.975 .999 1.000

Example: Observed from sample 10/25. The 95% confidence limits for the population are .211 and .614.

APPENDIX 3B

Table 2 (Continued)

۲		1	<u></u>	1		<del>1</del>						
	x		26		28		30	3	35	<u>_</u> '	40	
.	0	.000	.132	.000	.123	.000	.116	.000	.100	.000	.088	
	1 2 3 4 5	.001 .009 .024 .044 .066	.197 .251 .301 .349	.001 .009 .023 .040	.184 .235 .282 .327 .369	.001 .008 .021 .038 .056	.172 .221 .265 .307	.001 .007 .018 .032 .048	.149 .192 .230 .268 .303	.001 .006 .016 .028 .042	.132 .169 .204 .236	
	6 7 8 9 10	.090 .116 .143 .172 .202	.436 .478 .518 .557 .595	.083 .107 .132 .159 .186	.410 .449 .487 .524	.077 .099 .123 .148 .173	.386 .423 .459 .494	.066 .084 .104 .125 .147	.336 .369 .401 .433	.057 .073 .090 .109	.298 .328 .357 .385 .412	
	11 12 13 14 15	.234 .266 .299 .334 .369	.631 .666 .701 .734 .766	.215 .245 .275 .306 .339	•594 •628 •661 •694 •725	.199 .227 .255 .283 .313	.561 .594 .626 .657 .687	.169 .192 .215 .239 .263	.493 .522 .551 .578 .607	.146 .166 .185 .206	.439 .465 .491 .517	
	16 17 18 19 20	.405 .4/.3 .482 .522 .564	.798 .828 .857 .384 .910	.372 .406 .440 .476 .513	.755 .785 .814 .341 .868	•343 •374 •406 •439 •472	.717 .745 .773 .801 .827	.258 .314 .340 .366 .393	.634 .660 .686 .712 .737	.249 .271 .293 .315 .338	.567 .590 .615 .639	
		.607 .651 .699 .749	.934 .956 .976 .991 .999	.551 .590 .631 .673	.893 .917 .939 .960 .977	.506 .541 .577 .614 .652	.852 .877 .901 .923	.422 .449 .478 .507 .537	.761 .785 .808 .831 .853	.361 .385 .410 .433 .458	.685 .707 .729 .751 .773	
	26 27 26 29 30	.863	1.000	.765 .316 .877	.991 .999 1.000	.693 .735 .779 .826 .884	.962 .979 .992 .999	.567 .599 .631 .664	.875 .896 .916 .934 .952	.423 .509 .535 .561 .588	.794 .815 .834 .854 .873	
	31 32 33 34 35	ï						.732 .770 .808 .851	.968 .982 .993 .999 1.000	.615 .643 .672 .702 .732	.691 .910 .927 .943 .958	
	36 37 38 39 40	Exampl	o. Oh	omea e	rom sam				onfiden	.76. .796 .831 .868 .912	.972 .984 .994 .999 1.000	

Example: Observed from sample 25/40. The 95% confidence limits for the population are .458 and .773.

APPENDIX 3B

### Table 2 (Continued)

n = 50

x		x	
0 1 2 3 4 5	.000 .071 .001 .106 .005 .137 .013 .165 .022 .192 .033 .218	26 27 28 29 30	.374 .663 .394 .682 .412 .700 .432 .718 .452 .736
6	.045 .243	31	.473 .753
7	.058 .267	32	.492 .771
8	.072 .291	33	.512 .788
9	.086 .314	34	.533 .805
10	.100 .338	35	.554 .821
11	.115 .360	36	.576 .837
12	.131 .381	37	.596 .854
13	.146 .404	38	.619 .869
14	.163 .424	39	.640 .885
15	.179 .446	40	.662 .900
16	.195 .467	41	.686 .914
17	.212 .488	42	.709 .928
18	.229 .508	43	.733 .942
19	.247 .527	44	.757 .955
20	.264 .548	45	.782 .967
21	.282 .568	46	.8(8 .978
22	.300 .588	47	.835 .987
23	.318 .606	48	.863 .995
24	.337 .626	49	.894 .999
25	.356 .644	50	.929 1.000

Example: Observed from sample 15/50. The 95% confidence limits for the population are .179 and .446.

APPENDIX 3B
Table 2 (Continued)

n = 100

			 				· .						
x			×								х		
0	•000	•036											
1 2 3 4 5	.000 .002 .006 .011	.054 .070 .035 .099 .113	26 27 28 29	.177 .187 .195 .204 .213	.357 .368 .378 .390 .399		51 52 53 54 55	.408 .418 .427 .437 .447	.611 .620 .630 .639		76 77 78 79 80	.664 .676 .686 .697 .708	.839 .848 .856 .865 .874
6 7 8 9	.022 .029 .035 .042 .049	.126 .139 .152 .164 .176	31 34 35	.221 .230 .240 .248 .257	.410 .420 .431 .441 .452		56 57 58 59 60	.457 .467 .477 .487 .497	.659 .668 .678 .687 .697		81 82 83 84 85	.719 .731 .742 .753 .764	.851 .890 .893 .906
11 12 13 14 15	.056 .064 .071 .078 .086	.188 .200 .212 .223 .236	36 37 38 39 40	.266 .276 .284 .294 .303	.463 .472 .482 .493 .503		61 62 63 64 65	.507 .518 .520 .537 .548	.706 .716 .724 .734 .743		36- 87 87 89 90	.777 .788 .800 .812 .824	.922 .929 .936 .944 .951
16 17 18 19 20	.094 .102 .110 .119 .126	.247 .258 .269 .281 .292	41 42 43 44 45	.313 .322 .332 .341 .350	.513 .523 .533 .543 .553		66 67 68 69 70	.559 .569 .580 .590 .601	.752 .760 .770 .779	•	91 92 93 94 95	.836 .848 .861 .674 .387	.958 .965 .971 .973
21 22 23 24 25	.135 .144 .152 .161 .169	.303 .314 .324 .336 .347	46 47 48 49 50	.361 .370 .380 .389 .398	.563 .573 .582 .592 .602	•	71 72 73 74 75	.610 .622 .632 .643 .653	.796 .805 .813 .823 .831		96 97 98 99 100	.901 .915 .930 .946 .964	.909 .994 .998 1.000 1.000

Example: Observed from sample 50/100. The 95% confidence limits for the population are .398 and .602.

#### **APPENDIX 3B**

#### Table 2 (Continued)

#### 99% CONFIDENCE INTERFVAL FOR BINOMIAL DISTRIBUTION

The following lists the 99% confidence interval for the binomial distribution. These tables are similar to the 90% tables.

#### TWO-SIDED 99% CONFIDENCE LIMITS FOR DEFECTS

x	1	2	3	4	. 5
0	.000 .995	.000 .929	.000 .829	.000 .734	.000 .653
1 2 3 4 5	.005 1.000	.003 .997 .071 1.000	.002 .959 .041 .998 .171 1.000	.001 .889 .029 .971 .111 .999 .266 1.000	.001 .815 .023 .917 .083 .977 .185 .999 .347 1.000
x	6	7	8	9	10
0	.000 .586	.000 .531	.000 .484	.000 .445	.000 .411
1 2 3 4 5	.001 .746 .019 .856 .066 .934 .144 .981 .254 .999	.001 .685 .016 .797 .055 .882 .118 .945 .203 .984	.001 .632 .014 .742 .047 .830 .100 .900 .170 .953	.001 .585 .012 .693 .042 .781 .087 .854 .146 .913	.001 .544 .011 .648 .037 .735 .077 .809 .128 .872
6 7 8 9 10	.414 1.000	.315 .999 .469 1.000	.258 .986 .363 .999 .516 1.000	.219 .958 .307 .988 .415 .999 .555 1.000	.191 .923 .265 .963 .352 .989 .456 .999 .589 1.000

APPENDIX 3B

Table 2 (Continued)

, n		11		12		13		14		15
0	.000	.382	.000	.357	.000	•335	.000	.315	.000	.298
1 2 3 4 5	.000 .010 .033 .069 .114	.509 .608 .693 .767 .831	.000 .009 .030 .062 .103	.477 .573 .655 .728 .791	.000 .008 .028 .057 .094	.449 .541 .621 .691 .755	.000 .008 .026 .053 .087	.424 .512 .589 .658 .720	.000 .007 .024 .049 .080	.402 .486 .561 .627 .688
7 8 9 10	.233 .307 .392 .491	.931 .967 .990 1.000	.209 .272 .345 .427	.897 .938 .970 .991	.189 .245 .309 .379	.862 .906 .943 .972	.172 .223 .280 .342	.828 .873 .913 .947	.159 .205 .256 .312	.795 .841 .883 .920
11 12 13 14 15	.618	1.000	.523 .643	1.000	.459 .551 .665	.992 1.000 1.000	.411 .488 .576 .685	.974 .992 1.000 1.000	.373 .439 .514 .598 .702	.951 .976 .993 1.000

Example: Observed from sample 5/10. The 99% confidence limits for the population are .128 and .872.

APPENDIX 3B
Table 2 (Continued)

x	16	17	18	19	20
0	.000 .282	.000 .268	.000 .255	.000 .243	.000 .233
1 2 3 4 5	.000 .381	.000 .363	.000 .346	.000 .331	.000 .317
	.007 .463	.006 .441	.006 .422	.006 .404	.005 .387
	.022 .534	.021 .510	.020 .488	.019 .468	.018 .449
	.045 .599	.043 .573	.040 .549	.038 .527	.036 .507
	.075 .658	.070 .631	.065 .605	.062 .582	.058 .560
6	.109 .714	.101 .685	.095 .658	.090 .633	.085 .610
7	.147 .764	.137 .735	.128 .707	.121 .681	.114 .657
8	.189 .811	.176 .781	.165 .753	.155 .726	.146 .701
9	.236 .853	.219 .824	.205 .795	.192 .768	.181 .743
10	.286 .891	.265 .863	.247 .835	.232 .808	.218 .782
11.	.342 .925	.315 .899	.293 .872	.274 .845	.257 .819
12.	.401 .955	.369 .930	.342 .905	.319 .879	.299 .854
13.	.466 .978	.427 .957	.395 .935	.367 .910	.343 .886
14.	.537 .993	.490 .979	.451 .960	.418 .938	.390 .915
15.	.619 1.000	.559 .994	.512 .980	.473 .962	.440 .942
16 17 18 19 20	.718 1.000	.637 1.000 .732 1.000	.578 .994 .654 1.000 .745 1.000	.532 .981 .596 .994 .669 1.000 .757 1.000	.493 .964 .551 .982 .613 .995 .683 1.000 .767 1.000

Example: Observed from sample 10/20. The 99% confidence limits for the population are .218 and .782.

APPENDIX 3B
Table 2 (Continued)

x	. 22		2	4	2	26	2	28	3	30
0	.cco .:	214	.000	.198	.000	.184	.000	.172	.000	.162
1 2 3 4 5	.005 .016 .032	292 358 416 470 520	.000 .004 .015 .029	.271 .332 .387 .438 .485	.000 .004 .013 .027	.253 .310 .362 .410 .455	.000 .004 .012 .025	.237 .291 .340 .385 .428	.000 .004 .012 .023 .038	.223 .274 .320 .363 .404
6 7 8 9	.102 .0 .131 .0 .162 .0	567 612 655 695 734	.069 .093 .119 .146 .176	.531 .573 .614 .653 .690	.064 .085 .109 .134 .161	.498 .538 .578 .615 .651	.059 .078 .100 .123 .148	.469 .508 .545 .581 .616	.054 .073 .093 .114 .137	.443 .480 .516 .550 .583
11 12 13 14 15	.266 .305 .345	771 8C5 838 869 898	.2C7 .240 .274 .310 .347	.726 ,760 .793 .824	.189 .218 .249 .281 .314	.686 .719 .751 .762 .811	.173 .200 .228 .257 .287	.649 .662 .713 .743 .772	.160 .185 .211 .237 .265	.616 .647 .678 .707 .735
16 17 18 19 20	.480 .530 .584	924 947 968 984 995	.386 .427 .469 .515 .562	.381 .907 .931 .952 .971	.349 .385 .422 .462 .502	.839 .866 .891 .915	.318 .351 .384 .419 .455	.800 .827 .852 .877 .900	.293 .322 .353 .384 .417	.763 .789 .815 .840 .863
21 22 23 24 25		000	.613 .668 .729 .802	.985 .996 1.000 1.000	.545 .590 .638 .690 .747	.956 .973 .987 .996 1.000	.492 .531 .572 .615	.922 .941 .959 .975 .988	.450 .484 .520 .557 .596	.886 .907 .927 .946 .962
26 27 28 29 30					.816	1.000	.709 .763 8.28	.996 1.000 1.000	.637 .680 .726 .777 .838	.977 .988 .996 1.000

Example: Observed from sample 6/30. The 99% confidence limits for the population are .054 and .443.

**APPENDIX 3B** 

Table 2 (Continued)

x n	3	5	4	0
0	.000	.140	.000	.124
1 2 3 4 5	.000 .003 .010 .020	.194 .239 .280 .318 .354	.000 .003 .009 .017 .028	.172 .212 .249 .283 .315
6 7 8 9 10	.046 .062 .079 .097	.389 .422 .455 .485 .516	.040 .054 .068 .084	.346 .376 .406 .434 .461
11 12 13 14 15	.135 .156 .177 .198	.545 .574 .602 .629 .655	.117 .134 .153 .171 .191	.489 .515 .541 .566 .589
16 17 18 19 20	.245 .269 .294 .319 .345	.681 .706 .731 .755	.211 .231 .252 .273 .295	.614 .638 .661 .(83

	25	
x	35	40
21	.371 .802	.317 .727
22	.398 .823	.339 .748
23	.426 .8:4	.362 .769
24	.455 .865	.386 .789
25	.484 .885	.411 .809
26	.515 .903	.434 .829
27	.545 .921	.459 .847
28	.578 .938	.485 .866
29	.611 .954	.511 .883
30	.646 .968	.539 .900
31	.682 .980	.566 .916
32	.720 .990	.594 .932
33	.761 .997	.624 .946
34	.806 1.000	.654 .960
35	.860 1.000	.685 .972
36 37 38 39 40		.717 .983 .751 .991 .788 .997 .828 1.000 .876 1.000

APPENDIX 3B
Table 2 (Continued)

X	4	5	5	С		n X		5
0	.000	.111	.000	.101		21	.276	.664
						22	.296	.684
j J	.000	.154	.000	.139		23	.316	.7C4
2	.002	.190	.002	.173		24	.336	.724
2 .	.008	.223	.CC7	.203		25	.356	.743
4	.015	.254	.C14	.231				
5	.025	.284	.022	.258		26.	.377	.761
			ì ·	,		27	•399	.779
6	.036	.312	.032	.285		28	.420	.798
7	.047	.339	.04.2	.309		29	.442	.816
8	.060	.366	.054	.334		30	.464	.833
9	.074	.392	.066	.357		·		
10	.088	.418	.079	.381		31	.487	.850
1 1						32	.510	.866
11	.103	.442	.092	.404		33	.535	.882
12	.118	.465	.106	.425		34	.558	.897
13	.134	.490	.120	.447		35	.582	.912
14	.150	.513	.134	.469				
15	.167	.536	.149	.490		36	.608	.926
i i						37	.634	.940
16	.184	. 758	.164	.511		38	,661	.953
17	.202	.580	.180	.532		39	.688	.964
18	.221	.601	.196	.551	i i	40	.716	.975
19	.239	.623	.213	.572	,			
20	.257	.644	.229	.591		41.	.746	.985
						42	.777	•992
	r					43	.810	.998
						77	.846	1,000

46 47 48 49 50	41 42 43 44 45	36 37 38 39 40	31 32 33 34 35	26 27 28 29 30	22 23 24 25
	.746 .985 .777 .992 .810 .998 .846 1.000 .889 1.000	.608 .926 .634 .940 .661 .953 .688 .964 .716 .975	.487 .850 .510 .866 .535 .882 .558 .897 .582 .912	.377 .761 .399 .779 .420 .798 .442 .816 .464 .833	.296 .684 .316 .7C4 .336 .724 .356 .743
.769 .797 .827 .861 .899	.643 .666 .691 .715	.531 .553 .575 .596 .619	.428 .449 .468 .489 .510	.334 .352 .371 .390 .409	.263 .280 .298 .315
.986 .993 .998 1.000	.934 .946 .958 .968	.866 .880 .894 .903	.787 .8C4 .820 .836 .851	.702 .720 .737 .754 .771	.629 .648 .666 .685

50

Example: Observed from sample 35/50. The 99% confidence limits for the population are .510 and .851.

APPENDIX 3B

# Table 2 (Continued)

n = 60

x		
С	.ccc	.085
1 2 3 4 5	.006 .002 .011	.117 .146 .172 .195 .218
6 7 8 9	.026 .035 .045 .055 .065	.241 .263 .283 .304 .324
11 12 13 14 15	.076 .087 .098 .110	.343 .363 .381 .399 .418
16 17 18 19 20	.135 .148 .160 .174 .187	.437 .454 .472 .489 .507
21 22 23 24 25	.201 .215 .228 .243 .257	.524 .54.0 .557 .574 .590
26 27 28 29 30	.272 .286 .3C1 .316 .331	.606 .622 .637 .654 .669

	<del></del>	
X	<u></u> _	'
31	.346	.684
32	.363	.699
33	.378	.714
34	.394	.728
35	.410	.743
36	.426	.757
37	.443	.772
38	.460	.785
39	.476	.799
40	.493	.813
41	.511	.826
42	.528	.840
43	.546	.852
44	.563	.865
45	.582	.877
46	.601	.890
47	.619	.902
48	.637	.913
49	.657	.924
50	.676	.935
51	.696	.945
52	.717	.955
53	.737	.965
54	.759	.974
55	.782	.982
56 57 58 59 60	.805 .828 .854 .883 .915	.989 .994 .998 1.000

APPENDIX 3B

Table 2 (Continued)

	·		n = 80				
x		x			x		
O	.000 .064	26	,198	.47%	56	• 553	.822
	1000	27	.208	.486	57	.566	.833
1 1	.000 .089		.219	500	58	.579	.844
	.001 .111	29	.230	.513	59	.593	.853
2	.004 .131	30	.241	.525	60	.606	.863
4	.009 .149			1,5,	1		1
5	.014 .167		.251	.538	61	.621	.872
	·	32	.262	.55C	62	.634	.882
6	.020 .184		.273	.561	63	.648	.891
7	.026 .201	34	.284	.574	64	.662	.901
8	.033 .217	35	.296	.587	65	.677	.910
9	.040 :233			.]	i		l
10	.048 .249	36	.307	.598	66	.691	.918
		37	.318	.611	67	.705	.927
11	.056264	38	.331	.623	68	.720	.936
12	.064 .280	39	.342	.635	69	.736	.944
13	.073 .295	40	-354	.646	. 70	.751	.952
14	.082 .309			,	. 1	]	ì
15	.090 .323	41	.365	.658	71	.767	.960
1	' '	42	•377	.669	72	.783	.967
16	.099 .338	43	.389	.682	73	.799	.974
17	.109 .352	4.4	.402	.693	74	.816	.98C
18	.118 .366		.413	.704	75	.833	.986
19	.128 .379				1.	l	·
20	.137 .394	46	.426	.716	76	.851	.991
		47	-439	.727	77	.869	.996
21	.147 .407	, ,	.450	.738	78	,889	
22	.156 .421	49	.462	.749	79	.911	1.000
23	.167 .434	50	.475	.759	80	.936	1.000
24	.178 .447						
25	.188 .461	51	.487	.770			•
		52	500	.781			
	•	53	.514	.792			
		54	.526	.802		٠.	
		55	.539	.812	• •		

Example: Observed from sample 50/80. The 99% confidence limits for the population are .475 and .759.

APPENDIX 3B

#### Table 2 (Continued)

n = 100

				<del></del>		<del></del>
x			x		x	
С	.000	.052	36	24C ,493	66	.527 .777
, `	, OCC	• • > > 2	37	.249 .5C3	67	.538 .786
· _	222	272			63	.543 .794
1 2	000	.072	33	.259 .514		
	101	,639	39	.263 .523	€9	
3	.003	.105	40	.276 .534	7C	.569 .811
4 1	. 007	.120		[ ' [		
5	. C11	.135	41	.286 .543	71	.581 .820
			42	.294 .553	72	.591 .528
6,	.016	.149	43	.304 .563	73	.601 .836
7	, C21	.163	44	.312 .573	74	.612 .344
	, C2L	.176	45	.322 .583	75	.622 .352
8 9			1 47	.,,,		
9	.032	.189	14	.331 .592	76	.633 .860
10	. 032	.202	46		77	.644 .868
! !			47	.341 .602		
11 .	.044	.214	48	,350 .611	78	.656 .876
12-	, C51	.227	49	.359 .622	79	.667 .8.4
13	. 058	.240	5C	.369 .631	80	.679 .891
14	, Cć5	.251				
15	.072	.263	51	.378 .641	81	.:90 .899
- '	•		52	.389 .650	82	.702907
16	.079	.275	53	.398 .659	83	.714 .914
17	.086	.286	- 1 5 <u>1</u>	.408 .669	84	.725 .921
18	. 093	,298	55	.417 .678	85	.737 .928
	.101	.310		1	"	
19			56	.427 .688	86	.749 .935
20	.109	.321	57	.437 .696	87	760 ,942
		222			1 1	.773 .949
21	.116	.333	58		89	
22	.124	.344	59	.457 .714		
23	.132	.356	60	.466 .724	90	.798 .962
24	.14C	.367				333 6(0)
25	148	.378	61	.477 .732	91	.811 ,968
	1 1	{	62	.436 .741	92	.824 .974
26	.156	.388	63	.497 .751	1 93	.837 .979
27	.164	399	64	.507 .760		.851 .984
28	172	.409	65	.518 .768		.865 .989
29	.180	419				
30	.189	.431			96	.830 .993
1 20	.109	•474	1		97	.895 .997
	! ,,,,	, , , 1			98	911 999
31	.197	.441				
32	.206	.452	1		99	.978 1.000
33	.214	.462		•	100	.948 1.0CC
34	.223	.473	,			•
1 25	232	/22			•	

35 .232 .432 Example: Observed from sample 50/100. The 99% confidence limits for the population are .369 and .631.

#### APPENDIX 3B

#### Table 3

#### CONFIDENCE IN INFERRING (90% ≤ p) FOR EINOMIAL DISTRIBUTION

The following tables list the confidence value in the body of the table in inferring that 90% < p for a binomial distribution.

These tables are useful for answering such questions as "if (x) units out of a sample of size (n) are observed to have some particular attribute, what confidence can be put in the statement that the true proportion of the population having this attribute is greater than 90%."

If the above question is asked about many different situations, then the table entry lists the percentage of situations in which p is actually greater than 90%.

Thus, the tables list for each sample size, n, and each cuserved number, x, a value for P such that

 $P(90\% \le p) = table entry$ 

Examples are given on each table.

#### PERCENTAGE CONFIDENCE IN INFERRING 90% ≤ n ≤ 100%

x n	1	2	.3	4	5	6	7	8	9	10
0 1 2 3 4 5	<1 10	<1 1 19	<1 <1 3 27	<1 <1 <1 5 34	<1 1 8 4	<pre>&lt;1 &lt;1 &lt;1 &lt;2 2 2 11</pre>	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1 <1	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1
6 7 8 9 10						47	15 52	4 19 57	<1 5 23 61	<1 1 7 26 65

APPENDIX 3B
Table 3 (Continued)

x	11	12	13	14	15	16	17	18	19	20
7 8 9 10	<b>∢</b> 1. 2 9 '30	<1 <1 3 11	<1 <1 <1 3	\ \ \ \ \ \ \ \	マ マ マ マ マ マ	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1
11 12 13 14 15	69	34 72	13 38 75	4 16 42 77	1 6 18 45 79	2 7 21 49	<1 <1 2 8 24	<b>√</b> 1 <b>√</b> 1 <b>√</b> 1 3 10	4444	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <
16 17 18 19 20		,	;			81	52 83	27 55 85	11 29 58 86	4 13 32 61 88

Example: Observed from sample 16/17 Confidence in inferring 90% ≤p ≤ 100% is 52%

APPENDIX 3B
Table 3 (Continued)

x	21	22	23	24	25	26	27	28	29	30
<b>\\$</b> 15	<b>&lt;</b> 1	<b>&lt;</b> 1	<b>&lt;</b> 1	<b>∢</b> l	<1	<1	<b>&lt;</b> 1	<b>&lt;</b> 1	<b>&lt;</b> 1	<1
16 17 18 19 20	1 5 15 35 64	41 2 6 17 38	<b>∢1 ∢1</b> 2 7 19	<1 <1 <1 3 9	<1 <1 <1 <1 3	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1	
21 22 23 24 25	89	66 90	41 68 91	21 44 71 92	10 24 46 73 93	4 11 26 49 75	1 5 13 28 52	<1 2 6 14 31	<b>2 6 16</b>	<1 <1 <1 3 7
26 27 28 29 30		,				94	<b>77</b> 94	54 78 95	33 57 80 95	18 35 57 82 96

Example: Observed from sam; le 21/24 Confidence in inferring 90%≤p ≤ 100% is 21%

APPENDIX 3B
Table 3 (Continued)

Хn	31	32	33	34	35	36	37	38	39	40
≤23 24 25	<b>V</b> 1 3	<1 <1 1	<1 <1 <1	<1 <1 <1	<1 <1 <1	444	<1 <1 <1	444	<1 <1 <1	444
26 27 28 29 30	8 19 38 61 83	4 9 21 40 63	1 4 11 23 42	<1 2 5 12 25	<1 1 2 6 13	<b>₹1</b> <b>₹1</b> <b>₹2</b> 6	<b>VI VI VI VI VI VI VI VI</b>	4444 444 1	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	44444
31 32 33 34 35	96	84 97	65 86 97	45 67 87 97	27 47 69 88 97	15 29 49 71 89	7 16 31 51 73	3 8 17 33 54	1 4 9 19 35	<b>₹1</b> 24 10 21
36 37 38 39 40	-	·				<b>98</b>	90 98	75 90 98	56 76 91 98	37 58 78 92 99

Example: Observed from sample 34/36 Confidence in inferring 90% &p \( \) 100% is 71%

APPENDIX 3B

Table 3 (Continued)

x n	45	50
≤ 35	<1	<1
36 37 38 39 40	1 3 8 16 29	<1 <1 <1 <1 <1 2
41 42 43 44 45	47 67 84 95 99	6 12 23 33 38
46 47 48 49 50		57 75 89 97 >99

x	55	60
<b>≤</b> 44 45	<1 2	<b>√</b> 1 <b>√</b> 1
46 47 48 49 50	4 9 18 31 48	<1 <1 <1 1 3
5 <u>1</u> 52 53 54 55	65 81 92 98 >99	7 14 25 39 56
56 57 58 59 60		73 86 94 99 >99

70	<1 <1 <1 <1	<b>V</b> 1 <b>V</b> 1 2 4 9	16 26 40 56 71	84 93 98 >99 >99
65	1 3 6	11 20 32 48 64	79 90 96 99 <b>&gt;</b> 99	
x	<b>≤</b> 52 53 54 55	56 57 58 59 60	61 62 63 64 65	66 67 68 69 70

**APPENDIX 3B** 

Table 3 (Continued)

x	75	80
<b>≤</b> 61 62 63 64 65	V1 22 4 7 13	44444
66 67 68 69 70	21 33 48 63 77	1 3 5 10 17
71 72 73 74 75	88 95 98 >99 >99	28 41 55 70 82
76 77 78 79 80		91 96 99 >99 >99

80 81 82
86 94 98
41 55

x n	95 95	100
<b>≤</b> 78 79 80	<b>V</b> 1 3	<1 <1 <1
81 82 83 84 85	5 9 15 24 35	<b>V</b> 1 <b>V</b> 1 1 2
86 87 88 89 90	48 62 75 85 92	7 12 20 30 42
91 92 93 94 95	97 99 >99 >99 >99	55 68 79 88 94
96 97 98 99 100		98 99 >99 >99 >99

Example: Observed from sample 76/85 Confidence in inferring 90% ≤p ≤100% is 34%

#### APPENDIX 3B

#### Table 3 (Continued)

#### CONFIDENCE IN INFERRING (95% ≤ p) FOR BINOMIAL DISTRIBUTION

The following tables list the confidence value in the body of the table in inferring that 95% < p for a binomial distribution.

These tables are useful for answering such questions as "if (x) units out of a sample of size (n) are observed to have some particular attribute, what confidence can be put in the statement that the true proportion of the population having this attribute is greater than 95%."

If the above question is asked about many different situations, then the table entry lists the percentage of situations in which p is actually greater than 95%.

Thus, the tables list for each sample size, n, and each observed number, x, a value for P such that

P(95% < p) = table entry

Examples are given on each table.

x	1	2	3	4	5	6	7	8	9	10
0	<1	<1	<1	<1	<1	<1	<1	41	<1	<1
1 2 3 4 5	5	<1 10	<1 1 14	<1 <1 1 19	<1 <1 <1 2 23	<b>₹</b> 1 <b>₹</b> 1 <b>₹</b> 1 <b>₹</b> 1	4444 4444	<1 <1 <1 <1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	V1 V1 V1 V1 V1
6 7 8 9 10			,			26	4 30	1 6 34	<1 7 37	₹11949

APPENDIX 3B

Table 3 (Continued)

x	ü	12	13	14	15	16	17	18	19	20
≤8 9 10	<b>&lt;</b> 1 2 10	<b>V</b> 1 2	<1 <1 <1	A 2.4	<b>√</b> 1 <b>√</b> 1 <b>√</b> 1	444	444	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<li>&lt;1</li> <li>&lt;1</li>	<1 <1 <1
11 12 13 14 15	43	12 46	2 14 49	<b>∢1</b> 3 15 51	1 4 17 54	<1 <1 1 4 19	<1 <1 <1 1 5	<1 <1 <1 <1 <1 1	<1 <1 <1 <1 <1 <1 <1 <1	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <
16 17 18 19 20		·				56	21 58	6 23 60	1 7 25 62	<b>Q1</b> 2 8 26 64

Example: Observed from sample 14/15
Confidence in inferring 95% ≤ p ≤ 100% is 17%

x	21 .	22	- 23	24	25	26	27	28	29	<u>3</u> 0
\$17 18 19 20	<1 2 8 28	<b>41</b>	<1 <1 <1 3	<li>&lt;1</li> <li>&lt;1</li> <li>1</li>	<b>V</b> V V	V V V V	रार्थ	ব্রব্	4444	4444
21 22 23 24 25	66	30 67	11 32 69	3 12 34 71	1 3 13 36 72	<1 <b>&lt;</b> 1 4 14 38	<1 <1 1 4 15	<1 <1 <1 <1 <5	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<b>2222</b>
26 27 28 29 30						74	39 75	16 41 76	5 18 43 77	2 6 19 45 79

APPENDIX 3B

Table 3 (Continued)

x	. 75	ලල
≤66 67 68 69 70	<1 1 3 8 17	\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
71 72 73 74 75	32 52 73 89 98	<1 1 4 10 21
76 77 78 79 80	,	37 57 77 91 98

X n	85	90
≤76 77 78 79 80	<1 3 6 13 25	</p </p </p </p </p </p
81 82 83 84 85	42 62 80 93 99	1 4 8 16 29
86 87 88 89 90		47 66 83 94 99

x	95	100
<b>≤</b> 85	<1	<1
86 87 88 89 90	2 5 10 20 34	44441
91 92 93 94 95	52 71 86 95 99	3 6 13 23 38
96 97 98 99 100		56 74 88 96 99

Example: Observed from sample 90/90 Confidence in inferring 95% ≤ p ≤ 100% is 99%

APPENDIX 3B

Table 3 (Continued)

x	75	80
≤66 67 68 69 70	<1 3 8 17	<1 <1 <1 <1 <1
71 72 73 74 75	32 52 73 89 98	<1 1 4 10 21
76 77 78 79 80		37 57 77 91 98

X. n	85	90
≤76 77 78 79 80	<1 3 6 13 25	44444 4444
81 82 83 34 85	42 62 80 93 99	1 4 8 16 29
86 87 88 89 90		47 66 83 94 99

x	95	100
<b>≤</b> 85	<1	<b>&lt;</b> 1
86 87 88 89 90	2 5 10 20 34	<pre><la><la><la></la></la></la></pre> <pre></pre> <pre></pre> <pre></pre>
91 92 93 94 95	52 71 86 95 99	3 6 13 23 38
96 97 98 99 100		56 74 88 96 99

Example: Observed from sample 90/90 Confidence in inferring 95%  $\leq p \leq 100\%$  is 99%

#### **APPENDIX 3B**

#### Table 3 (Continued)

#### CONFIDENCE IN INFERRING (97% ≤ p) FOR BINOMIAL DISTRIBUTION

The following tables list the confidence value in the body of the table in inferring that 97% p for a binomial distribution.

These tables are useful for answering such questions as "if x units out of a sample of size n are observed to have some particular attribute, what confidence can be put in the statement that the true proportion of the population having this attribute is greater than 97%."

If the above question is asked about many different situations, then the table entry lists the percentage of situations in which p is actually greater the 97%.

Thus, the tables list for each sample size, n, and each observed number, x, a value for P such that

P  $(97\% \leq r)$  = table entry.

Examples are given on each table.

x	1	2	3	4	5	6	7	. 8	9	10
0	<1	<1	<1	<1	<1	<1	<1	<1	<1	<1
1 2 3 4 5	3	<b>&lt;</b> 1 6	<b>V1</b> 9	<1 <1 <1 11	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	₹1 ₹1 ₹1 ₹1	전	Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q	₹1 ₹1 ₹1 ₹1	<1 <1 <1 <1 <1 <1 <1 <1
6 7 8 9 10	·					17	2 19	<1 2 22	41 3 24	<1 <1 <1 3 26

APPENDIX 3B
Table 3 (Continued)

x	11	12	13	1/.	15	16	17	18	19	20
<b>≦</b> 9	<1 4	<1 <1	<1 <1	<1 <1	<1 <1	<b>₹1</b>	<1 <1	<b>&lt;</b> 1 <b>&lt;</b> 1	<1 <1	থ থ
11 12 13 14 15	28	5 31	<1 6 33	<1 <1 6 35	Cl Cl Cl 7 37	<1 <1 <1 <1 8	신 신 신 1	<pre><!-- <! <! <! <! <! <! <! <</th--><th>&lt;1 &lt;1 &lt;1 &lt;1 &lt;1</th><th>VI VI VI VI VI VI VI VI</th></pre>	<1 <1 <1 <1 <1	VI VI VI VI VI VI VI VI
16 17 18 19 20						39	40 40	2 10 42	<1 2 11 44	<1 <1 2 12 46

Example: Observed from sample 19/20 Confidence in inferring 97% ≤ p ≤ 100% is 12%

x	. 21	22	23	24	25	26	27	28	29	30
≤18 19 20	<1 2 13	<1 <1 3	<1 <1 <1	<1 <1 <1	<1 <1 <1	<1 <1 <1	<1 <1 <1	<1 <1 <1	V V V	\$ \$ \$
21 22 23 24 25	47	14 49	3 15 50	<1 3 16 52	<1 <1 4 17 53	<1 <1 <1 4 18	<1 <1 <1 <1 <1 <5	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1 <1 <1 <1 <1	44444
20 27 28 29 30						55	19 56	5 20 57	1 6 22 59	√1 1 6 23 60

APPENDIX 3B

Table 3 (Continued)

x	. 31	32	33	34	35	36	37	38	39	40
<b>≤</b> 27 28 29 30	<1 1 7 24	<1 <1 1 7	<1. <1 <1 2	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1	<1 <1 <1 <1	<1	<1 <1 <1 <1
31 32 33 34 35	61	25 62	8 26 63	2 · 8 27 64	<b>∢1</b> 2 9 28 66	<1 <1 <1 29	<1 <1 <1 2 10	<1 <1 <1 <1 <1 <1 <1 <1 <	<pre></pre> <pre>&lt;</pre>	<1 <1 <1 <1 <1
36 37 38 39 40						67	31 - 68 	11 32 69	3 11 33 70	<1 3 12 34 70

Example: Observed from sample 35/36 Confidence in inferring 97% ≤p ≤100% is 29%

x	45	50
<b>\$</b> 40	<b>&lt;</b> 1	<1
41 42 43 44 45	1 5 15 39 75	<1 <1 <1 <1 <1
46 47 48 49 50		2 6 19 44 78

x	· 55	60
<b>≤</b> 50	<b>&lt;</b> 1	<1
51 52 53 54 55	2 8 23 49 81	\$1 \$1 \$1 \$1 \$1 \$1
56 57 58 59 60		3 11 27 54 84

x	6 <b>5</b>	70
<b>≤</b> 59 60	<1 1	<1 <1
61 62 63 64 65	5 13 31 58 86	<1, <1 <1 <1 <2
66 67 68 69 <b>70</b>		6 16 35 62 88

APPENDIX 38

Table 3 (Continued)

x	75	8C
<b>≤</b> 69	<1	<1
70	3	<1
71	8	<1
72	19	<1
73	39	<1
74	66	1
75	90	3
76 77 78 79 80		9 22 43 70 91

x	85	90
<b>≤</b> 78 79 80	1 4	<1 <1 <1
81 82 83 84 85	11 25 47 73 92	<1 <1 <1 2 5
86 87 88 89 90		13 28 51 76 94

x	95	190
<b>≤</b> 88	<b>&lt;</b> l	<1
89 96	2 7	<b>₹1</b>
91 92 93 94 95	16 32 55 78 94	<1 <1 3 8
96 97 98 99 100		18 35 58 81 95

Example: Observed from sample 93/95 Confidence in inferring 97% ≤ p ≤ 100% is 55%

#### APPENDIX 3B

#### Table 3 (Continued)

#### CONFIDENCE IN INFERRING (99% ≤ p) FOR BINOMIAL DISTRIBUTION

The following tables list the confidence value in the body of the table in inferring that 99% < p for a binomial distribution.

These tables are useful for answering such questions as "if (x) units out of a sample of size (n) are observed to have some particular attribute, what confidence can be put in the statement that the true proportion of the population having this attribute is greater than 99%."

If the above question is asked about many different situations, then the table entry lists the percentage of situations in which p is acutally greater than 99%.

Thus, the tables list for each sample size, n, and each observed number, x, a value for P such that

P (99% < p) = table entry

Examples are given on each table.

X n	1	2	3	4	5	6	7	8	9	10
o	<1	<1	<1	<1	<b>&lt;</b> 1	<1	<1	<1	<1	<b>&lt;</b> 1
1 2 3 4 5	1	<b>&lt;</b> 1 2	<b>&lt;</b> 1 <b>&lt;</b> 1 3	<1 <1 <1 4	<1 <1 <1 <1 5	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1	<1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1 <1 <1	<pre>&lt;1 &lt;1 &lt;1 &lt;1 &lt;1 &lt;1 &lt;1 </pre>
6 7 8 9 10						6	<b>∢1</b> 7	<b>∢1</b> <b>∢1</b> 8	<b>∢</b> 1 <b>∢</b> 1 <b>∢</b> 1 <b>⋄</b> 1	<b>∢</b> 1 <b>∢</b> 1 <b>∢</b> 1 <b>∢</b> 1 10

APPENDIX 3B

Table 3 (Continued)

x	ນ	12	13	14	15	16	17	18	19	20
\$10 11 12 13 14 15	<1 10	<1 <1 11	<1 <1 <1 12	<1 <1 <1 13	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <		000000	AAAAA	\$\$\$\$\$\$
16 17 18 19 20						15	1 16	1 1 17	<1 <1 <2 17	<1 <1 <1 2 18

Example: Observed from sample 16/16
Confidence in inferring 99% ≤p ≤ 100% is 15%

x n	21	22	23	24 .	25	26	27	28	29	30
<b>≤</b> 19 20	<b>≺1</b> 2	<1 <1	<1' <1	<1 <1	<1 <1	<1 <1	AA	AA	<b>₹1</b>	<b>₹</b>
21 22 23 24 25	19	20	<1 2 21	<1 <1 2 21	<1 <1 <1 3 22	<1 <1 <1 <1 <1 <3	<1 <1 <1 <1 <1 <1	41 41 41 41	₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹	<1 <1 <1 <1 <1 <1
26 27 28 29 30						23	3 24	<b>∢</b> 1 3 24	<b>&lt;</b> 1 <b>€</b> 1 <b>3</b> 25	<b>₹1</b> <b>₹1</b> <b>₹1</b> <b>4</b> <b>26</b>

APPENDIX 3B

Table 3 (Continued)

X	31	32	33	34	35	36	37	38,	39	40
<b>≤</b> 29 30	<b>&lt;1</b> 4	<1 <1	<1 <1	<1 <1	<1 <1	<1 <1	<1 <1	<1 <1	<1 <1	<1 <1
31 32 33 34 35	27	4 28	<1 4 28	<1 <1 5 29	<1 <1 <1 5 30	<1 <1 <1 <1 5	<1 <1 <1 <1 <1	<1 <1 <1 <1 <1	<1 <1 <1 <1 <1 <1	<1 <1 <1 <1 <1
36 37 38 39 40						30	5 31	<1 6 32	<b>4</b> 1 6 32	<1 <1 <1 6 33

Example: Observed from sample 27/28 Confidence in inferring 99%  $\leq p \leq 100\%$  is 3%

X n	45	50
<b>≤</b> 42 43 44 45	<1 7 36	<1 <1 <1 <1
46 47 48 49 50		<1 <1 1 9 39

x n	65	70
<b>\$</b> 62 63	<1 3 14	<1 <1 <1
64 65	48	<1
66 67 68		<1 <1 3
69 70		16 51

n X	55	60
<b>≤</b> 52 53 54 55	<b>&lt;</b> 1 2 11 42	41 41 41
56 57 58 59 60		<b>&lt;</b> 1 <b>&lt;</b> 1 2 12 45

X n	75	80
<b>5</b> 72 73 74 75	<1 4 17 53	<b>222</b>
76 77 78 79 80		<1 <1 5 19 55

**APPENDIX 3B** 

Table 3 (Continued)

n	85	90
<b>≤</b> 81 82 83 84 85	V1 1 5 21 57	4444
86 87 88 89 90	·	<b>₹1</b> 1 6 23 60

n n	95	100
<b>≤</b> 91. 92 93 94 95	<1 2 7 25 62	2225
96 97 98 99 100		<b>∢1</b> 2 8 26 63

Example: Observed from sample 74/75 Confidence in inferring 99% ≤ p ≤ 100% is 17%

x<sup>2</sup> 0 x<sup>2</sup>

APPENDIX 3C

•												
P = 0.99	26.0	0.95	06.0	0.80	0.70	0.50	c.3c	0.20	0.10	0.05	0.02	0.01
C.CCC157	C.CCC628	0.00393	0.0158	0.0642	C.148	0.455	1.074	1.64%	2,706	3.841	217°5	6.635
0.0001	C.0404	c.103	0.211	0.446	0.713	1.386	2.408	3.219	4.605	5.991	7.824	9.210
c.115	0.185	0.352	0.584	1.005	1.424	2.366	3.665	7.642	6.251	7.815	9.837	11.341
c.297	0.429	c.711	1.064	1.649	2,195	3.357	4.878	5.989	7.779	887.6	11.668	13.277
C.554	0.752	1.145	1.610	2.343	3.00	4.351	790.9	7.289	9.236	11.070	13,388	15.086
0.872	1.134	1.635	7.507	3.070	3.828	5.348	7,231	8.558	10.645	12,592	15.033	16.812
1.239	1.564	2,167	2,833	3.822	4.671	6,346	8,383	9.83	12,017	14.067	16,622	18.475
973	2.032	2,733	3.490	760.7	7,77,7	7.544	9.524	11.030	13,302	15.507	201-81	20.0X
2,553	3,059	3,940	4.165	6,179	7.267	9,342	11.781	13.442	15,987	18,307	21,161	23,259
) (			```			11/2/						
3.053	3.609	4.575	5,578	6.986	8,148	10.341	12.899	14.631	17,275	19,675	22.618	24.725
3.571	4.178		325			11.340	14.011	15.812	18.549	21.026	54.054	26.217
1.107	4.765		°042		_	12,340	15,119	16.985	19,812	22.362	25.472	27.688
099*	5,368		.790			13.339	16,222	18.151	21.064	23.685	26.873	29,141
5.23	5.985		.547		_	14.339	17,322	19.311	22,307	54.996	28.259	30,578
5.812	6.614	•	.312	11.152		15.338	18.418	20°465	23.542	26.296	29.633	35,000
827.9	7,255		.085			16.338	19.511	21.615	27.76	27.587	30.995	33.409
7.015	7.906		.865	*	14.440	17,338	20.601	22.760	25.989	28.869	32°376	34.805
7.633	8.567		.651		15,352	18.338	21.689	23.900	27.204	30.144	33.687	36,191
3.260	9.237	0.851	773	14.578	16.266	19.337	22.775	25.038	28.412	31.410	35.C20	37.566
8 207			270		17,182	20,337	23.858	26.171	29,615	32,671	36, 343	38,932
9.572	10,600	12.338	77	16.314	18.101	21.337	24.939	27.301	30,813	33.924	37.659	40.289
*****	1.293		878		19,021	22,337	26,018	28.429	32,007	35.172	38.968	41,633
	.992	13.848	5.65'	233	19.943	23,337	27 096	29.553	33,196	36,415	40,270	77°,980
1.524	12.697		16,473	18.940	20.867	24.337	28.172	30.675	34.382	37.652	41°266	44.314
			,292		21.792	25.336	29.276	31.795	35,563	38.885	75.856	. 45,642
			8,114	,703	22.719	26.336	30,319	32,912	36.741		77.77	76,963
13.565	14.847	16,928	8.939		23.647	27.336	31,391	34.027	37.916	41 337	72°718	48,278
14.256		17.708		475	24,577	28,336	32,461	35.139	39°087	42,557	66,693	49.588
14,953	.306		665°	23.364	25,508	29,336	33,530	36.250	70.256	13 773	17 062	F.C. 892

# APPENDIX 3D Table 1 CONFIDENCE LIMITS FOR THE EXPECTATION OF A POISSON VARIABLE

1-2a	0.99	3	C.99		0.9	8	0.95		C.9	C	1-2e
a	0.00	1	0.005		C.0	1	0.02	.5	. 0.0	5	æ
С	Lower	Upper	Lower	Upper	Lower	Upper	Lower	Upper	Lower	Upper	С
0 1 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 11 2 3 4 5 6 7 8 9 0 3 5 0 4 5 0 2 2 2 2 2 2 2 2 2 2 2 3 3 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0	C.000CO .CC1CO .CC1CO .C454 .191 .429 C.739 1.11 1.52 1.97 2.45 2.96 3.49 4.61 5.20 5.79 5.41 7.63 7.66 8.31 8.96 9.62 10.96 11.65 12.34 13.73 14.44 15.15 15.87 19.52 23.26 27.08 30.96	6.91 9.23 11.23 13.06 14.79 16.45 18.06 19.63 21.16 22.66 24.13 25.03 28.45 29.85 31.24 32.62 33.99 35.35 36.70 43.83 45.94 47.23 48.80 57.42 69.83 75.94	0.00000 .CC5C1 .103 .338 .672 1.08 1.54 2.04 2.57 3.13 3.72 4.32 4.94 5.58 6.23 6.89 7.57 8.25 8.94 9.64 10.35 11.07 11.79 12.52 13.25 14.00 17.77 21.64 25.59 29.60 33.66	5.30 7.43 9.27 10.98 12.59 14.15 15.66 17.13 18.58 24.14 25.50 26.84 28.16 29.48 30.79 33.38 34.67 35.95 37.22 38.48 47.21 53.32 59.36 41.27	0.000C .0101 .149 .436 .823 1.28 1.79 2.33 2.91 3.51 4.17 5.43 6.10 6.78 8.18 8.89 9.62 10.35 11.08 11.82 12.57 13.33 14.09 14.85 16.40 17.17 17.96 16.74 22.72 26.77 35.03 35.03	4.61 6.64 8.41 10.05 11.60 13.11 14.57 16.00 17.40 18.78 20.14 21.49 22.82 24.14 25.45 26.74 28.03 29.31 30.58 31.85 33.10 34.36 35.60 36.84 38.93 41.76 42.93 44.19 45.40 51.41 57.35 69.07	0.0000 6.253 .2,2 .619 1.62 2.81 3.45 4.12 4.80 5.49 6.92 7.65 9.15 9.15 9.15 9.16 12.20 13.79 14.58 16.98 17.79 18.61 19.42 24.38 28.53 32.82 37.11	3.69 5.57 7.22 8.77 10.24 11.67 13.66 14.42 15.76 18.39 19.68 20.96 21.23 23.49 24.74 25.98 27.22 28.45 27.32 28.45 27.32 28.45 27.32 28.45 27.32 28.45 29.69 31.31 31.31 31.31 31.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 48.68 54.47 41.65 42.83 43.49 44.65 45.92	0.0000 .0513 .355 .818 1.37 1.97 2.61 3.29 3.98 4.70 5.43 6.92 6.92 10.83 11.63 12.44 13.25 14.89 15.72 16.55 17.38 18.26 19.90 20.75 21.59	3.00 4.74 6.30 7.75 9.15 10.84 15.96 11.31 12.44 15.96 11.31 12.44 15.96 11.31 12.44 15.69 12.44 15.69 12.44 15.69 12.44 15.69 12.44 15.69 16.69 16.69 17.49	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 40 45

If c is the observed frequency or count and m , m are the lower and upper confidence limits for its expectation, m, then

 $\Pr' m_A \le m \le m_B \le 1-2\alpha$ 

# APPENDIX 3D Table 1

## CONFIDENCE LIMITS FOR THE EXPECTATION OF A POISSON VARIABLE

1-2a	0.99	8	c.99		0.9	8	0.95	5	0.9	00	1-2 <b>a</b>
a	0,00	1	0.005		0.0	1	0.02	25	0.0	05	a
С	Lower	Upper	Lower	Upper	Lower	Upper	Lower	Upper	Lower	Upper	Ç
01234567890112314561713902122324562789035450	C.00000 .00100 .0454 .191 .429 C.739 1.11 1.52 1.97 2.45 2.96 3.49 4.61 5.20 5.79 5.41 7.66 8.31 8.96 9.62 10.96 11.65 12.34 13.73 14.44 15.15 15.87 19.52 23.26 27.08 30.96	6.91 9.23 11.23 13.06 14.79 16.45 18.63 21.66 22.62 24.13 27.63 28.85 31.26 29.35 30.70 42.33 44.94 47.23 44.94 47.23 44.94 47.23 48.86 57.42 69.83 75.94	0.00000 .cc5c1 .103 .338 .672 1.08 1.54 2.57 3.13 3.72 4.94 5.58 6.23 6.89 7.57 8.25 8.94 9.64 10.35 11.07 11.79 12.52 13.25 14.00 17.77 21.64 25.59 29.60 33.66	5.30 7.43 9.27 10.98 12.59 14.15 15.66 17.15 18.58 20.00 21.40 22.78 24.14 25.50 26.84 29.48 30.79 33.38 34.67 35.95 37.22 38.48 47.21 53.32 59.36 65.34 71.27	0.000c .0101 .149 .436 .823 1.28 1.79 2.33 2.91 3.51 4.77 5.43 6.10 6.78 7.48 8.89 9.62 10.35 11.08 11.82 12.57 13.33 14.09 14.85 16.40 17.17 17.96 18.74 22.72 26.77 30.83 35.73	4.61 6.64 8.41 10.05 11.60 13.11 14.57 16.00 17.40 18.78 20.14 21.49 22.82 24.45 26.74 29.31 30.58 31.85 33.10 36.84 39.31 41.76 42.93 44.19 45.40 51.41 57.35 69.07	0.0000 0.253 .242 .619 1.62 2.81 3.45 4.80 5.49 10.65 9.15 9.15 9.15 11.44 12.20 13.79 14.58 16.98 17.79 18.62 24.38 20.24 24.38 20.24 24.38 25.49 18.63 26.38 17.79 18.63 27.65 28.15 29.15 20.24 24.38 26.38 27.65 27.6	3.69 5.57 7.22 8.77 10.24 11.67 13.06 14.42 15.76 18.39 19.68 18.39 19.68 27.22 28.45 29.67 30.89 31.35.71 36.90 37.41.65 42.83 48.68 40.47 41.65 42.83 48.68 40.47 41.65 42.83 48.68	0.0000 .0513 .355 .818 1.37 1.97 2.61 3.29 3.40 5.43 10.83 11.63 11.63 11.63 11.63 11.63 11.63 11.65 14.89 15.72 16.55 17.38 18.20 19.90 20.75 21.59	3.00 4.74 6.30 7.75 9.15 10.51 11.84 15.71 16.96 18.21 19.44 20.67 21.30 24.30 25.50 27.38 29.24 30.24 31.42 32.59 34.92 33.75 34.92 37.23 38.39 46.40 57.29 63.29	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 40 45 45 46 46 46 46 46 46 46 46 46 46 46 46 46

If c is the observed frequency or count and m , m are the lower and upper confidence limits for its expectation, m, then

 $\Pr (m_A \le m \le m_B) \le 1-2\alpha$ 

APPENDIX 3E

Table 1A

F DISTRIBUTION: UPPER 10 FERCENT POINTS

V₁	1	_ ^ _		· · ·				_	
V2	Τ.	2	3	4	5	6	7	8	9
1	39.864	49.500	53.593	55.833	57.241	58.204	58.906	59.439	59.858
2	8.5263	9.0000		9.2434	9.2926				9.3805
3	5.5383	5.4624	5.3908	5.3427		5.2847		5.2517	5.2400
4	4.5448	4.3246	4.1908	4.1073	4.0506	4.0098			3.9357
5.	4.0604	3.7797	3.6195	3.5202	3.4530	3.4045			3.3163
6	3.7760	3.4633	3.2888	3.1808	3.1075	3.0546		2.9830	2.9577
7	3.5894	3.2574	3.0741	2.9605	2.0833	2.8274		2.7516	2.7247
8	3.4579	3.1131	2.9238	2.8064	2.7265	2.6683		2.5893	2.5612
9	3.3603	3.0065	2.8129	2.6927	2.6106	2.5509		2.4694	2.4403
10	3.2850	2.9245	2.7277	2.6053	2.5216	2.4606		2.3772	2.3473
11	3.2252	2.8595	2.6602	2.5362	2,4512	2.3891	2.3416	2.3040	2.2735
12	3.1765	2.8068	2.6055	2.4801	2.3940	2.3310		2.2446	2.2135
13	3.1362	2.7632	2.5603	2.4337	2.3467	2.2830		2.1953	2.1633
14	3.1022	2.7265	2.5222	2.3947	2.3069	2.2426	2.1931	2.1539	2.1220
15	3.0732	2.6952	2.4898	2.3614	2.2730		2.1582	2.1185	2.0862
16	3.0431	2.6682	2.4618	2.3327	2.2438	2.1783	2.1250	2.0860	2.0553
17	3.0262	2.6446	2.4374	2.3077	2.2183	2.1524	2.1017	2.0613	2.0284
13	3.0070	2.6239	2.4160	2.2858	2.1958			2.0379	2.0047
19	2.9899	2.6056	2.397C	2.2663	2.1760				1.9836
20	2.9747	2.5893	2.3801	2.2489	2.1582	2.0913	2.0397	1.9985	1.9649
21	2.9609	2.5746	2.3649	2.2333	2.1423	2.0751	2.0232	1.9819	1.9480
22 <sup>-</sup> 23	2.9486	2.5613	2.3512	2,2193	2.1279	2.0605	2.0084	1.9668	1.9327
24	2.9374	2.5493	2.3387	2.2065	2.1149	2.0472	1.9949	1.9531	1.9189
25	2.9271	2.5383	2.3274	2.1949	2.1030	2.0351	1.9826	1.9407	1.9063
26	2.9091	2.5283	2.3170	2.1843	2.0922	2.0241	1.9714	1.9292	1.8947
27	2.9012	2.5106	2.3075 2.2907	2.1745	2.0822	2.0139	1.9610	1.)188	1.8841
28	2.8939	2.5028	2.2906	2.1655	2.0730	2.0045	1.9515	1.90/1	1.8743
29	2.8871	2.4955	2.2831	2.1571	2.06.15	1.9959	1.9427		1.8652
		1		2.1494	2.0566	1.9878	1.9345	1.8918	1.8568
30	2.8807	2.4887	2.2761	2.1422	2.0492	1.9803	1.9269		1.8490
40 -60	2.8354	2.4404	2.2261	2.0909	1.9968	1.9269			1.7929
120	2.7914	2.3932	2.1774	2.0410	1.9457	1.8747	1.8194	1.7748	1.7380
	2.7478 2.7055	2.3473	2.1300	1.9923	1.8959	1.8238	1.7675	1.7220	1.6843
80	2,1000	2.3026	2.0838	1.9449	1.8473	1.7741	1.7167	1.6702	1.6315

This table gives the values of F for which  $I_{\overline{F}}(v_i, v_2) = 0.10$ 

One-sided 90 porcent test.

Two-sided 60 percent test.

APPENDIX 3E

Table 1B

F DISTRIBUTION: UPPER 10 PERCENT POINTS

							_			
V	10	12	15	20	24	30	40	60	120	8
V2		-								
•	10.305	(0.005	43.000	(3 710	(5, 600	62 265	(0.500	(0.70)	(2.06)	62 202
	60.195	60.705	61.220	61.740	62.002	62.265	62.529	62.794	63.061	63.328
2	9.3916	9.4081	9.4247	9.4413	9.4496	9.4579	9.4663	9.4746	9.4829	9.4913
3	5.2304	5.2156	5.2003	5.1845	5.1764	5,1681	5.1597	5.1512	5.1425	5.1337
4	3.9199	3.8955	3.8689	3.8443	3.8310	3.8174	3,8036	3.7896	3.7753	3.7607
5	3.2974	3.2682	3.2380	3.2067	3.1905	3.1741	3.1573	3.1402	3.1228	3.1050
6	2.9369	2.9047	2.8712	2.8363	2.8183	2.8000	2.7812	2.7620	2.7423	2.7222
7	2.7025	2.6681	2.6322	2.5947	2.5753	2.5555	2.5351	2.5142	2.4928	2.4708
8	2.5380	2.5020	2.4642	2.4246	2.4041	2.3830	2.3614	2.3391	2.3162	2.2926
9	2.4163	2.3789	2.3396	2.2983	2.2768	2.2547	2.2320	2.2085	2.1843	2.1592
10	2.3226	2.2841	2.2435	2.2007	2.1784	2.1554	2.1317	2.1072	2.0818	2.0554
11	2.2482	2.2087	2.1671	2.1230	2.1000	2.0762	2.0516	2.0261	1.9997	1.9721
12	2.1878	2.1474	2.1049	2.0597	2.0360	2.0115	1.9861	1.9597	1.9323	1.9036
13	2.1376	2.0966	2.0532	2.0070	1.9827	1.9576	1.9315	1.9043	1.8759	1.8462
14	2.0954	2.0537	2.0095	1.9625	1.9377	1.9119	1.8852	1.8572	1.8280	1.7973
15	2.0593	2.0171	1.9722	1.9243	1.8990	1.8728	1.8454	1.8168	1.7867	1.7551
16	2.0281	1.9854	1.9399	1.8913	1.8656	1.8388	1.8108	1.7816	1.7507	1.7182
17	2.0009	1.9577	1.9117	1.8624	1.8362	1.8090	1.7805	1.7506	1.7191	1.6856
18	1.9770	1.9333	1.2868	1.8368	1.8103	1.7827	1.7537	1.7232	1.6910	1.6567
19	1.9557	1.9117	1.8647	1.8142	1.7873	1.7592	1.7298	1.6988	1.6659	1.6308
20	1.9367	1.8924	1.8449	1.7938	1.7667	1.7382	1.7083	1.6768	1.6433	1.6074
21	1.9197	1.8750	1.8272	1.7756	1.7481	1.7193	1.6890	1.6569	1.6228	1.5862
22	1.9043	1.8593	1.8111	1.7590	1.7312	1.7021	1.6714	1.6389	1.6042	1.5668
23	1.8903	1.8450	1.7964	1.7439	1.7159	1.6864	1.6554	1.6224	1.5871	1.5490
24	1.8775	1.8319	1.7831	1.7302	1.7019	1.6721	1.6407	1.6073	1.5715	1.5327
25	1.8658	1.8200	1.7708	1.7175	1.6890	1.6589	1.6272	1.5934	1.5570	1.5176
26	1.8550	1.8090	1.7596	1.7059	1.6771	1.6468	1.6147	1.5805	1.5437	1.5036
27	1.8451	1.7989	1.7492	1.6951	1.6662	1.6356	1.6032	1.5686	1.5313	1.4906
28	1.8359	1.7895	1.7395	1.6852	1.6560	1.6252	1.5925	1.5575	1.5198	1.4784
29	1.8274	1.7808	1.7306	1.6759	1.6465	1.6155	1.5825	1.5472	1.5090	1.4670
30	1.8195	1.7727	1.7223	1.6673	1.6377	1.6065	1.5732	1.5376	1.4989	1.4564
40	1.7627	1.7146	1.6624	1.6052	1.5741	1.5411	1.5056	1.4672	1.4248	1.3769
60	1.7070	1.6574	1.6034	1.5435	1.5107	1.4755	1.4373	1.3952	1.3476	1.2915
120	1.6524	1.6012	1.5450	1.4821	1.4472	1.4094	1.3676	1.3203	1.2646	1.1926
<b>©</b>	1.5987	1.5458	1.4871	1.4206	1.3832	1.3419	1.2951	1.2400	1.1686	1.0000
	1									

$$F = \frac{sf}{s\frac{s}{s}} = \frac{v_2S_1}{v_1S_2}$$

Ore-sided 90 percent test.

Two-sided 80 percent test.

**APPENDIX 3E** 

Table 2A

# F DISTRIBUT!ON: UPPER 5 PERCENT POINTS

This table gives the values of F for which  $I_F(V_1, V_2)=0.05$ .

One-sided 95 percent test.

Two-sided 90 percent test.

APPENDIX SE

Table 2B

F DISTRIBUTION: UPPER 5 PERCENT POINTS

-					67	30	40	60	120	80
VI	10	12	15	20	24	30	40	00	120	ω
<u>vz</u>	212 00	012.03	015.05	2/0 07	249.C5	250.09	251.14	252.2C	253,25	254.32
1	241.88	243.91	245.95	248.01		19.462	19.471	19.479	19.487	19.496
2	19.396	19,413	19.429	19.446	19'.454	8.6166	8.5944	8.5720	8.5494	3.5265
3	8.7855	8,7446	8.7029	8.6602	8.6385		5.7170	5.6878	5.6581	5.6281
4	5.9644	5.9117	5.8578	5.8025	5.7744	5.7459			4.3984	4.3650
5	4.7351	4.6777	4.6188	4.5581	4.52?2	4.4957	4.4638	4.4314		3.6688
6	4. 760C	3,9999	3.9381	3.8742	3.8415	3.8082	3.7743	3.7398	3.7047	
<b>7</b> ·	3 .6365	3.5747	3.5108	3 . 4445	3.4105	3.3758	3.3404	3.3043	3.2674	3.2298
Ø,	3.3472	3 . 2840	3.2184	3.1503	3.1152	3.0794	3.0428	3.0053	2,9669	2.9276
9	3.1373	3 0729	3.0061	2.9365	2.9CC5	2.8637	2.3259	2.7872	2.7473	2.7067
10	2.9782	2.9130	2.845C	2.7740	2.7372	2.6996	2,6609	2.6211	2.5801	2.5379
11	2-8536	2.7876	2.7186	2.6464	2.6090	2.5705	2.5309	2.4901	2.4480	2.4045
12	2.7534	2.6866	2.6169	2.5436	2.5055	2.4663	2.4259	2.3842	2.3410	2.2962
13	2.6710	2,6037	2.5331	2.4589	2.4202	2.3803	2.3392	2.2966	2.2524	2.2064
14	2.6021	2.5342	2.463C	2.3879	2.3487	2.3082	2.26(4	2.2230	2.1778	2,1307
·· 15	2.5437	2.4753	2.4035	2.3275	2.2878	2.2468	2.2043	2.1601	2.1141	2.0658
16	2.4935	2.4247	2.3522	2.2756	2.2354	2.1938	2.1507	2.1058	2.0589	2,0096
17	2,4499	2.3807	2.3077	2.2304	2.1898	2.1477	2.1040	2.0584	2.0107	1.9604
18	2.4117	2.3421	2.2686	2.1906	2.1497	2.1071	2.0629	2.C166	1.9681	1.9168
19	2.3779	2.308C	2.2341	2.1555	2.1141	2.0712	2.0264	1.9796	1.9302	1.8780
20	2.3479	2.2776	2.2033	2.1242	2.0825	2.0391	1.9938	1.9464	1.8963	1.8432
21	2.3210	2.2504	2.1757	2.0960	2.0540	2.0102	1.9645	1.9165	1.8657	1.8117
22	2.2967	2.2258	2.1508	2.0707	2.0283	1.9842	1.9360	1.8895	1.8380	1.7831
23	2.2747	2.2036	2.1282	2,0476	2.0050	1.9605	1.9139	1.8649	1.8128	1.7570
24	2.2547	2.1834	2.1077	2.0267	1.9838	1.9390	1.8920	1.8424	1.7897	1.7331
25	2.2365	2.1649	2.0889	2.0075	1.9643	1.9192	1.8718	1.8217	1.7684	1.7110
26	2.2197	2.1479	2.0716	1.9898	1.9464	1.9010	1.8533	1.8027	1.7488	1.6906
27	2.2043	2.1323	2.C558	1.9736	1.9299	1.8842	1.8361	1.7851	1.7307	1.6717
28	2.1900	2.1179	2.0411	1.9586	1.9147	1.8687	1:8203	1.7689	1.7138	1.6541
29	2.1768	2.1045	2.0275	1.9446	1.9005	1.8543	1.8055	1.7537	1.6981	1.6377
30	2.1646	2.0921	2.0148	1.9317	1.8874	1.8409	1.7918	1.7396	1.6835	1.6223
40	2.0772	2.0035	1.9245	1.8389	1.7929	1.7444	1.6928	1.6373	1.5766	1.5089
60° -	1.9926	1.9174	1.8364	1.7480	1.7001	1.6491	1.5943	1.5343	1.4673	1.3893
L20	1.9105	1.8337	1.7505	1.6587	1.6084	1.5543	1.4952	1./290	1.3519	1.2539
Ø	1.8307	1.7522	1.6664	1.5705	1.5173	1.4591	1.3940	1.3180	1.2214	1.0000
_			<u> </u>				L			لببسسيا

$$F = \frac{s_1^2}{s_2^2} = \frac{v_2}{v_1} \frac{S_1}{S_2}$$

One-sided 95 percent test.

Two-sided 90 percent test.

APPENDIX 3E

Table 3A

F DISTRIBUTION: UPPER 2.5 PERCENT POINTS

	· · · · · ·						·		
7	1.	2	.3	4	5	6	7	8	9
V <sub>2</sub>									
1	647.79	799.50	864.16	899.58	921.85	937.11	948.22	956.66	963.28
2	38.506	39.000	39.165	39.248	39.298	39.331	39.355	39.373	39.387
3	17.443	16.044	15.439	15.101	14.885	14.735	14.624	14.540	14.473
4	12.2'9	10.649	9.9792	9.6045	9.3645	9.1973	9.0741	8.9796	8.9047
5	7	8.4336	7.7636	7.3879	7.1464	6.9777	6.8531	6.7572	6.6810
6	0.0131	7.2598	6.5988	6.2272	5.9876	5.8197	5.6955	5.5996	5. <del>5</del> 234
7	8.0727	6.5415	5.8898	5.5226	5.2852	5.1186	4.9949	4.8994	4 3232
8	7.5709	6.0595	5.4160	5.0526	4.8173	4.6517	4.5286	4.4352	4.3572
9	7.2093	5.7147	5.0781	4.7181	4.4844	4.3197	4.1971	4.1020	4.0260
10	6.9367	5.4564	4.8256	4.4683	4.2361	4.0721	3.9498	3.8549	3-7790
11	6.7241	5.2559	4.6300	4.2751	4.0440	3.8807	3.7586	3.6638	3.5879
12	6.5538	5.0959	4.4742	4.1212	3.8911	3.7283	3.6065	3.5118	3.4358
13	6.4143	4.9653	4.3472	3.9959	3.7667	3.6043	3.4827	3.3880	3.3120
14	6.2979	4.8567	4.2417	3.8919	3.6634	3.5014	3 <b>.37</b> 99	3.2853	3.2093
15	6.1995	4.7650	4.1528	3.8043	3.5764	3.4147	3.2934	3.1987	3.1227
16	6.1151	4.6867	4.0768	3.7294	3.5021	3.3406	3.2194	3.1248	3.0488
17	6.0420	4.6189	4.0112	3.6648	3.4379	3.2767	3.1556	3.0610	2.9849
18-	5.9781	4-5597	3.9539	3.6083	3.3820	3.2209	3.099 <del>9</del>	3.0053	2.9291
19	5.9216	4.5075	3.9034	3.5587	3.3327	3.1718	3.0509	2.9563	2.8800
20	5.8715	4.4613	3.8587	3.5147	3.2891	3.1283	3,0074.	2.9128	2.8365
21	5.8266	4.4199	3.8188	3.4754	3.2501	3.0895	2.9686	2.8740	2.7977
22	5.7863	4.3828	3.7829	3.4401	3.2151	3.0546	2.9338	2.8392	2.7628
23	5.7498	4.3492	3.7505	3.4083	3.1835	3.0232	2.9024	2.8077	2.7313
24	5.7167	4.3187	3.7211	3.3794	3.1548	2.9946	2.8738	2.7791	2.7027
25	5.6864	4.2909	3.6943	3.353Q	3.1287	2.9685	2.8478	2.7531	2.6766
26	5.6586	4.2655	3.6697	3.3289	3.1048	2.9447	2.8240	2.7293	2.6528
27	5.6331	4.2421	3.6472	3.3067	3.0828	2.9228	2.8021	2.7074	2.6309
28	5.6096	4.2205	3.6264	3.2863	3.0625	2.9027	2.7820	2.6872	2.6104
29	5.5878	4.2006	3.6072	3.2674	3.0438	2.8840	2.7633	2.6686	2.5919
30	5.5675	4.1821	3.5894	3.2499	3.0265	2.8667	2.7460	2.6513	2.5746
40	5.4239	4.0510	3.4633	3.1261	2.9037	2.7444	2.6238	2.5289	2,453 3
60	5.2857	3.9253	3.3425	3.0077	2.7663	2.6274	2.5068	2.4117	2.33
120	5.1524	3.8046	3.2270	2.8943	2.6740	2.5154	2.3948	2.2994	2.22.7
Φ .	5.0239	3.6889	3.1161	2.7858	2.5665	2.4082	2.2875	2.1918	2.1136

This table gives the values of F for which  $I_{\overline{Y}}(v_1,v_2) = 0.025$ .

One-sided 97.5 percent test. Two-sided 95.0 percent test.

APPENDIX 3E

Table 3B

F DISTRIBUTION: UPPER 2.5 PERCENT POINTS

V1										
V2	10	12	15	20	24	30	40	60	120	8
					207 25	7007	3005 (	7000 0	2027.0	1018.3
	968.63	976.71	984.87	993,10	997,25	1001.4	1005.6	1009.8	1014.0	
	39.398	39.415	39.431	39.448	39.456	39.465	39.473	39.481	39.490	39.498
	14,419	14.337	14.253	14.167	14.124	14.081	14.037	13.992	13.947	13.902
•	8.8439	8.7512	8.6565	8.5599	8.5109	8,4613	٤.4111	8.3604	E.3C92	8.2573
5	6.6192	6.5246	6.4277	6.3285	6.2780	6.2269	6.1751	6.1225	6.0693	6.0153
6	5.4613	5.3662	5.2687	5.1684	5.1172	5.0652	5.0125	4.9589	4.9045	4.8491
7	4.7611	4.6658	4.5678	4.4667	4.4150	4.3624	4.3089	4.2544	4.1989	4.1423
8	4.2951	4.1997	4.1012	3.9995	3.9472	3.8940	3.8398	3.7844	3.7279	3.6702
9	3.9639	3.8682	3.7694	3.6669	3.6142	3.5604	3.5055	3.4493	3.3918	3.3329
10	3.7168	3.6209	3.5217	3.4186	3.3654	3.3110	3.2554	3.1984	3.1399	3.0798
11	3.5257	3.4296	3.3299	3.2261	3.1725	3.1176	3.0613	3.0035	2.9441	2.8828
12	3.3736	3.2773	3.1772	3.0728	3.0187	2.9633	2.9063	2.8478	2.7874	2.7249
13	3.2497	3.1532	3.0527	2.9477	2.8932	2.8373	2.7797	2.7204	2.6590	2.5955
14	3.1/69	3.0501	2.9493	2.8437	2.7888	2.7324	2.6742	2.6142	2.5519	2.4872
15	3.0662	2.9633	2.8621	2,7559	2.7006	2.6437	2.5850	2.5242	2.4611	2.3953
16	2.9862	2.8890	2.7875	2.6808	2.6252	2.5678	2.5085	2.4471	2.3831	2.3163
17	2.9222	2.8249	2.7230	2.6158	2.5598	2.5021	2.4422	2.3801	2.3153	2.2474
18	2.8664	2.7689	2.6667	2.5590	2.5027	2.4445	2.3842	2.3214	2.2558	2.1869
19	2.8173	2.7196	2,6171	2.5089	2.4523	2,3937	2.3329	2.2695	2.2032	2.1333
20	2.7737	2.6758	2.5731	2.4645	2.4076	2.3486	2.2873	2.2234	2.1562	2.0853
21	2.7348	2.6368	2.5338	2.4247	2.3675	2.3082	2.2465	2.1819	2.1141	2.0422
22	2.6998	2.6017	2.4984	2.3890	2.3315	2.2718	2.2097	2.1746	2.0760	2.0032
23	2.6682	2.5699	2.4665	2.3567	2.2989	2.2389	2.1763	2.1107	2.0415	1.9677
24	2.6396	2.5412	2.4374	2.3273	2.2693	2.2090	2.1460	2.0799	2.0099	1.9353
25	2.6135	2.5149	2.4110	2.3005	2.2422	2.1816	2.1183	2.0517	1.9811	1.9055
26	2.5895	2.4909	2.3867	2.2759	2.2174	2.1565	2.0928	2.0257	1.9545	1.8781
27	2.5676	2.4688	2.3544	2.2533	2.1946	2.1334	2.0693	2.0018	1.9299	1.8527
28	2.5473	2.4484	2.3438	2.2324	2.1735	2.1121	2.0477	1.9795	1.9072	1.3291
29	2.5286	2.4295	2.3248	2.2131	2.1540	2.0923	2.0276	1.9591	1.8861	1.8072
30	2.5112	2.4120	2.3072	2.1952	2.1359	2.0739	2.0089	1.9400	1.8664	1.7867
40.	2.3882	2.2882	2.1819	2.0677	2.0069	1.9429	1.8752	1.8028	1.7242	1.6371
60	2.2702	2.1692	2.0613	1.9445	1.8817	1.8152	1.7440	1.6668	1.5810	1.4822
120	2.1570	2.0548	1.9450	1.8249	1.7597	1.6899	1.6141	1.5299	1.4327	1.3104
00	2.0483	1.9447	1.8326	1.7085	1.6402	1.5660	1.4835	1.3883	1.2684	1.0000
	<u> </u>	L								الـــــــا

$$F = \frac{s^{\frac{1}{2}}}{n_{\frac{2}{2}}} = \frac{v_2 S_1}{v_1 S_2}$$

One-sided 97.5 percent test. Two-sided 95.0 percent test.

APPENDIX 3E

Table 4A

E DISTRIBUTION:	LIPPER .	1 PERCENT POINTS
I DISTAIDUTION.	UFFER	I PENCENII PUNVIO

		r	<del></del>	<del></del>		·		·	<del></del>
V <sub>1</sub>	1	2	3	4 .	5	6	7	8 .	9
V <sub>2</sub>			,						, , , , , , , , , , , , , , , , , , ,
1	4052.2	4999.5	5403.3	5624.6	5763.7	5859.0	5928.3	5981.6	6022.5
2	98.503	99.CCO	99.166	99.249	99,299	99.332	99.356	99.374	99.388
3	34.116	30.817	29.457	28.710	28.237	27.911	27.672	27.489	27.345
4	21.198	18.000	16.694	15.977	15.522	15.207	14.976	14.799	14.659
5	16.258	13.274	12.060	11.392	10.967	10.672	10.456	10.289	10,158
t	13.745	10.925	9.7795	9.1483	8.7459	8.4661	8.2600	8.1016	7,9761
7	12.246	9.5466	8.4513	7.8467	7.4604	7.1914	6.9928	6.8401	6.7188
£	11.259	8.6491	7.5910	7.0060	6.6318	6.3707	6.1776	6.0289	5.9106
9	10.561	8.0215	6.9919	6.4221	6.0569	5.8018	5.6129	5.4671	5.3511
10	10.044	7.5594	6,5523	5.9943	5.6363	5.3858	5.2001	5,0567	4.9424
11	9.6460	7.2057	6.2167	5.6683	5.3160	5.0692	4.8861	4.7445	4.6315
12	9.3302	6,9266	5.9526	5.4119	5.0643	4.8206	4.6395	4.4994	4.3875
13,	9.0738	6.7010	5.7394	5.2053	4.8616	4.6204	4.4410	4.3021	4.1911
14	8.8616	6.5149	5.5639	5.0354	4.6950	4.4558	4.2779	4.1399	4.0297
25	8.6831	6.3589	5-4170	4.8932	4.5556	4.3183	4-1415	4.0045	3.8948
16	8.5310	6.2262	5.2922	4.7726	4.4374	4.2016	4.0259	3.8896	3.7804
17	8.3997	6.1121	5.1850	4.6690	4.3359	4.1015	3.9267	3,7910	3.6822
18	8.2854	6.0129	5.0919	4.5790	4.2479	4.0146	3.8406	3.7054	3.5971
19	8.1850	5.9259	5.0103	4.5003	4.1708	<b>3.</b> 9386	3.7653	3.6305	3.5225
20.	8.0960	5.8489	4.9382	4.4307	4.1C27	3.8714	3.6987	3.5644	3.4567
21	8.0166	5.7804	4.8740	4.3688	4.0421	3.8117	3.6396	3.5056	3.3961
22 '	7.9454	5.7190	4.8166	4.3134	3.9880	3.7583	3.5867	3.4530	3.3458
23	7.8811	5.6637	4.7649	4.2635	3.9392	3.7102	3.529C	3.4057	3,2986
24	7.8229	5.6136	4.7181	4.2184	3.8951	3.6667	3 - 4959	3.3629	3.2560
25	7.7698	5.5680	4.6755	4.1774	3.8550	3.6272	3.4568	3, 3239	3.2172
26	7.7213	5.5263	4.6366	4.14CO	3.8183	3.5911	3.4210	3.2884	.3.1818
27	7.6767	5.4881	4.CCC9	4.1056	3.7848	3.5580	3.3882	3.2558	3.14.94
25	7.6356	5.4529	4.5681	4.0740	3.7539	3.5276	3. <u>3</u> 581	3.2259	3.1195
29	7.5976	5.4205	4.5378	4.0449	3.7254	3.4995	3-3302	3.1982	3.0920
30	7.5625	5.3904	4.5097	4.0179	3.6990	3.4735	3.3045.	3.1726	3.0665
40	7.3141	5.1785	4.3126	3.8283	3.5138	3.2910	3.1238	2.9930	2.8876
60	7.0771	4.9774	4.1259	3.6491	3.3389	3.1187	2.9530	2.8233	2.7185
120 <b>Ø</b>	6.8510	4.7865	3.9493	3.4796	3.1735	2.9559	2.7918	2.6629	2.5586
<u> </u>	6.6349	4.6052	3.7816	3.3192	3.0173	2.8020	2.6393	2.5113	2.4073

This table gives the values of F for which  $I_F(v_1, v_2) = 0.01$ .

One-sided 99 percent test.

Two-sided 98 percent test.

APPENDIX 3E

Table 4B

F DISTRIBUTION: UPPER 1 PERCENT POINTS

	10 055.8 9.399.	12 6106.3	15	20	24	30	.40	60	120	8
1 60	055.8 9.399.	6106.3				į.				
1 60	9.399.		· · · · · ·			1		i	į	
	9.399.									
	9.399.		6157.3	6208.7	6234 6	6260.7	6286. <b>8</b>	6313.0	6339.4	6366.0
		99.416	99.432	99.449	99.458	99.466	99.474	99.483	99.491	99.501
	7.229	27.052	26.872	26.69C	26.598	26.505	26.411	26.316	26.221	26.125
	4.546	14.374	14.198	14.020	13.929	13.838	13.745	-13.652	13.558	13.463
	0.051	9.8883	9.7222	9.5527	9.4665	9.3793	9.2912	9.2020	9.1118	9.0204
	.8741	7 7183	7.5590	7.3958	7.3127	7.2285	7.1432	7.0568	6.9690	6.8801
	.6201	6.4691	· 6.3143	6:1554	6.0743	5.9921	5.9084	5.8326	5.7572	5.6495
	.8143	5.6668	5.5151	5.3591	5.2793	5.1981	5.1156	5.0316	4.9460	4.8588
3-	.2565	5.1114	4.9621	4.8080	4.7290	4.6486	4.5667	4.4831	4.3978	4.3105
	.8492	4.7059	4.5582	4.4054	4.3269	4.2469	4.1653	4.0819	3.9965	3.9090
•	.5393	4.3974	4.2509	4.0990	4.0209	3.9411	3.8596	3.7761	3.6904	3.6025
	.2961	4.1553	4.0096	3.8584	3.7805	3,7008	3.6192	3.535 <b>5</b>	3.4494	3.3608
13 4	1003	3.9603	3.8154	3.6646	3.5868	3.5070	3.4253	3.3413	3.2548	3 1554
14 3	。9394	3.80(1	3.6557	3.5052	3.4274	3,3476	3.2656	3.1813	3.0942	-3.CC40
	.8049	3.6662	3.5222	3.3719	3.2940	3.2141	3.1319	3.0471	2.9595	2.8684
16 3	.6909	3.5527	3,4089	3.2588	3.1808	3.1007	3.0182	2.9330	2.84.7	2.7528
	.5931	3.4552	3.3117	3.1615	3.0835	3.0032	2.9205	2.8348	2.745	2.6530
18 3	5082	3 - 3706	3.2273	3.0771	2.9990	2,9185	2.8354	2.7493	2.6597	2.5660
19   3	.4338	3.2965	3.1533	3.0031	2.9249	2.8442	2.7608	2.6742	2.5839	2.4893
	3682	3.2311	3.0880	2.9377	2.8594	2.7785	2.6947	2.6077	2.5168	2,4212
	.3098	3.1729	3.0299	2.8796	2.8011	2.7200	2.6359	2.5484	2.4568	2.3603
	.2576	3:1209	2.9780	2.8274	2.7488	2.6675	2.5831	2.4951	2.4029	2.3055
	,2106	3.0740	2.9311	2.7805	2.7017	2.6202	2.5355	2.4471	2.3542	2.2559
	.1681	3.0316	2.8387	2.7380	2 6591	2.5773	2.4923	2.4035	2.3099	2,2307
	،1294	2.9931	2.8502	2.6993	2.6203	2.5383	2.4530	2.3637	2.2695	2.1694
	1.0941	2.9579	2.8150	2.6640	2.5348	2.5026	2.4170	2.3273	2.2325	2.1315
	.0618	2.9256	2.7827	2.6316	2.5522	2.4699	2.3840	2.2938	2.1984	2.0965
1 -	.0320	2.8959	2.7530	2.6017	2.5223	2.4397	2.3535	2.2629	2.1670	2.0642
	1.0045	2.8685	2.7256	2.5742	2,4946	2.4118	2.3253	2+2344	2.1378	2.0342
	.9791	2.8431	2.7002	2.5487	2,4689	2.3860	2.2992	2.2079	2.1107	2.0062
	2.8CC5	2.6648	2.5216	2,3689	2,2880	2.2034	2.1142	2.0194	1.9172	1.8047
	.6318	2.4961	2.3523	2.1978	2.1154	2.0285	1.9360	1.8363	1.7263	1.6006
	.4721	2.3363	2.1915	2.0346	1.9500	1.8600	1.7628	1.6557	1.5330	1.3805
<b>co</b> 2	.3209	2.1848	2.0385	1,8783	1,7908	1.6964	1.5923	1.4730	1,3246	1.0000

$$F = \frac{3^{\frac{3}{4}}}{5\frac{2}{2}} = \frac{V_2 S_1}{V_1 S_2}$$

One-sided 99 percent test.

Two-sided 98 percent test.

APPENDIX 3F STUDENT'S t-DISTRIBUTION

df	.60	.70	.80	.90	•95	•975	•99	•995
1	.325	.727	1.376	3.078	6.314	12.706	31.821	63.657
-2	.289	.617	1.061	1.886	2.920	4.303	6.965	9.925
3	277	.584	.978	1.638	2.353	3.182	4.541	5.841
4	.271	.569	.941	1.533	2.132	2.776	3.747	4.604
5	.267	.559	.920	1.476	2.015	2.571	3.365	4.032
6	.265	.553	.906	1.440	1.943	2.447	3.143	3.707
7	.263	.549	.895	1.415	1.895	2.365	2.998	3 • 499
8	.262	.546	.889	1.397	1.860	2.306	2.896	3.355
9	.261	.543	.883	1.383	1.833	2.262	2.821	3.250
1ó	.260	.542	.879	1.372	1.812	2.228	2.764	3.169
ii	.26C	.540	.876	1.363	1.796	2.201	2.718	3.106
12	.259	.539	.873	1.356	1.782	2.179	2.681	3.055
13	259	.538	.870	1.350	1.771	2.160	2.650	3.012
14	.258	.537	.868	1.345	1.761	2.145	2.624	2.977
15	.258	.536	.866	1.341	1.753	2.131	2.602	2.947
16	.258	.535	.865	1.337	1.746	2.120	2.583	2.921
17	.257	.534	.863	1.333	1.740	2.110	2.567	2.898
18	.257	.534	.862	1.330	1.734	2.101	2.552	2.878
19	.257	.533	.861	1.328	1.729	2.093	2.539	2.861
.20	.257	.533	.860	1.325	1.725	2.086	2.528	2.845
21	.257	•532°	.859	1.323	1.721	2.080	2.518	2.831
22	.256	.532	.858	1.321	1.717	2.074	2.508	2.819
23	.256	•532	.858	1.319	1.714	2.069	2.500	2.807
24	.256	.531	.857	1.318	1.711	2.064	2.492	2.797
25	.256	.531	.856	1.316	1.708	2.060	2.485	2.787
26	.256	.531	.856	1.315	1.706	2.056	2.479	2.779
27	.256	.531	.855	1.314	1.703	2.052	2.473	2.771
28	.256	•530	.855	1.313	1.701	2.048	2.467	2.763
29	.256	.530	.854	1.311	1.699	2.045	2.462	2.756
30	.256	.530	.854	1.310	1.697	2.042	2.457	2.750
40	.255	.529	.851	1.303	1.684	2.021	2.423	2.704
60	. 254	.527	.848	1.296	1.671	2.000	2.390	2.660
120	. 254	.526	.845	1.289	1.658	1.980	2.358	2.617
ω	.253	.524	.842	1.282	1.645	1.960	2.326	2.576
df								

APPENDIX 3G

AREAS UNDER THE STANDARD

NORMAL CURVE TO THE RIGHT OF THE ORDINATE

T		_ <b>T</b> _	. A	T	A	T	A
.00	.500000C	.22	.4129356	.44	.3299686	.66	.2546269
.01	.4960106	.23	.4090459	.45	.3263552	.67	.2514289
.02	.4920217	.24	.4051651	.46	.3227581	.68	.2482522
.03	.4880335	.25	.4012937	.47	.3191775	.69	.2450971
.04	.4840466	•26	.3974319	.48	.3156137	.70	.2419637
.05 .	.4800612	.27	.3935801	-49	.3120669	.71	.2388521
.06	.4760778	.28	.3897388	.50	.3085375	.72	.2357625
.07	.4720968	.29	.3859081	.51	.3050257	.73	.2326951
.08	.4681186	.30	.3820886	.52	.3015318	.74	.2296500
.09	.4641436	.31	.3782805	.53	.2980560	.75	.2266274
.10	.4601722	.32	.3744842	. 54	.2945985	.76	.2236273
.11	.4562047	.33	.3707000	.55	.2911597	.77	.2206499
.12	.4522416	-34	.3669283	.56	.2877397	.78	.2176954
.13	.4482832	•35	.3631693	.57	.2843388	.79	.2147639
.14	.4443300	.36	.3594236	.58	.2809573	.80	.2118554
.15	.4403823	.37	-3556912	.59	.2775953	.81	.2089701
.16	.4364405	.38	.3519727	.60	.2742531	.82	.2061081
.17	.4325051	•39	.3482683	.61	.2709309	.83	.2032694
.18	.4285763	.40	.3445783	.62	.2676289	.84	.2004542
.19	.42,46546	.41	.3409030	.63	.2643473	.85	.1976625
.20	.4207403	-42	.3372427	.64	.2610863	.86	.1948945
.21	.4168338	.43	.3335978	.65	.2578461	.87	.1921502

.88 .1							
	894297	1.16	.1230244	1.44	.0749337	1.72	.0427162
.99 .1	867329	1.17	.1210005	1.45	.0735293	1.73	.0418151
.90 .18	840601	1.18	.1190001	1.46	.0721450	1.74	.0409295
.91 .18	814113	1.19	.1170232	1.47	.0707809	1.75	.0400592
.92 .17	787864	1 :0	.1150697	1.48	.0694366	1.76	.0392039
.93 .17	761855	1.21	.1131394	1.49	.0681121	1.77	.0383636
.94 .17	736088	1.22	.1112324	1.50	.0668072	1.78	.0375380
.95 .17	710561	1.23	.1093486	1.51	.0655217	1.79	.0367270
.96 .16	685276	1.24	.1074877	1.52	.0642555	1.80	.0359303
.97	660203	1.25	.1056498	1.53	.0630084	1.81	.0351479
.98 .10	635431	1.26	.1038347	1.54	.0617802	1.82	.0343795
.99 .10	610871	1.27	.1020423	1.55	.0605708	1.83	.0336250
1.00	586553	1.28	.1002726	1.56	.0593799	1.84	.0328841
1.01 .1	562476	1.29	.0985253	1.57	.0582076	1.85	.0321568
1.02	538642	1.30	.0968005	1.58	.0570534	1.86	.0314428
1.03	515050	1.31	.0950979	1.59	.0559174	1.87	.0307419
1.04	491700	1.32	.0934175	1.60	.0547993	1.88	.0300540
1.05 .1.	468591	1.33	.0917591	1.61	.0536989	1.89	.0293790
1.06	445723	1.34	.0901227	1.62	.0526161	1.90	.0287166
1.07 .1.	423097	1.35	.0385080	1.63	.0515507	1.91	.0280666
1.08 .1.	400711	1.36	.0869150	1.64	.0505026	1.92	.0274289
1.09 .1	378566	1.37	.0853435	1.65	.0494715	1.93	.0268034
1.10 .1	356661	1.38	.0837933	1.66	.0484572	1.94	.0261898
1.11	334995	1.39	.0822644	1.67	.0474597	1.95	.0255881
1.12 .1	313569	1.40	.0807567	1.68	.0464787	1.96	.0249979
1.23 .12	292381	1.41	.0792698	1.69	.0455140	1.97	.0244192
1.14 .13	271432	1.42	.0778038	1.70	.0445655	1.98	.0238518
1.15 .12	250719	1.43	.076358 <b>5</b>	1.71	.0436329	1.99	.0232955

## APPENDIX 3G (Continued)

T	A	T	A	T	A	<u> </u>	A
2.00	.0227501	2.26	.0119106	2.52	.0058677	2.78	.0027179
2.01	.0222156	2.27	.0116038	2.53	.0057031	2.79	.0026354
2.02	.0216917	2.28	.0113038	2.54	.0055426	2.80	.0025551
2.03	.0211783	2.29	.0110107	2.55	.0053861	2,81	.0024771
2.04	.0206752	2.30	.0107241	2.56	.0052336	2.82	.0024012
2.05	.0201822	2.31	.0104441	2.57	.0050849	2 <b>.83</b>	.0023274
2.06	.0196993	2.32	.0101704	2.58	.0049400	2.84	.0022557
2.07	.0192262	2.33	.0099031	2.59	.0047988	2.85	.0021860
2.08	.0187628	2.34	.0096419	2.60	.0046612	2.86	.0021182
2.09	.0183089	2.35	.093867	2.61	.0045271	2.87	.0020524
2.10	.0178644	2.36	.0091375	2.62	.0043965	2.88	.0019884
2.11	.0174292	2.37	.0088940	2.63	.0042692	2.89	.0019262
2.12	.0170030	2.38	.0086563	2.64	.0041453	2.90	.0018658
2.13	.0165858	2.39	.0084242	2.65	.0040246	2.91	.0018071
2.14	.0161774	2.40	.0081975	2.66	.0039070	2.92	.0017502
2.15	.0157776	2.41	·CC79763	2.67	.0037926	2.93	.0016948
2.16	.0153863	2.42	.0077603	2.68	.0036811	2.94	.0016411
,2.17	.0150034	2.43	.0075494	2.69	.0035726	2.95	.0015889
2.18	.0146287	2.44	.0073436	2.70	.0034670	2.96	.0015382
2.19	.0142621	2.45	.0071428	2.71	.0033642	2.97	.0014690
2.20	.0139034	2.46	.0069469	2.72	.0032641	2.98	.0014412
2.21	.0135526	2.47	.0067557	2.73	.0031667	2.99	.0013949
2.22	.0132094	2.48	.0065691	2.74	.0030720	3.00	.0013449
2.23	.0128737	2.49	.0063872	2.75	.0029708	3.01	.0013062
2.24	.0125455	2.5C	.062097	2.76	.0028901	3.02	.0012639
2.25	.0122245	2.51	.0060366	2.77	.0028028	3.03	.012228

## APPENDIX 3G (Continued)

<u>T</u>	A	<u>T</u>	A	T	A	<u>T</u>	A
3.04	.0011829	3.28	.0005190	3.52	.0002158	3.76	.0000850
3.05	.0011442	3.29	.005009	3.53	.coo2078	3.77	.000816
3.06	.0011067	3.30	.0004834	3.54	.0002001	3.78	.0000784
3.07	.0010703	3.31	.0004665	3.55	.0001926	3.79	.0000753
3.08	.0010350	3.32	.0004501	3.56	.CC01854	3.80	.000723
3.09	.0010008	3.33	.0004342	3.57	.0001785	3.81	.0000695
3.10	.0009676	3.34	.0004189	3.58	.0001718	3.82	.0000667
3.11	.0009354	3.35	.0004041	3.59	.0001653	3.83	.0000641
3.12	.0009043	3.36	.0003897	3.60	.0001591	3.84	.0000615
3.13	.0008740	3.37	.0003758	3.61	.0001531	3.85	.0000591
3.14	.0008447	3.38	.00(3624	3.62	.001473	3.86	.cocc 567
3.15	.0008164	3.39	.COC3495	3.63	.0001417	3.87	.0000544
3.16	.0007888	3.40	.0003369	3.64	.0001363	3.88	.0000522
3.17	.0007622	3.41	.0003248	3.65	.0001311	3.89	.0000501
3.18	.CCC7364	3.42	.0003131	3.66	.001261	3.90	.00004.81
3.19	.0007114	3.43	.0003018	3.67	.0001213	3.91	.0000461
<del>3.</del> 20	.0006871	3.44	.0002909	3.68	.0001166	3.92	.0000.443
3.21	.0006637	3.45	.0002803	3.69	.0001121	3. 93	.0CC0425
3.22	.0006410	3.46	.0002701	3.70	.0001078	3.94	.C000407
3.23	.0006190	3.47	.0002602	3.71	.0001036	3.95	.0000391
3.24	.0005976	3.48	.0002507	3.72	.0000996	3.96	.000C375
3.25	.0005770	3.49	.0002415	3.73	.0000957	3.97	.0000359
3.26	.0005571	3.50	.0002326	3.74	.0000920	3.98	.0000345
3.27	.0005377	3.51	.0002241	3.75	.0000884	3.99	.COOC330

# APPENDIX 3G (Continued)

T	A	T	A	<u>.T</u>	A	<u></u>	<u> </u>	A
4.00	.0000317	4.27	.000098	4.54	.000028			,
4.01	.0000304	4.28	.0000093	4.55	.0000027			
4.02	.00/CC291	4.29	.0000089	4.56	.0000026	•		·
4.03	.000C279	4.3C	.0000085	4.57	.0000024			
4.04	.0000267	4.31	.0000082	4.58	.0000023			
4.C5	.0000256	4.32	.0000078	4.59	.0000022	•		
4.06	.0000245	4.33	.0000075	4.60	.0000021		•	
4.07	.0000235	4.34	.0000071	4.61	.COC0020			,
4.08	.000225	4.35	.000068	4.63	.0000019		•	
4.09	.000216	4.36	.0000065	4.63	.0000018			,
4.10	.6060207	4.37	.0000062	4.64	.000017			
4.11	.0000198	4.38	.0000059	4.65	.000017			,
4.12	.000189	4-39	.000057	4.66	.000016			
4.13	.000181	4.40	.COCC054	4.67	.000015			
4.14	.0000174	4.41	.0000052					
4.15	<b>.0</b> C0C <b>166</b>	4.42	.0000049	•				
4.16	.0000159	4.43	•000C047				,	
4.17	.00CC152	4.44	.0000045					
4.18	.0000146	4.45	.0000043					,
4.19	.0000139	4.46	.0000041					
4.20	.0000133	4.47	•0000039		•			1
4.21	.0000128	4.48	.0000037					i
4.22	.0000122	4.49	.000036		• .			
4.23	.0000117	4.50	.000034				•	
4.24	.000112	4.51	.000032			•		r .
4.25	.000107	4.52	.000.0031					
4.26	.0000102	4.53	.000030				· •	

Table 1

Upper 90- and 95-Percent Confidence Bounds for the Number of Defectiv
in a Finite Lopulation of 40 Members.

Number of	<del></del>	<del> </del>		S	ample S	ize				
Observed	2	2	4		8	3	1	6	3	2
Defectives	90	95	90	95	90	95	90	95	90	95
0 1 2 3 4 5	26 37 40	30 38 40	16 26 33 38 40	20 29 35 39 40	9 15 20 25 29 33	11 17 22 27 31 34	4 7 10 13 16 18	5 8 11 14 17 20	1 2 4 5 7 8	1 3 4 6 7 9
7 8 9 10					36 39 40	37 39 40	21 23 25 28 30	22 24 27 29 31	9 11 12 13 15	10 11 13 14 15
11 12 13 14 15							32 34 36 38 39	33 35 37 38 39	16 17 18 20 21	16 18 19 20 21
16 17 18 19 20			,				40	40	22 23 25 26 27	23 24 25 26 27
21 22 23 24 25									28 29 31 32 33	29 30 31 32 33
26 27 28 29 30								,	34 35 36 37 38	34 35 36 37 38
31 32									39 40	39 40

**APPENDIX 3H** 

Table 2

Upper 9C- and 95-Percent Confidence Bounds for the Number of Defectives in a Finite Population of 60 Members.

Number of					Sample	∋ Size				
Observed		3		6		12	2	24 .	1	8
Defectives	90	95	90	95	90	9,5	90	95	90	95
0 1 2 3 4 5	31 47 57 60	37 51 58 60	18 29 39 47 54 58	22 33 42 50 55 59	9 16 21 27 32 37	11 18 24 30 35 39	4 7 10 13 16 19	5 9 12 15 18 21	1 2 4 5 7 8	1 3 4 6 7 9
6 7 8 9 10			60	60	41 46 50 53 56	44 48 51 54 57	22 24 27 29 32	23 26 29 31 33	10 11 12 14 15	10 12 13 14 16
11 12 13 14 15		,			59 60	59 60	34 37 39 41 44	36 38 41 43 45	16. 17 19 20 21	17 18 19 21 22
16 17 18 19 20							46 48 50 52 54	47 49 51 53 55	23 24 25 26 28	23 25 26 27 23

APPENDIX 3H

## Table 2 (Continued)

Upper 90- and 95-Percent Confidence Bounds for the Number of Defectives in A Finite Population of 60 Members.

Number of	Sample Size												
Observed		3		6		12	2	4	48				
Defectives	90	95	9C	95	-90	95	90	95	90	95			
21 22 23 24 25 26 27 28 29 30							56 58 59 60	57 58 59 60	29 30 31 33 34 35 36 37 39 40	30 31 32 33 34 36 37 38 39 40			
31 32 33 ,34 35					,				41 42 44 45 46	42 43 44 45 46			

Table 3

Upper 90- and 95-Percent Confidence Bounds for the Number of Defectives in a Finite Fopulation of 100 Members.

Number of				<del></del>	Sa	mple Si	ze	<del></del>	······································	
Observed	:	5	10	0	·	c.	40		ε	0
Defectives	90	95	90	95	90	95	90	95	90	95
C 1 2 3 4 5	36 57 74 88 97 100	44 64 80 91 98 100	19 32 43 54 63 72	24 38 49 59 68 76	9 16 23 28 34 39	12 19 26 32 38 43	7 11 14 17 19	5 9 12 15 19 21	1 3 4 5 7 8	1 3 5 6 7 9
6 7 8 9 10		,	80 87 94 98 100	84 90 95 99 100	45 50 55 60 64	48 53 58 63 68	22 25 28 30 33	24 27 30 33 35	10 11 12 14 15	10 12 13 14 16
11 12 13 14 15				•	69 73 78 82 86	72 76 80 84 88	36 38 41 44 46	38 41 43 46 48	16 18 19 20 22	17 18 20 21 22
16 17 18 19 20	,				90 93 97 99 100	91 95 97 99 100	49 51 54 56 58	51 <sup>-</sup> 53 56 58 61	23 24 25 27 28	24 25 26 <b>28</b> <b>29</b>
21 22 23 24 25		,					61 63 66 68 70	63 65 68 70 72	29 31 32 33 34	30 32 33 34 35
26 27 28 29 30							73 75 77 80 82	75 77 79 81 83	36 37 38 40 41	37 38 39 40 42
31 32 33 34 35							84 86 88 90 92	85 87 89 91 93	42 43 45 46 47	43 44 45 47 48

Table 4

Upper 90- and 95-Percent Confidence dounds for the Number of Defectives in a Finite Population of 200 Members.

Number of	<u> </u>	<del></del>			Say	mple Si	ze			
Observed	1	0	2	0	4	-	80	)	16	0
Defectives	90	95	90	95	90	95	90.	95	90	95
0 1 2 3 4 5	40 66 88 109 128 145	50 77 100 120 138 154	20 34 47 59 70 81	26 41 54 66 78 89	10 17 23 30 36 42	12 20 27 34 40 46	4 8 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 8	1 3 5 6 8 9
6 7 8 9 10	161 176 188 197 200	169 181 192 198 200	91 102 112 121 131	99 109 119 128 137	47 53 58 64 69	52 58 63 69 74	23 26 29 31 34	25 28 31 34 37	10 11 12 14 15	10 · 12 · 13 · 15 · 16
11 12 13 14 15 16 17 18 19 20 21 22 23			140 149 157 165 173 181 188 194 198 200	146 155 163 170 178 184 190 196 199 200	74 80 85 90 95 100 105 110 125 129 134	80 85 90 95 100 105 110 115 120 125 129 134 139	37 40 42 45 48 53 56 58 61 64 69	40 42 45 48 51 56 59 61 67 69 72	16 18 19 20 22 23 22 26 27 28 30 31	17 19 20 21 23 24 23 27 28 29 31 32 33
24 25 26 27 28 29 30 31 32 33 34 35					139 143 148 153 157 161 166 170 274 178 182 186	143 148 152 157 161 165 169 173 177 181 185 188	71 74 77 79 82 84 87 89 92 94 97	74 77 80 82 85 87 90 92 95 97 100	34 35 36 37 39 40 41 43 44 45 47 48	35 36 37 39 40 41 43 44 45 46 48 49

APPENDIX 3H

Table 5

Upper 9C- and 95+ Percent Confidence Bounds for the Number of Defects in a Finite Population of 220 Members.

_	T. 3 TIME	± اړ∪≱		240 %					· · · · · · · · · · · · · · · · · · ·		
	Natur of			,, · · -	Sa	mple Si	ze	•			
1	Cuserved	1	.2	2	4	4	8	9	Θ	. 19	92
	Defectives	9C	32	90	95	90	95	90	95	èС	95
	0 1 4 3 4 5	40 67 91 112 133 152	51 79 103 125 144 103	20 35 43 40 71 83	26 44 55 68 80 91	10 17 24 30 36 44	13 21 28 34 41 47	4 3 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 3	1 3 5 6 8, 9
	6 7 9 10	169 186 202 216, 223	179 195 209 241 232	93 104 114 124 134	102 112 123 133 144	13 53 53 53 70	53 58 64 70 75	25 26 29 31 34	25 28 31 34 37	10 11 12 14 15	10 12 13 15 16
•	11 12 13 14 15	237 240 ,	239 240	144 153 163 172 180	152 161 170 179 137	75 31 36 41 90	31 86 92 97 102	37 40 43 45 45	40 45 45 48 51	16 18 19 20 22	17 19 20 21 23
	16 17 13 19 20			169 193 106 1213 241	195 203 211 218 224	102 107 112 117 12.	107 112 117 122 127	51 53 56 59 61	54 56 59 62 65	23 24 20 27 23	23 25 27 28 29
	21 22 23 24 25	,		223 234 239 240	230 236 239 240	127 132 137 142 146	132 137 142 147 152	64 67 69 72 74	67 70 73 75 78	30 31 32 34 35	31 32 33 35 36
	26 27 28 29 30					151 150 161 165 170	150 101 166 170 175	77 30. 82 85 87	30 33 86 83 91	36 38 39 40 41	37 39 40 41 43
	31 32 33 34 35					175 179 184 188 193	179 184 188 193 197	90 93 95 98 100	93 96 99 101 104	43 44 45 47 48	44 45 47 48 49

Table 6

Upper 90- and 95- Percent Confidence Bounds for the Number of Defectives in a Finite Population of 300 Members.

	· ·									<del></del>
Number of			Sa	umple Si	28		<u> </u>		·	
Observed	1	5	3	С	6	0	12	2C	24	.0
Defect ives	90	95	90	95	90	95	90'	95	90	95
0 1 2 3 4 5	41 69 93 116 137 158	53 82 107 130 151 171	21 35 48 61 73 84	27 42 56 69 81 93	10 17 24 30 36 42	13 21 28 34 41 47	4 8 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 8	1 3 5 6 8 9
6 7 8 9 10	177 196 214 231 247	190 208 225 241 256	95 106 117 127 138	104 115 126 137 147	48 54 60 65 71	53 59 65 71 76	23 26 29 32 34	25 28 31 34 37	10 11 12 14 15	10 12 13 15 16
11 12 13 14 15	262 276 288 297 300	270 282 292 299 300	148 158 168 177 187	157 167 177 186 196	76 82 87 92 98	82 88 93 98 104	37 40 43 45 48	40 43 46 49 51	16 18 19 21 22	17 19 20 21 23
16 17 18 19 20			196 206 215 224 233	205 214 223 231 240	103 108 113 119 124	109 114 120 125 130	51 54 56 59 62	54 57 60 62 65	23 24 26 27 28	24 26 27 28 30
21 22 23 24 25			241 250 285 266 274	248 256 264 271 278	129 134 139 144 149	135 140 145 150 155	64 67 70 72 75	68 70 73 76 79	30 31 32 34 35	31 32 34 35 36
26 27 28 29 30			281 288 294 298 300	285 291 296 299 300	154 159 164 169 174	160 165 170 175 180	78 80 83 86 88	81 84 87 89 92	36 38 39 40 42	37 39 40 41 43
31 32 33 34 35					179 184 189 193 198	185 190 194 199 204	91 93 96 99 101	94 97 100 102 105	43 44 45 47 48	44 45 47 48 49

Table 7

Upper 9C- and 95- Percent Confidence Bounds for the Number of Defectives in a Findle Population of 360 Members.

					<del></del> _					
Number of		<del></del>	r <del>r</del>	Se	ample S	ize ·	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		···	· — · · · · · · · · · · · · · · · · · ·
Observed		18		36		72	1.	44	28	38
Defectives	90	95	90	95 -	90	95	90	95	90	95
0 1 2 3 4 5	42 70 95 119 141 162	53 84 110 133 156 177	21 36 49 61 73 85	27 43 57 70 82 94	10 17 24 30 36 42	13 21 28 35 41 47	4 8 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 8	1 3 5 6 8 9
6 7 8 9	182 202 221 240 258	197 217 235 253 270	96 108 118 129 140	106 117 129 139 150	48 54 60 66 71	54 60 66 71 77	23 26 29 32 35	25 28 31 34 37	10 11 12 14 15	10 12 13 15 16
11 12 13 14 15	275 292 308 323 336	287 302 317 330 342	150 161 171 181 191	161 171 181 191 201	77 82 88 93 99	83 88 94 100 105	37 40 43 46 48	40 43 46 49 52	17 18 19 21 22	17 19 20 22 .23
16 17 18 19 20	348 357 360	352 359 360	201 211 220 230 239	211 220 230 239 248	104 109 115 120 125	110 116 121 127 132	51 54 57 59 62	54 57 60 63 65	23 25 26 27 28	24 26 27 28 30
21 22 23 24 25			248 258 267 276 285	257 266 275 284 292	130 135 141 146 151	137 142 148 153 158	65 67 70 73 75	68 71 74 76 79	30 31 32 34 35	31 32 34 35 36
26 27 28 29 30			293 302 310 318 326	300 308 316 324 331	156 161 166 171 176	163 168 173 178 183	78 81 83 86 89	82 84 87 90 92	36 38 39 40 42	38 39 40 42 43
31 32 33 34 35			334 341 348 354 359	338 345 351 356 359	181 186 191 196 201	188 198 203 208	91 94 96 99 102	95 98 100 103 106	43 44 45 47 48	44 45 47 48 49

Table 8

Upper 90- and 95-Percent Confidence Bounds for the Number of
Defectives in a Finite Population of 400 Members.

Number of				Sa	mple S	lze	·			
Obse <b>rve</b> d	20		. 4	<b>,</b> 0		3C	16	xo ]	32	0
<b>Tefectives</b>	90	95	90	95	9C	95	90	95	90	95
0 1 2 3 4	42 71 96 120 142 164	54 84 111 135 158 180	21 36 49 62 74 86	27 43 57 70 83 95	10 17 24 30 37 43	1.3 21 28 35 41 48	4 8 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 8	1 3 5 6 8 9
6 7 8 9 10	185 205 225 244 263	201 221 240 259 277	97 108 119 130 141	107 119 130 141 152	49 54 60 66 71	54 60 66 72 77	23 26 29 32 35	26 29 32 34 37	10 11 12 14 15	10 12 13 15 16
11 12 13 14 15	281 299 316 332 348	294 311 327 342 357	152 162 172 183 193	162 173 183 194 204	77 83 88 94 99	83 89 94 100 106	37 40 43 46 48	40 43 46 49 52	17 18 19 21 22	17 19 20 22 23
16 17 18 19 20	363 376 328 397 400	370 382 392 399 400	203 213 223 233 242	214 224 233 243 253	104 110 115 120 126	111 117 122 127 133	51 54 57 59 62	54 57 60 63 66	23 25 26 27 29	24 26 27 28 30
21 22 23 24 25			252 261 271 280 289	262 271 280 289 298	131 136 141 147 152	138 143 149 154 159	65 68 70 73 76	68 71 74 77 79	30 31 32 34 35	31 32 34 35 36
26 27 28 29 30			298 307 316 325 333	307 316 324 333 341	157 162 167 172 177	164 169 174 180 185	78 81 84 86 89	82 85 87 90 93	36 38 39 40 42	38 39 40 42 42
31 32 33 34 35			342 350 358 366 374	349 357 364 371 378	183 188 193 198 203	190 195 200 205 210	91 94 97 99 102	95 98 101 103 106	43 44 46 47 48	44 46 47 48 49

Table 9

Upper 90- and 95-Percent Confidence Bounds for the Number of Defectives in a Finite Population of 500 Members.

Number of				Sa	mple Si	<b>z</b> e				
Ctserved		25		50		100	20	0	40	00
Defectives	90	95	90	95	90	95	90	95	90	95
0 1 2 3 4 5	42 72 98 122 145 168	55 86 113 138 162 185	21 36 49 62 74 86	27 43 58 71 84 96	10 17 24 30 37 43	13 21 28 35 42 48	4 8 11 14 17 20	5 9 13 16 19 22	1 3 4 5 7 8	1 3 56 8 9
6 7 8 9 10	190 211 232 252 272	207 229 249 269 289	98 110 121 132 143	109 120 132 143 155	49 55 60 66 72	54 60 66 72 78	23 26 29 32 35	26 29 32 35 38	10 11 12 14 15	10 12 13 15 16
11 12 13 14 15	291 310 329 348 366	308 327 345 363 380	154 165 175 186 196	166 176 187 198 208	78 83 89 94 100	84 90 95 101 107	37 40 43 46 49	40 43 46 49 52	17 18 19 21 22	17 19 20 22 23
16 17 18 19 20	383 400 417 433 448	397 413 428 443 457	207 217 227 237 247	219 229 239 250 260	105 111 116 121 127	112 118 123 129 134	51 54 57 60 62	55 58 60 63 66	23 25 26 27 29	24 26 27 28 30
21 22 23 24 25	463 477 489 497 500	470 482 492 499 500	257 267 277 287 297	270 279 289 299 309	132 137 143 148 153	140 145 150 156 161	65 68 70 73 76	69 71 74 77 80	30 31 32 34 35	31 32 34 35 36
26 27 28 29 30		e	307 216 326 335 345	318 327 337 346 355	159 164 169 174 179	166 172 177 182 187	79 81 84 87 89	82 85 88 91 93	36 38 39 40 42	38 39 40 42 43
31 32 33 34 35			354 363 372 381 390	364 373 382 391 400	185 190 195 200 205	193 198 203 208 213	92 94 97 100 102	96 99 101 104 107	43 44 46 47 48	44 46 47 48 50

#### **FACTORIAL TREATMENT PROCEDURE WORKSHEETS**

Table 1

#### 4 TREATMENTS AND 8 ITEMS

Design: 1/2 X 24 (Ref. 15, page 484)

Item numbers											
Treatments		1	2	3	4	5	3	7	8		
	4		+	+	,	+		ļ	+		
I	в	ы	+		+		+		+		
		NONE		+ .	. · <b>+</b> ·			.+	+		
. 1	۵					+	+	+	+		
Results						,					

- 1. All main effects are clear of two-factor interactions.
- 2. Two-factor interactions are confused with one another and are not measurable.
- 3. Three-factor and higher order interactions are assumed negligible.

**APPENDIX 4** 

Table 2

### 5 TREATMENTS AND 8 ITIMS

Design:  $1/4 \times 2^5$  (Ref. 15, page 484)

	•			Item r	umbers	3		<b>.</b>	
Treatments		1_	2	3	4	5	6	7	8
	A		+		+	+		+	
	В			+	+	+	+		
•	C	NONE		+ .	+		1	+	+
	D		+		+		+		+
,	E					+	+	+	+
Results									

- 1. All main effects are confused with two-factor interactions.
- 2. All interactions are assumed negligible.

Table 3

#### 6 TPEATMENTS AND 8 ITEMS

Design: 1/8 X 26 (Ref. 15, page 485)

	,			Item n	mbers				
Treatments		1	2	3	4	5	6	7	8
	A		+		+ '	+		+	
	В			+	+		,	+	+
	С	63	+ .		+	·	+		+
	D	NONE		+	+	+	+ ,		
•	E		+	+			+	+	
	F					+	+	+	+
Results									
D		<u> </u>	ļ		Ļ			لسنسا	

- 1. All main effects are confused with two-factor interactions.
- 2. All interactions are assumed negligible.

APPENDIX 4

Table 4

## 7 TREATMENTS AND 8 ITEMS

Design: 1/16 X 27 (Ref. 15, page 485)

Treatments		1	2						
	A			3	4	5	6	7	8
	•		+	+	+	+			
	В		+	+			+	+	
	C		+		+	,	+		+
	ם	NO NE	+			+ -	,	+	+
	E	2		+	+			+	+
	F			- <b>+</b>		<b>,+</b>	+		+,
	G		·		+	+	+	+	
Results						,			

- 1. All main effects are confused with two-factor interactions.
- 2. All interactions are assumed negligible.

**APPENDIX 4** 

Table 5

## 7 TREATMENTS AND 8 ITEMS

Design: Multifactorial (Ref. 5, page 323)

				Item n	umbers				
Treatments	_	1	2	3	4	5	6	7 .	8
	A				+		+	+	+
:	В	'		+		+	+	+	٠.
	С		+		+	+ ,	+		
•	D	臣		+	+	+			+
	E	NONE	+	.+	+			+	
	F		+	` <b>+</b>			+		+
	G		+			+		+	+
Results						,			

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

APPENDIX 4

Table 6

## 8 TREATMENTS AND 12 ITEMS

Design: Multifactorial (Ref. 5, page 323)

•					It	em r	umbe	rs					
Treatments		1	2	3	4	5	6	7	8	9	10	11	12
	A			+				+	+	+		+	+
	В		+				+	+	+	•	÷	+	
	C		•			+	+	+		+	+		+
i i	D	NONE			+	+	. + ,		+	+		+	
	E	ž		+	+	+		+	+		+		,
	F		+	+	+		+	+		+			
	G		+	+		+	+		+	,			+
	H		+		+	+		+				+	+
Results													
		L	لبسيا				<u>'</u>			L	L	,	

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negigible.

Table 7

## 9 TREATMENTS AND 12 ITEMS

Design: Multifactorial (Ref. 5, page 323)

	_							•					
						It em	ກນກາໄ	bers					
Treatments	_	1	2	3	4	5	6	7	8	9	10	11	12
. *	A			+	-'			+	+	+		+	+
	В		+				+	+	+		+	+	
	С				'	+	+	+		+	+		+
1	D			, ,	+	+,	+		+	+		+	
	E	NONE		+	+	+		+	+		+		
	F		+	+	+	<u> </u>	+	+		+			
	G		+	+		+	+		+				+.
•	H		+		+ .	+		+		ŀ		+	+
	I			+	+		+				+	+	+
Results													,
Remarks:		<u> </u>	<b></b>	L	<u> </u>	L	<u> </u>	<u> </u>	<u></u>	<u> </u>	<u></u>	<u> </u>	

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

**APPENDIX 4** 

Table 8

## 10 TREATMENTS AND 12 ITEMS

Design: Multifactorial (Ref. 5, page 323)

			-P •					1601	-,	F-0-	7~7	1.	
					I	tem	numb	er <b>s</b> .					
Treatment		1	2	3	4	5	6	7	8	9	10	11	12
	A			+				+	+	.+		+	+
	В	١,	+				+	+	+		+	+	
	C					+	+	+		+	+		+
	D				+	+	+		+	+		+	
	E	NONE		+	+	+		+	+	:	+		
	F	2	+	+	+		+	+		.+			
	G		+.	+		+	+		+				+
	H		+		+	+		+				+	+
	I			+	+		+				+	+	+
	J		+	+		+				+	+	+	
Results													
E-marke.				<u> </u>	L	L		ļ	l		7	L	

#### <u>Remarks:</u>

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

Table 9

## 11 TREATMENTS AND 12 ITEMS

Design: Multifactorial (Ref. 5, page 323)

1			-6								7-71		
					I	tem 1	nampe	ers					
Treatment s	_	1	2	3	4	5	6	7	8	9	10	11	12
	٨			+				+	+	, +		+	+
	В						+	+	انا		_	_	
i	_							•	*			Τ.	l
	C		,			4.	+	+		+	+		+
	D				+	+	+		+	+		+	·
•	E	<b>6</b> 3		+	+	+		+	+		+		
	F	ENCK.	+	+	+		+	+		+			
	G		+	+		+	+		+				+
•	н		+		+	+		+				+	+
	I			+	+		+				<b>4</b> ·	. +	+
	J		+	+		+				+	+	+	
	K	,	+		+				+	+	+		+
Results				,		·							
Remarks:													

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

Table 10

### 5 TREATMENTS AND 16 ITEMS

Design: 1/2 X 2<sup>5</sup> (Ref. 6, page 5)

							It	em	กบระ	ber	8		<u> </u>				
Treatments	_	7	2	3	4	5	6	7	8	9	10	11	12	::3	14	15	16
	•		+		+	+		+		+	,	+			+	,	+
	B		+		+	+		+			+		+	+		<b>+</b> ,	
	С	NCNE	+		+		+		+	+		+		+		÷	
•	a		+	+			+	+			+	+			+	+	
	E			+	+			+	+			+	÷			+	+
Blocks	,				1			,					I	I	1		
Results		·					·										

- 1. All main effects are clear of two-factor interactions.
- 2. When blocks are not used all two-factor interactions are measurable. When blocks are used the AB interaction is not measurable.
- All three-factor and higher order interactions are assumed negligible.

Table 11

#### 5 TREATMENTS AND 16 ITEMS

Design: 1/2 X 2<sup>5</sup> (Ref. 6, page 5)

•													4			
				I	tem	numb	ers									]
Treatments	ī	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
A		+	+		+			+	+			+		+	+	
В		+	+		+			+		+	+		+.			+
С	NONE	+	+		,	+	+		+			+	+			+
D	1	+		+	+		+		+		+			+		+
E			+	+	+	+			+	+			,		+	+
Blocks '		1				IJ				1:	II.			IV	,	
Results																

#### Remarks:

- 1. All main effects are clear of two-factor interactions.
- 2. When blocks are not used, all two-factor interactions are measurable.

When blocks are used, interactions AB, AC, and BC are not measurable.

3. All three-factor and higher order interactions are considered negligible.

#### Table 12

#### 6 TREATMENTS AND 16 ITIMS

Design: 1/4 X 26 (Factorial (Ref. 6, page 18)

•						Iten	טמ ו	mbe	rs							
Treatments	1	2	3	4	٤	٤	7	8	ò	ic	11	12	13	14	15	16
Á		+	+		+			+	+			+		+	+	
В		+	+			+	+		+			+	+			÷
С	E	+		+	+	,	+		+		+			+	,	+
	NONE	+		+		+		+	+		+		+		+	
E			+	+			+	+	+	•⊧			+	+		
F			+	+	.+	+			+	+					+	+
Blocks				I								I	I			
Results																

#### Remarksi

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assume negligible.

Table 13

#### 6 TREATMENTS AND 16 ITEMS

Design: 1/4 X 26 Factorial (Ref. 6, page 18)

	Г		-			74			<u> </u>							
	L					11	em	וועטמ	bers	} <del></del>		,	<del></del>			
Treatments	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
· .	2	+	+		+			+	+		•	+	 	+	+	
	в	+	+		+			+		+	+	, ,	+		,	+
. (	c <sub>j</sub>	+	·	+	+		+		+		+'			+		+
	NON	+		+	+		+			+		+	+		+	
:	E		+	+	+	+					+	+	+	+		
	F		+	+	+	+			+	+					+	+.
Blocks	L		<u> </u>				II			I	11			IV	7	
Results																

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

Table 14

## 6 TREATMENTS AND 16 ITUS

Design: 1/4 X 25 Factorial (Ref. 6, page 18)

	•												<del>-                                    </del>			<del> </del>	
					_		Ite	מת	mp	ers							
Treatments	_	1	2	3	4	5	દ	7	8	9	10	11	12	13	14	15	16
•	A		+		+	+		+			+		+	+		<b>+</b> '	
	В		+		+	+		+		+		+			+ -		+
	С	NONE	+	+			+	+			+	+			+	+	
	ם	M	+	+		+			+		+	+		+			+
	E	·	+	+	'		+	+		+			+	+			+
	F		+	+		+			+	+			+		+	+	
Blocks		1		I	Ι	III		IV		V		VI		V:	II	VI	11
Results													:				

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

#### Table 15

### 7 TREATMENTS AND 16 ITEMS

Design: 1/8 X 2 Factorial (Ref. 6, page 30)

				,		Ite	מ	<b>map</b>	ers	<b>.</b>					'	
Treatments	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
		+	+		+			+		+	+		+			+
В		+	+		+			+	+			+		+	+	
C		+	+			+	+			+	+		,	+	+	
D	NONE	+	+			+	+		+			+	+			+
E		+		+	+		+		,	+		+	+		.+	
F		+		+		+		+	+		+		+		+	
G		+		+	+	. ,	+		+		+			+		+
Blocks				I				,	·			11	,	,		
Results					•									,		

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

Table 16

## 7 TREATMENTS AND 16 ITEMS

Design: 1/8 X 2<sup>7</sup> Factorial (Ref. 6, page 30)

	Item numbers															
Treatments	1	2	3	4	5	6	7	2	9	10	11	12	1.3	14	15	16
A		+	+		+	· .		+		+	+		+			+
Ē		+	+		+			+	+		·	+		+	+	
С	,	+	+			+	+			+	+			+	+	
ٔ <del>۵</del> .	NONE	+	+			+	+		+			+	+		,	+
E		+		+	+		+			+		+	+		+	
F		+		+		+		+	+		+		+		+	
G		+		+	+		+		+		+			+		+
Blocks	I				II				III				IV			
Results							,									

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

Table 17

# 8 TREATMENTS AND 16 ITCMS

Design: 1/16 X 28 Factorial (Ref. 6, page 42)

		,				Ite	ימ ב	umb	ers							
Treatments	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
<b>A</b>			+	+	+	+			+	+					+	+
В			+	+	+	+					+	+	+	+	ı	
C		+	+		+			+	+			+		+	+	
D		+	+		+			+		+,	+		+			+
E	題	+		+	+		+			+		+	+		+	
P	NONE	+		+	+		+		+		+			+		+
G					+	+	+	+	+	+	+	+				
н					+	+	+	+					+	+	+	+
Blocks		<b>.</b>	,	I								1]				
Results										,						

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

fable 18

# 8 TREATMENTS AND 16 ITEMS

Design: 1/16 X 28Factorial (Ref. 6, page 41)

						It	em :	num	ber	<b>s</b>						
Treatments	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
A		+	+		+			+		+	+		+,			+
. В		+	+ ,			+	+			+	+			+	+	
C		+	+		+			+	+			+		+	+	
מ		+	+			+	+		+			+	+ ,			+
E	NONE		+	+			+	+	+	+			+	+		
r	NO		+	+	+	+			+	+					+	+
. <b>G</b>			+	+	+	+					+	+	+	+		
н			+	+			+	+			+	+			+	+
Blocks		I	,			ĮΙ				111				ĪΔ		
Results															,	

- 1. All main effects are clear of two-factor interactions.
- 2. All two-factor interactions are confused with one another and are not measurable.
- 3. All three-factor and higher order interactions are assumed negligible.

**APPENDIX 4** 

Table 19

# 9 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

					<u> </u>								-, .				
								It	em i	num	bers						
Treatment	<u>8</u>	1	2	3	4	5	6	7	8	9	10	11	12	13	14	.15	16
,	A					+			+	+		+		+	+	+	+
	В				+			+	+		+		+	+	+	+	
	C			+			+	+		+		+	+	+	+		
	D		+			+	+		+		+	+	+	.+			
	E				+	+		+		+	+	+	+				+
	F	NONE		+	+		+		+	+	+	+				+	
	G		+	+		+		+	+	+	+				+		
	H		+		+		+	+	+	+		1		+	, .	,	+
	I			+		+	+	+	+				+			+ .	+
Results																	

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

APPENDIX 4

Table 20

# 10 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

							I	ter	nu	nbe	rs						
Treatment	8	1	2	3	4	5	6	7	æ	9	10	11	12	13	14	15	16
	<b>A</b>					+			+	+		+		+	+	+	+
	В	ľ			+			+	+		+		+	+	+	4	
	C			+			+	+		+		+	+	+	+		
	D		+			+	+		+		+	#	+	+			
	E	NONE			+	+		+		+	+ .	+	+				+,
	F	2		+	+		+		+	+	+	+				+	
	G		+	+		+		+	+	+	+				+		. ]
	H		+		+		+	+	+	+				+		,	+
	I			+		+	+	+	+	`		,	+			+	+
	J		+		+	+	+	+			-	+			+	+	
Results																	

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

Table 21

# 11 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

	Г		-			I	tem	nu	mbe	rs						
Treatments	1	2	3	4	5	6	7	8	9	10	.11	12	13	14	15	16
					+			+	+		+		+	+	+	+
В				+			+	+		+		+	, +	+	+	
C			+	'		+	+		+	,	, j +	+	+	+		
I	,	+			. +	+		+		+	+	+	+		<u>'</u>	
I				+	+		+		+	+	+	· +				+
1	.   9		+	+		+		+	+	+	+				+	
C		+	+		+		+	+	+	+				+		
I		+		+		+	+	+	+				+			+
]	:		+		+	+	+	+				+			+	+
,		+		+	+	+	+.				+			+	+	
	ٔ ا		+	+	+	+				+			+	+		+
Results																í

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

Table 22

12 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

•						Ite	m n	למעני	ers				,			
Treatments	i	2	3	4	5	6	7	8	9	1C	11	12	13	14	15	16
A					+			+	+		+		+	+	+	+
В				+			+	+		+		+	+	+	air	
C			+			+	+		+		+	+	+	+		
. <b>D</b>		+			+	+		+		+	+	+	+			
E				+	+		+		+	+	+	+				+
F			+	+		+		+	+	+	+				+	
G	NONE	+	+		+		+	+	+	+		·		+		
H.		+		+	,	+	+	+.	+				+			+
I			+		+	+	+	+				+			+	+
J		+		+	+	+	+				+ 1			+	+	
<b>K</b> .			+	+	+	+				+			+	+		+
L L		+	+	+	+				+			+	+		÷	
Results	Ŀ									,						

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

APPENDIX 4

Table 23

# 13 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

	•						Ite	n n	umb	ers							
Treatments	_	1	2	3	4	5	6	7	8	9	<b>1</b> C	11	12	13	14	15	16
	A					+			+	+		+		+	+	+.	+
	В				+	,		+	+		+		+	+	+	+	
	С		!	+			+	+		+		+	+	+	+		
	D		+			+	+		+		+	4	+	+			
	E		,		+	4		+		+	. +	+	+				+
	F			+	+		+		+	+	+	+		,		+	
	G		+	+		+		+	+	+	+-				+		
	II	NONE	+		+		+	+	+	+				+			+
•	I			+		+	+	+	+				+		·	+	+
	J		+		+	+	,+	+				+	,		+	+	
	K			+	+	+	+				+			+	+		+
•	L		+	+	+	+				+			+	+		+	1.
•	M		+	+	+		<u> </u>		+			+	+		+		+
Results								,									

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

APPENDIX 4

Table 24

# 14 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

		,	- 5								, ,, ,		~ / /				
					<b>-</b>		Ite	= n	umb	ers							
Treatments		1	2	3	4	5	6	7	8	9	1C	11	12	13	14	15	16
	A					+			+	+		+		+	+	+	+
	В		٠		+			+	+		+		+	+	+	+	
•	С			+			+	+		+		+	+	+	+		·
	ם		+			+	÷		+		+	+	+	+			
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Results		•				•											

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.

#### Table 25

# 15 TREATMENTS AND 16 ITEMS

Design: Multifactorial (Ref. 5, page 323)

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		L					Ite	מבב	den	ers			·				$\rightarrow$
Treatments		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
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	В				+			+	+		+		+	+	+	+	
•	C			+			+	+		+		+	+ '	+	+		
	D		+			+	+		+		+	+	+	+			
	E				+	÷		+		+	+	+	÷				+
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	G		+	+		+		+	+	+	+				+		
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Results												1				,	

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.
- 3. The treatment combinations in the individual rows of this design can be used in any combination of two or more, up to and including 15 treatments.

### Table 26

### 19 Treatments and 20 Items

Design: Multifactorial (Ref. 5, page 323)

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Results																1				

- 1. All main effects are confused with interactions.
- 2. All interactions are assumed negligible.
- 3. The treatment combinations in the individual rows of this design can be used in any combination of two or more, up to and including 19 treatments.

23 Treatment and 24 Items Design: Multifactorial (Ref. 5, page 323) Table 27

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All main effects are confused with interactions. Remarks:

નું લં ભં

All interactions are assumed negligible. The treatment combinations in the individual rows of this design can be used in any combination of two or more up to and including 23 treatments.

Table 27 23 Treatment and 24 Items Design: Multifactorial (Ref. 5, page 323)

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	19		+	+	+	+	+					+		+			+	+			+	+		+	
	138	+		+	+	+	÷	+					+		+			+	+			+	+		
	17		+		+	+	+	+	+					+		+			+	+			+	+	
	16	+		+		+	+	+	+	+					+		+			+	+			+	
	15	+	+		+		+	+	+	+	+				-	+		+			+	+			
	1,4		+	+		+	L	+	+	+	+	+					+		+			+	+		
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All main effects are confused with interactions. Remarks:

All interactions are assumed negligible. The treatment combinations in the individual rows of this design can be used in any combination of two or more up to and including 23 treatments.

Table 29 6 Treatments and 32 Items Design: 1/2 X 26 Factorial (Ref. 6, page 7)

	30 37 S	+	+	+	+	+	+		
	25 26 27 28 29	+				+			
	82	+	+	+	+	+	+	'	
	12	,				+	+		
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	<u>31</u>	+	+			+	+		2.5
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Treat-	ments	< -	m	ပ	<b>A</b> 25	M	<b>P4</b>	Blocks	Results

Remarks: 1. All main effects are clear of two-factor interactions.

<sup>2.</sup> All two-factor interactions are measurable.

All three-factor and higher order interactions are assumed negligible.

Table 30 6 Treatments and 32 Items
Design: 1/2 X 26 Factorial (Ref. 6, page 6)

1	TITEM NUMBERS	73 14 17 10 17 10 17 17 17 17 17 17 17 17 17 17 17 17 17	+ + + + + + + + +	+ + + + +	+ + + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + + +	+ + + + + + + +	+ + + + + + + +	VI III IV	
H + + + + + + H	2. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	ि स मिल	+	+	+	+	+	+	11	
		3 4 5 0 7	+	+	+	+	+ +	+	н	

All main effects are clear of two-factor interactions. Remarks:

When blocks are not used, all two-factor interactions are measurable.

All three-factor and higher order interactions are assumed negligible. When blocks are used, interaction BC is not measurable.

Table 31 6 Treatments and 32 Items Design: 1/2 X 2<sup>6</sup> Factorial (Ref. 6, page 6)

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Results							,								,										

All main effects are clear of two-factor interactions.

then blocks are not used, all two factor interactions are measurable. when blocks are used, interactions AD, BC, & EF are not measurable.

ill three-factor and higher order interactions are assumed negligible.

Table 32-7 Treatments and 32 Items

Design: 1/4 x 27 Factorial (Ref. 6, page 20)

Γ	32			+		+	+	+		
1	-		+		<del> </del>		+	+		
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	39		+	+		<del>  '</del>	+			
	28	+		+	+	+		+		
	122	+			+			+		
	26	+			+	+		1		
	53	+		+	+					
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	23	+					+	+		
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Treat-	ments	4	<b>A</b>	ပ	A 26	M	₿¥ę	ပ	Blocks	Results

All main effects are free of two-factor interactions. Remarks:

When blocks are not used interactions AB, AC, AE, BC, RE and CE are EST measurable. When blocks are used interactions AB, AD, AF, BD, BF and RF are not measurable. All three-factor and higher order interactions are assumed negligible.

7 Treatments and 32 Items Design: 1/4 X 27 Factorial (Ref. 6, page 19)

	30 31	· 	+	+ ′	+	+	+	+		
	8	+		+			+			
	82		+	+	+				1	
	12 97	+			+	+				
ľ	92	+	+	+		+	+	+		
	22 23 24 25						+	+		
	72			+		+				
	23	+	+							
		+		+	• +		+	+		
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	17	<del>_</del>	+	+	+	+	+			
SERS	2			+		+	+	+		
NGW	17	+	+				+	+		
ITEM NUMBERS	引	+	,	. +	+					
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Treat-	ments	∢,	æ	<b>υ</b>	A	ы 262	, <b>(%)</b>	•	Blocks	Results

All main effects are free of two-factor interactions. Remarks:

When blocks are not used interactions AB, AC, AE, BC, BE and CE are not measurable. When blocks are used interactions AB, AC, AE, BC, BE, CE and DF are not measurable. All three-factor and higher order interactions are assumed negligible.

i.rreatments and 32 Items
Design: 1/4 X 2 Factorial (Ref. 6, page 19)

Remarks: 1. All main effects are clear of two-factor interactions.

When blocks are not used, interactions AB, AC, AE, BC, HE and CE are not measurable. When blocks are used only interactions AD, AF, AG, BD, HF, BG, CD, CF, CG, EF, EG and HE are measurable.

All three-factor and higher order interactions are assumed negligible.

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	23 24 25 26 27			+	+			+	+		
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Treat-	ments	∢	(4	ບ	A	M	Çing.	o	· 🚾 .	Brocks	Kesults

All main effects are clear of two-factor interactions.

Only the following interactions are measurable: AE, AH, BE, BH, CE, CH, DE, DH, EF, EG,

EH, FH and GH whether or not blocks are used.

Table 36
8 Treatments and 32 Items
Design: 1/8 X 28 Factorial (Ref. 6, page 31)

,	MELLI	ITEM NUNBERS										ĺ		
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+	+	+	+	+	<u>+</u>		+			+		+	<del>                                     </del>	<u> </u>
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main effects are clear of two-factor interactions.

When blocks are not used interactions AE, AH, BE, BH, CE, CH, DE, DH, KF, EG, EH, FH and GH are measurable. When blocks are used interactions AE, AH, BE, BH, CE, CH, DE,

three-factor and higher order interactions are assumed negligible. EF, EG, FH and GH are measurable.

8 Treatments and 32 Items Design: 1/8 X 28 Factorial (Ref. 6, page 30) Table 37

1 1		+			_		,			l	
ITEM	भर हर टा	+	+	+	+	+	+ +	+	+	IV	
ITEM NUMBERS	15 16	+	+	+	+	+	+	+	+		
	०ट 6ा ११ ८७	+	+	+	+	+	+	+	+	Λ	
	21 22 23 24	+	+	+	+ +	+	+	+	+	IA	
	25 26 27 28	+	+	+ +	+	+	+	+	+	VII	
	20 31 32	+	+	+	+	+	+	+	+	VIII	

All main effects are clear of two-factor interactions. Remarks:

Only the following interactions are measurable: AE, AH, BE, BH, CE, CH, DE, DH, KF, EH, FH and GH whether or not blocks are used.

All three-factor and higher order interactions are assumed negligible.

Table 38

9 Treatments and 32 Items Design: 1/16 X 2 Protorial (Ref. 6, page 43)

1 1 2 13 14 15 1 3 (1 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	+	+	1	+	+ + + +	+	+	+	+ + +	
+	+		+	•		1	<del>                                     </del>	<del>                                     </del>	+	
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	+				-			+		
15	+	•		_			+		+	
7	+	+			·	+	ı	+	+	
-+	<del></del> -						-	+	+	·
+	+	+	+	+						
2	+	. +					+	, +		
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<b>*</b>					+	+	+	+		
* 1		*	-+	٠	+	•	•	+		
V		+	+	+						

All main effects are clear of two-factor interactions. Reserks:

Only the following interactions are measurable: AH AI, BH, BI, CH, CI, DH, DI, EH, RI, FH, FI, GH, GI and HI whether or not blocks are used.

Ail three-lactor and higher order interactions are assumed negligible.

Table 3) 9 Ireatments and 32 Items Design: 1/16 X 29 Factorial (Ref. 6, Page 42)

	33	+			+	+		+	+	+		
	31		+	+		+		+	+	+		
	<u>چ</u>		+	+			+			+	,	
	8	+			+		+			+		
	53	+			+		+		+		Δ	
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				•	+	+	+				H	
	7.7	+	+			+	+					<u> </u>
	. 15	+	+		-			+	+			
	17.1			+	+				•			
ERS	16	+		+		+				+		
::EME	15		+		+	4				+		
TTEN NUMBERS	77		+		+		+	+	+	+		
Ħ	1.3	+		٠			+	+	+	+		$\neg$
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	9	+	+	•	+	+	+	+		-		+
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	<u></u>		L		(3 (4)	V 11		L		L	ا ب	+-4
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•	••					ı	268			÷		, se

All main effects & elear of two-factor interactions.

Only the following interactions are measurable: All, AI, BH, BI, CH, CI, DH, DI, EH, KI FH, FL, GH, GI and HI whether or not blocks are used.

three-factor and higher order interactions are assumed negligible.

Table 40

9 Treatments and 32 Items Design: 1/16 X 2 Factorial (Ref. 6, page 42)

	32		+	+		+		+	+	+		
	31	+			+		+			+		
	33	+			+		+		+		H	· · · · ·
	62		+	+		+		+			IIIA	
	28	+	+					+		+		
	12 93			+	+	+	+		+	+	<b>F-4</b>	
				+	+	+	+				1	
	[25]	+	+					+				_
	124		+		+	+				+		
	23	+		+			+	+	+	+		
	8			+		-	+	+			I	
			+	-	-	+						
	19 20 21 22 23 24 55	+	+	+	+				+	+		
								<u></u>		<u>+</u>		
,	7 13	·				+	+	+	+		>	
i	17	+	+	+	*						-	
ERS	97	+			+	+		+	+	+		
UMB	15		+	+			+			+		
ITEM NUMBERS	7,7		+								2	
II	_			+			+		+			· .
	13				+	+		+				-
	12			+	+			+		+	·	, .
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Treat-	nents	<b>4</b>	Ø	<b>U</b>	Q	M	<b>5</b> 9	ဗ	tra	<b>H</b>	Blocks	Regulte

All main effects are clear of two-factor interactions. Remarks:

Only the following interactions are measurable: AH, AI, BH, BI, CH, CI, DH, DI, EH, EI, FH, FI, GH, GI and HI whether or not blocks are used.

All three-factor and higher order interactions are assumed negligible.

Table 41

10 Treatments and 32 House
Design: 1/32 X 2'9 Factofial (Ref. 5: page 53)

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	0.11.0	+	+	+		+	+	+	+	+	+	
1		+	,	+		+	+	'+	+			
TOTAL NUMBERS	77	+	+			+	+	+	+	+	+	
		٠			**		+	, +	4.	+		
	200	•	+	+	- + - +	<u> </u>	+	+	+	<b>+</b>	+	
	20 21 25 2	+	+	+	*	+	+		<u>+</u>	.+	<u>+</u>	
	23 24 25	+			+	+		+		+	+	H -
	5	+	, +	+		+	+		+	+		
	5/ 50 59	+	+.	+			+	+		+	+	
	1 30 31	+	+	+	+	+	+		+			
	R		+		+	+		+			+	'

All main effects are clear of two-factor interestions. None of the two-factor interactions are measurable. Remarks:

All three-factor and ingher order interactions are assumed negligible.

Table 42 10 Treatments and 32 Items Design: 1/32 X 2<sup>10</sup> Factorial (Ref. 6, page 52)

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	8		+		+	+		+			+		,
	3	+		· +	'		+		+		+		
	8		+		+	+			+	+			
	8	+		+			+	+		+			
	88		+	+			+	+			+	IV	
ļ	27	+			+	+			+		+		
1	50		+	+			+		+	. +			
	23/24/125	+			+	+		+		+			
	2	+		. +		+		÷			+		
1	23		+		+		+		+	,	+		
	23	+		. +		+		·	+	+			
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	117		+	+		.+		+		+			
SHE	79		-	+	+					+	+		ļ
TOMEN	15	+	+			. +	+	-+	+	+	+		
ITEM NUMERERS	77			+	+			+	+				
F	13										_		
	72	+	+			+	+					н	
	Н	· · ·		,		+	+			+	+	II	-
			+	. +	+			+	+	+	+		
	21					+	+	. +	+			,	
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Treat-	ments	Y	Ø	ပ	A	̈Μ	271	O	Ħ	H	<b>13</b>	Blocks	Results

All main effects are clear of two-factor interactions. Remarks:

નં લં ભં

None of the two-factor interactions are measurable.
All three-factor and higher order interactions are assumed negligible.

Table 43 10 Treatments and 32 Items Design: 1/32 X 2 10 Factorial (Ref. 6, page 52)

Treat-						: }				1				LUZI	E	ITEM NUMBERS	100											İ		İ		
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Blocks		н				Ħ	-			III				IV				>				VI				ΙŅ	<b>—</b>			VIII	ы	
Results							,							٠.																	·· · · · ·	
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Remarks: 1. All main effects are clear of two-factor interactions.

<sup>2.</sup> None of the two-factor interactions are measurable.

All three-factor and ingher order interactions are assumed negligible.

Table 44
11 Treatments and 32 Items
Design: 1/64 X 2" Factorial (Ref. 6, page 58)

	رر													
	733		+		+		+			. +	+		ł	7.
	0 31	+		+			+			+	+	_+		
	30	+		+		+		+	+			+		
	88 83		+		+	+		+	+				_	
	K Z		+		+		+		+			_+	À	
	2	+		+			+		+				• •	
	5 26	-+		+		+		+		+	+			
	54 55					+		+		<u>+</u>			==	==
,	32		+	+		+	+	+	,	+				
	22 23	+			+	+	+	+		+		_+		
		+			+				+		+	-+	.	
	22		+	+					+		+		H	
	02 61		+	+		+	+	+	+		+	+	Н	
		+			+	+	+	+	+		+			
	81 12	+			+					+			. }	
	17		+	+						+	-	+		
55	16			+	+		+	+			+	+		
TUMB	15	+	+	,			+	+	·		+	-		
item numbers	14	+	+			+			+	+				
II	13			+	+	+			+	+		+		
	75						+	+	+	+	-			
	11			+	+								ΊΪ	
	1 0	+	+				+	+	÷	+		+	Ĭ.	
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,	6			+	+	+					+			
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	II	+	+	+	+	+	+	+						
	9]	+	.+	+	+				+	+	+			
	3	ŕ							+	+	+	+		
	7					+	+	+	+	+	+		H	
	3	+	+	+	+	+	+	+	+	+	+	. +	•	$\vdash$
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Treat-	ments	≺	М	v	A	M	β <b>.</b> ,	<b>.</b>	', <b>#</b>	<b>.</b>	حر	×	Blocks	Results

All main effects are clear of two-factor interactions. નં લં ભં

None of the two-factor interactions are measurable.

All three-factor and higher order interactions are assumed negligible.

Table 45 12 Treatments and 32 Items Design: 1/128 X 2<sup>12</sup> Factorial (Ref. 6, page 65)

	П														
	걵			+	+		+			+	+	+	+		
	30 31	+	+		+		+			+					
	<u> 130</u>		+	+			+	+	+	÷	+				
	82	+					+	+	+	+		+	+		
	႘ၟ	+			+	+						+	+	IV	
	$\mathbf{Z}$		+	+	+	+					+				,
	92	+	+			+		+	+						
	25			+		+		+	+		+	+	+		
	<del>†</del> 2			+	+		+		+				+		
	23	+	+		+		4.		+		+	+			
	22		+	. +			+	+				+			
	77	+					+	+			+		+		
	18 19 20 21 22 23 24  25 26 27 28 29	+			+	+			+	+	+		+	İII	
	61		+	+	+	+			÷	+		+		,	
	118	+	+			+		+		+	+	+			
	17			+	-	+		+		+			+		
ERS	16	,			+	+	+	+			+	+			,
ITEM NUMBERS	15														<u>'</u>
M.		+	+	+	+	+	+	+					+		
II	14		+			+	+		+		+		+		·
	13	+		+		+	+		+			+		٠	
	21.	+		+	+			+		+	,	+		11	
	11		+		+			+	·	+	+		+		
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	7	+	+	+					+	+			+		
	6										+	<u></u>			
	8				+	+	+	+	+	+		,			
	17	+	+	+	+	+	+	+	+	+	+	+	+		
,	9		+			+	+	_		+		+	+		-
	. 5	+		+		+	+			+	+				
	†	+		+	+			+	+		+			H	ļ
	3		+		+			+	+			+	+		
	2	+	+	+				7 1	0 17		+	+	+		
	_		<u>.</u>	<u> </u>		<u> </u>	<u> </u>	N E	ОИ	<u> </u>	L	L	<u> </u>	<u> </u>	<u> </u>
Treat-	ments	₹	m	့ ပ	A	ĸ	Į <b>s</b>	to	· ##	H	, <b>b</b>	×	H	Blocks	hecults

1. All main effects are clear of two-factor interactions. Remarks:

None of the two-factor interactions are measurable. All three-factor and higher order interactions are assumed negligible.

Table 46 13 Treatments and 32 Items Design:  $1/256 \times 2^{13}$  Factorial (Ref. 6, page  $7^{14}$ )

	<b>T</b>	<del></del>			<u> </u>			r	r		,	<u> </u>		•			
	었		+		+		+		+		+		+				_
	31	+	-	+		+		+		+		+		+			
	30	+	+				+		+	+	+			+			
	8			+	+	+		+			,	+	+				
	58	·	+	+				+			+		+	+	Δ		
	62   53   54   52   56   54   58   56	+		,	+	+	+		+	+		+					
	56	+	+	+	+			+		+	+						
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Ħ	1.3			+	+			,	+	+	+	+					
1	75		+	+		+			+	+				+	11		
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1	7	+		+			+	+	+	+			+				
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ļ	7		+	+		+	+	+	+		+	+			H		
	3	+			+					+			+	+			
1	5	+	+	+	+	+	+	+	+	+	+	+	+	+			
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Treat-	ments	∢	Д	ບ	A	M	faq	27!	# 5	н	73	×	w	×	Blocks	Results	,

All main effects are clear of two-factor interactions.
None of the two-factor interactions are measurable.
All three-factor and higher order interactions are assumed negligible. નાં હાં ભં

Table 47

Multifactorial (Ref. 5, page 323) 31 Treatments and 32 Items Design:

Treatments

_		_						_	<del></del> ;																			_					
	ĸ		+			+		+	+			+	+	+	+	+			+	+			+	+	+		+		+				
	31			+			+	Ι.	+	+			+	+	4	+	+		_	+	+			+	+	+		+		+			7
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All main effects are confused with interactions. Results: Remarks:

All interactions are assumed negligible. The treatment combinations in the individual rows of this design can be used in any

combination of two or more up to and including 31 treatments.

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#### PREFACE

This handbook is intended as a guide for determining reliability of functioning characteristics of weapon components by testing to failure.

Component reliability of weapon systems is basically a function of engineering design. Margins of safety used in engineering design to create high reliabilities must be measured by testing to failure techniques to obtain unbiased estimates of reliability.

The author does not hold that the concepts and principles presented herein are final. Revisions will inevitably be made as the state of the art advances.

#### **ACKNOWLEDGEMENTS**

The following tables have been used thru the kind permission of the publishers and authors:

#### Appendix 3A

Mainland, Donald; Herrera, Lee; and Sutcliffe, M.I.; "Tables for Use with Binomial Samples", Dept of Medical Statistics, N.Y. Uni., College of Medicine, 550 First Ave, NYC 16, N.Y. Table I: Minimum Contrasts at the 5 per cent Level, pages 1, 2, and 3: Table II: Minimum Contrasts for the 1 per cent Level, pages 5, 6, and 7.

#### Appendix 3B Table I

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#### Appendix 3C and 3F

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#### Appendix 3D

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#### Appendix 3E

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#### Appendix 4 (Multifactorials)

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### ppendix 3H

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